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16 September 2008

Certificate

The PRELIMINARY GEOTECHNICAL ASSESSMENT – PROPOSED SUBDIVISION DEVELOPMENT HEARNS LAKE, SANDY BEACH, CH1132-1AB Report, dated 28 January 2004, has been reviewed and it contains all available current information that is relevant to the environmental assessment of that aspect of the Concept Plan Approval Application to which the Report relates.

The information contained in this Report is neither false nor misleading.

I certify that I have reviewed the contents of the PRELIMINARY GEOTECHNICAL ASSESSMENT CH1132-1AB, 28 January 2004, and that it is true in all material particulars and does not by presentation or omission of information, materially mislead.

For and on behalf of Coffey Geotechnics Pty Ltd

Jeber Balan

Andrew Ballard

Associate Environmental Scientist
Environmental Team Leader – Coffs Harbour

BLUEGRASS NOMINEES

PROPOSED SUBDIVISION DEVELOPMENT

Hearns Lake, Sandy Beach

PRELIMINARY GEOTECHNICAL ASSESSMENT

CH1132/1-AB

28 January 2004



CH1132/1-AB DJB 28 January 2004

Bluegrass Nominees 33 Windsor Crescent BROWNSVILLE NSW 2530

Attention: Mr John Oliver

Dear Sir,

RE: PROPOSED SUBDIVISION DEVELOPMENT – HEARNS LAKE, SANDY BEACH PRELIMINARY GEOTECHNICAL ASSESSMENT

Coffey Geosciences Pty Ltd (Coffey) is pleased to present our report on the preliminary geotechnical investigation for the proposed subdivisional development near Hearns Lake at Sandy Beach.

We draw your attention to the attached sheet entitled "Important Information About Your Coffey Report" which should be read in conjunction with this report.

We trust that this report meets with your requirements. If you require further information please contact the undersigned in our Coffs Harbour office.

For and on behalf of

COFFEY GEOSCIENCES PTY LTD

IAN SHIPWAY

Manager, Northern NSW

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20 copies Bluegrass Nominees

Coffey

Email coffs@coffey.com.au

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IMPORTANT INFORMATION ABOUT YOUR COFFEY REPORT

FIGURES

Figure 1 Site Plan

APPENDICES

- A Engineering Logs
- B Laboratory Test Reports

Coffey ****

1. INTRODUCTION

Coffey Geosciences Pty Ltd has conducted a geotechnical assessment for proposed subdivision development of a 35 hectare site located near Hearns Lake at Sandy Beach. The client has indicated that the site will be split into 14 assemblages, with only Assemblages 1, 2 and 13 proposed for residential and rural-residential development. It has been estimated from plans provided by the client that the development area is about one half of the total site area or about 15 to 20 hectares.

The aims of the study, which was commissioned by Localplan Pty Ltd, were to provide a preliminary assessment of the suitability of the site for residential development including subsurface conditions across the development area, acid sulfate soils and potential for soil contamination and general advice on the geotechnical conditions encountered at the site relevant to residential development. An assessment of groundwater levels and fluctuations was also carried out, though the results of water level monitoring are not complete at this stage and will be forwarded when complete and assessed.

Coffey conducted the work in general accordance with proposal no. CH1132/1-AA of 26 November 2003. This report presents the results of the site investigation and provides comments and recommendations relevant to the above scope of work.

2. SITE DESCRIPTION & PROPOSED DEVELOPMENT

The site is situated just north of the residential area of Sandy Beach to the east of the Pacific Highway. The site, comprising Assemblages 1, 2 and 13 is about 15 to 20 hectares in area. The ground surface is generally flat lying with varying densities of scrub and trees. The more densely vegetated areas fall into assemblages which the client has indicated are not to be developed at this stage.

It is understood that Assemblages will be developed for residential use and part of assemblages 2 and 13 for rural-residential purposes.

3. FIELD WORK AND LABORATORY TESTING

Field work for the geotechnical assessment was conducted on 8 December 2003 and consisted of the excavation of twelve test pits (TP1 to TP12) to between 2.0m and 3.5m depth using a JCB 4WD Backhoe. In addition, five boreholes (GW1 to GW4 including GW2a) were drilled on 19 December 2003 to depths of about 4m using a 4WD mounted MD200 drill rig. Groundwater monitoring wells were installed in four of the boreholes (GW1, GW2a, GW3 and GW4) and equipped with electronic data loggers to monitor water level fluctuations.

The test pits/boreholes were excavated/drilled in the full time presence of a geotechnical engineer from Coffey who located the pits/boreholes, took samples and produced engineering logs of the subsurface conditions encountered. The engineering logs are presented in Appendix A, together with explanation sheets defining the terms and symbols used in their preparation. Test pit and borehole locations are shown on Figure 1.

Samples obtained during test pitting were placed in a chilled esky during field work and transport to our Coffs Harbour laboratory where they were placed in refrigerated storage. Laboratory testing was conducted in our Coffs Harbour laboratory and consisted acid sulphate soil screening tests on 12 samples of soils taken from a number of depths in TP2, TP5, TP8 and TP12. The results of the screening tests are shown in Table 1 presented in Appendix B. Samples were screened using laboratory methods 21Af and 21Bf of Ahern, CR,

Blunden, B and Stone, Y (eds) (1998), Acid Sulfate Soil Laboratory Methods Guidelines, ASSMAC, which tests pH of soils in distilled water and 30% Hydrogen Peroxide (H₂O₂). Screening test results are attached.

Following the screening tests, four samples were selected and sent to an external analytical laboratory for further Peroxide Oxidisable Combined Acidity and Sulfate (POCAS) testing. The results of this testing are also presented in Appendix B.

GROUND CONDITIONS

4.1 Sub-Surface Stratigraphy

The Dorrigo/Coffs Harbour 1:250,000 geological map shows that the site is underlain by Quaternary aged alluvium and rock of the Coramba Beds, which mainly comprises siltstone and greywacke with minor volcanic intervals.

The subsurface conditions observed in the test pits generally fall into one of three geological units, comprising:

- Unit 1 Residual soil overlying weathered siltstone observed in TP1. Subsurface conditions comprised shallow silty clay topsoil, overlying stiff to hard sandy and silty gravely clay, grading to weathered siltstone at about 1.5m depth.
- Unit 2 Alluvial soil deposits observed in TP2 to TP9 and underlain by residual soils in TP2 and possibly TP3. The subsurface conditions for this unit generally consisted of a 100mm to 200mm thick topsoil layer overlying stiff to hard medium to high plasticity silty and sandy clay, to beyond the limit of investigation in TP6. In other test pits, clayey alluvial soils were underlain by either residual clay soils in TP2 and possibly TP3 from a depth of about 2m, or alluvial clayey sand and sand soils from depths of about 2m to 2.5m in TP4 and TP7 to TP9 and 0.5m in TP5 to beyond the limit of investigation.
- Unit 3 Aeolian and alluvial beach deposits observed in TP10 to TP12. The subsurface conditions for this unit generally consisted of a 100mm to 300mm thick topsoil layer overlying mainly sand and sand with some clay fines, with some clayey sand layers observed in TP10, to beyond the limit of investigation.

As mentioned previously, information on groundwater levels at the site will be forwarded in a separate letter when monitoring has been completed. Water levels in the monitoring wells on the day of drilling were between about 0.6m and 2.4m depth below ground level. Water inflow in GW3 was first observed at 1.7m depth, with the water level rising after drilling to 0.6m depth. This borehole was drilled relatively close to the lake edge as shown on Figure 1, and thus a drop in ground level or the lake water level may have caused the high water level in this borehole. A water level of 1.95m was recorded in GW2a after drilling, which is located about 100m to the south west of GW3. More information on water levels at the site will be forwarded after the completion of monitoring.

DISCUSSION AND RECOMMENDATIONS

5.1 General Suitability with Respect to geotechnical Constraints

Based on the results of the preliminary assessment, the site is generally considered to be suitable for





The test pits indicated that subsurface conditions are suitable for residential developments supported on high level footings founded in the natural clay or sand soils. Some additional site preparation may be required for developments founded in sand soils, particularly towards the eastern side of the site, which would most likely consist of compaction with a vibrating roller if required. This report should not be used for the design of footings for developments on the site. More detailed assessment of the site is recommended prior to development.

Subgrade soils for road construction are likely to vary between clay and sand soils, both of which are considered suitable for pavement support. Clay soils are expected to require a thicker pavement due to a generally lower California Bearing Ratio (CBR), though the need for unusually thick pavements is considered unlikely. Some subgrade replacement and/or use of geofabric may be required in some areas, though this is the case for many residential subdivision sites.

Where excavation is required, such as for service trenches, footings and roads, it is anticipated that all site materials could be excavated by conventional dozer blade or backhoe bucket at least to the depths indicated on the attached field logs. Excavations may experience water inflow, which is likely to occur more often and at a greater rate in sand soils than can be expected in clay soils. Depths of water inflows observed during test pitting are shown on the engineering logs. Additional information on water levels at the site will be forwarded separately. Results of the assessment of acid sulfate soils are presented below.

Soils observed in test pits are considered to be suitable for the placement of fill, though again some over excavation, geofabric or additional site preparation may be required in some areas. Soils appeared to be generally suitable for re-use as general site fill, though additional testing of soils may be required to confirm this. Topsoil or root affected material should not be re-used as general fill.

Based on the proximity of the site to environmentally sensitive areas, it is our opinion that that site is generally unsuitable for on-site effluent disposal. Further assessment of site suitability for effluent disposal should be carried out if this is proposed in rural-residential developments.

Sand soils may be suitable for disposal of stormwater from future developments by infiltration into site soils. Clay soils would be considered to have low potential for stormwater disposal by infiltration due to their relatively low permeability. Further assessment of infiltration suitability and flow rates should be carried out prior to development.

5.2 Acid Sulfate Soils

5.2.1 Formation and Potential Impacts

Acid Sulfate Soils (ASS) are soils which contain significant concentrations of pyrite which, when exposed to oxygen, in the presence of sufficient moisture, oxidises, resulting in the generation of sulfuric acid. Unoxidised pyritic soils are referred to as potential ASS. When the soils are exposed, the oxidation of pyrite occurs and sulfuric acids are generated, the soils are said to be actual ASS.

Pyritic soils typically form in waterlogged, saline sediments rich in iron and sulfate. Typical environments for the formation of these soils include tidal flats, salt marshes and mangrove swamps below about RL 5m AHD. They can also form as bottom sediments in coastal rivers and creeks.

Pyritic soils of concern on low lying NSW and coastal lands have mostly formed in the Holocene period, (ie. 10,000 years ago to present day) predominantly in the 7,000 years since the last rise in sea level. It is



generally considered that pyritic soils which formed prior to the Holocene period (ie: >10,000 years ago) would already have oxidised and leached during periods of low sea level which occurred during ice ages, exposing pyritic coastal sediments to oxygen.

Disturbance or poorly managed development and use of acid sulfate soils can generate significant amounts of sulfuric acid, which can lower soil and water pH to extreme levels (generally <4) and produce acid and salts, resulting in high salinity.

The low pH, high salinity soils can reduce or altogether preclude vegetation growth and can produce aggressive soil conditions which may be detrimental to concrete and steel components of structures, foundations, pipelines and other engineering works.

Generation of the acid conditions often releases aluminium, iron and other naturally occurring elements from the otherwise stable soil matrices. High concentrations of some such elements, coupled with low pH and alterations to salinity can be detrimental to aquatic life. In severe cases, affected waters flowing off-site can have detrimental effect on aquatic ecosystems.

5.2.2 Acid Sulfate Soils Risk Map

Reference to the Acid Sulfate Soils Risk Map for Moonee Beach (reference 9537S4) indicates the site is located in an area where there is a high probability of the occurrence of acid sulfate soils at shallow depths (<1m) along the western edge of Hearns Lake for a distance of about 100m to 200m. The remainder of the site was judged to be in an area of high probability of acid sulfate soils at a depth of about 1m to 3m from the ground surface.

5.2.3 Test Results

Sampling and testing for the assessment of acid sulfate soils is discussed in section 3.

The results of all soil screening and laboratory tests conducted are presented in Appendix B, and are summarised in Table 2, which also compares results to action criteria presented in ASSMAC 1998 Acid Sulfate Soil Guidelines.





TABLE 2 – RESULTS OF LABORATORY TESTING

LOCATION	DEPTH (m)	TEXTURE	pH in H ₂ O ₂	%S _{CR}	Action Criteria Value for S _{POS} (%)	TPA (mole/tonne)	Action Criteria Value for TAA (mol/t)
TP2	0.5	Fine	6.7	-	0.1	-	62
TP2	1.0	Fine	5.4	-	0.1	-	62
TP2	2.0	Fine	5.2	-	0.1	-	62
TP5	0.2	Fine	3.9	<0.01	0.1	6	62
TP5	0.7	Coarse	3.4	0.12	0.03	224	18
TP5	2.0	Coarse	3.2	0.05	0.03	43	18
TP8	0.5	Fine	4.7	-	0.1	-	62
TP8	1.0	Medium	6.4	-	0.06	-	36
TP8	2.5	Coarse	6.3	-	0.03	-	18
TP11	1.0	Coarse	6.3	-	0.03	-	18
TP11	2.3	Coarse	6.2	-	0.03	-	18
TP11	2.7	Coarse	3.2	0.04	0.03	8	18

Note: Values in bold exceed action criteria for less than 1000 tonnes of soil disturbed.

Action criteria have been adopted from those presented in ASSMAC (1998) Acid Sulfate Soil Guidelines for excavations of less than 1000 tonnes of soil. Values exceeding action criteria for excavations of less than 1000 tonnes also exceed action criteria for excavations greater than 1000 tonnes.

The following points are noted from the soil screening and laboratory test results presented in Table 2:

- Soil pH<3 in the H₂O₂ test is an indication of potential acid sulfate soil. Soils samples with a value of about pH of 3 were considered to be potential acid sulfate soils;
- Oxidisable Sulfur in three of the four samples analysed exceeded the action criteria values in Table
 4.4 of the ASSMAC Guidelines and hence construction work should be accompanied by an Acid Sulfate Soils Management Plan;
- Total Potential Acidity in two of the four samples analysed exceeded the action criteria values in Table 4.4 of the ASSMAC Guidelines and hence a management plan and development consent are required prior to development.

5.2.4 Interpretation of Results

The acid sulfate soils assessment was based on a limited amount of sampling over quite a large site. The preliminary assessment has indicated that acid sulfate soils are present within the Alluvial materials (Unit 2). It is recommended that more detailed assessment of acid sulfate soils be carried out when the location and size of excavations is known, which may involve test pitting to further assess the extent of alluvial soils and/or additional sampling and testing on proposed excavation areas. Following assessment of the extent of the acid sulfate conditions, an Acid Sulphate Soils management plan should be prepared to guide development of the site.

5.3 Potential Contamination

Based on a walkover assessment during field work, the site does not appear to have been developed for any particular use apart from possibly grazing animals. No obvious signs of soil contamination were observed during the walkover assessment or during excavation/drilling of test pits/boreholes.

The site is currently zoned for low density residential and tourism purposes, with the surrounds of Hearns Lake zoned for environmental protection.

Based on there being no signs of contamination or potentially contaminating developments observed at the site, and the current zoning, it is our opinion that there is a low likelihood of significant concentrations of contaminants being present on the site. Areas of potential contamination, if any, would be likely to be isolated and result from minor spills and leaks from vehicles, plant or containers, or past agricultural use.

5.4 Additional Comments

The site is considered to be suitable for residential and rural-residential development in general.

It is recommended that a geotechnical consultant review the requirements for additional assessment of the site once the development type and location are known in more detail.

We trust that this information meets your requirements for the project at this stage. Details of groundwater monitoring will be forwarded as soon as possible.

For and on behalf of

COFFEY GEOSCIENCES PTY LTD

IAN SHIPWAY

Manager - Northern New South Wales



Information

Important information about your **Coffey** Report

As a client of Coffey you should know that site subsurface conditions cause more construction problems than any other factor. These notes have been prepared by Coffey to help you interpret and understand the limitations of your report.

Your report is based on project specific criteria

Your report has been developed on the basis of your unique project specific requirements as understood by Coffey and applies only to the site investigated. Project criteria typically include the general nature of the project; its size and configuration; the location of any structures on the site; other site improvements; the presence of underground utilities; and the additional risk imposed by scope-of-service limitations imposed by the client. Your report should not be used if there are any changes to the project without first asking Coffey to assess how factors that changed subsequent to the date of the report affect the report's recommendations. Coffey cannot accept responsibility for problems that may occur due to changed factors if they are not consulted.

Subsurface conditions can change

Subsurface conditions are created by natural processes and the activity of man. For example, water levels can vary with time, fill may be placed on a site and pollutants may migrate with time. Because a report is based on conditions which existed at the time of the subsurface exploration, decisions should not be based on a report whose adequacy may have been affected by time. Consult Coffey to be advised how time may have impacted on the project.

Interpretation of factual data

Site assessment identifies actual subsurface conditions only at those points where samples are taken and when they are taken. Data derived from literature and external data source review, sampling and subsequent laboratory testing are interpreted by geologists, engineers or scientists to provide an opinion about overall site conditions, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist, because no professional, no matter how qualified, can reveal what is hidden by

earth, rock and time. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. For this reason, owners should retain the services of Coffey through the development stage, to identify variances, conduct additional tests if required, and recommend solutions to problems encountered on site.

Your report will only give preliminary recommendations

Your report is based on the assumption that the site conditions as revealed through selective point sampling are indicative of actual conditions throughout an area. This assumption cannot be substantiated until implementation has commenced and therefore your report recommendations can only be regarded as preliminary. Only Coffey, who prepared the report, is fully familiar with the background information needed to assess whether or not the report's recommendations are valid and whether or not changes should be considered as the project develops. If another party undertakes the implementation of the recommendations of this report there is a risk that the report will be misinterpreted and Coffev cannot be held responsible misinterpretation.

Your report is prepared for specific purposes and persons

To avoid misuse of the information contained in your report it is recommended that you confer with Coffey before passing your report on to another party who may not be familiar with the background and the purpose of the report. Your report should not be applied to any project other than that originally specified at the time the report was issued.





Interpretation by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a report. To help avoid misinterpretations, retain Coffey to work with other project design professionals who are affected by the report. Have Coffey explain the report implications to design professionals affected by them and then review plans and specifications produced to see how they have incorporated the report findings.

Data should not be separated from the report*

The report as a whole presents the findings of the site assessment and the report should not be copied in part or altered in any way.

Logs, figures, drawings etc. are customarily included in our reports and are developed by scientists, engineers or geologists based on their interpretation of field logs (assembled by field personnel) and laboratory evaluation of field samples. These logs etc. should not under any circumstances be redrawn for inclusion in other documents or separated from the report in any way.

Geoenvironmental concerns are not at issue

Your report is not likely to relate any findings, conclusions, or recommendations about the potential for hazardous materials existing at the site unless specifically required to do so by the client. Specialist equipment, techniques, and personnel are used to perform a geoenvironmental assessment. Contamination can create major health, safety and environmental risks. If you have no information about the potential for your site to be contaminated or create an environmental hazard, you are advised to contact Coffey for information relating to geoenvironmental issues.

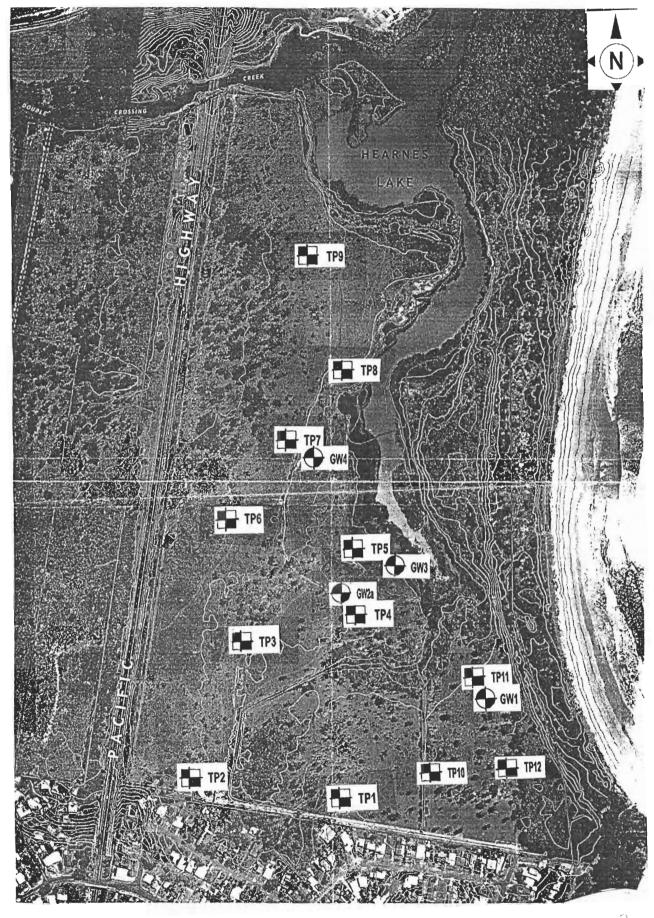
Rely on Coffey for additional assistance

Coffey is familiar with a variety of techniques and approaches that can be used to help reduce risks for all parties to a project, from design to construction. It is common that not all approaches will be necessarily dealt with in your site assessment report due to concepts proposed at that time. As the project progresses through design toward construction, speak with Coffey to develop alternative approaches to problems that may be of genuine benefit both in time and cost.

Responsibility

Reporting relies on interpretation of factual information based on judgement and opinion and has a level of uncertainty attached to it, which is far less exact than the design disciplines. This has often resulted in claims being lodged against consultants, which are unfounded. To help prevent this problem, a number of clauses have been developed for use in contracts. reports and other documents. Responsibility clauses do not transfer appropriate liabilities from Coffey to other parties but are included to identify where Coffey's responsibilities begin and end. Their use is intended to help all parties involved to recognise their individual responsibilities. Read all documents from Coffey closely and do not hesitate to ask any questions you may have.

* For further information on this aspect reference should be made to "Guidelines for the Provision of Geotechnical Information in Construction Contracts" published by the Institution of Engineers Australia, National Headquarters, Canberra, 1987.



ASQUITH JdeWITT



Coffey Geosciences		
Drawn	DJB	
Approved	8	
Date	30/1/04	
Scala	4.4000	

Pty Ltd AC1056335516 Geotechnical I Resources | Environmental I Technical | Project Management LOCALPLAN PTY LTD
PROPOSED DEVELOPMENT
HEARNS LAKE SANDY BEACH
TEST PIT LOCATION PLAN

FIGURE 1

Job no CH1132/1-AB

APPENDIX A

ENGINEERING LOGS

Soil Description

Explanation Sheet



DEFINITION:

In engineering terms soil includes every type of uncemented or partially cemented inorganic or organic material found in the ground. In practice, if the material can be remoulded or disintegrated by hand in its field condition or in water it is described as a soil.

Other materials are described using rock description terms.

CLASSIFICATION SYMBOL & SOIL NAME

Soils are described in accordance with the Unified Soil Classification (USC) as shown in the table on the following page.

PARTICLE SIZE DESCRIPTIVE TERMS

NAME	SUBDIVISION	SIZE		
Boulders		>200mm		
Cobbles		63mm to 200mm		
Gravel	coarse	20mm to 63mm		
	medium	6mm to 20mm		
	fine	2.36mm to 6mm		
Sand	coarse	600µm to 2.36mm		
	medium	200μm to 600μm		
	fine	75μm to 200μm		

MOISTURE CONDITION

Dry	Looks and feels dry. Cohesive and cemented soils
-	are hard, friable or powdery. Uncemented
	granular soils run freely through hands.

Soil feels cool and darkened in colour. Cohesive Moist soils can be moulded. Granular soils tend to

Wet As for moist but with free water forming on hands when handled.

CONSISTENCY OF COHESIVE SOILS

	UNDRAINED			
TERM	STRENGTH	FIELD GUIDE		
	su (kPa)			
Very Soft	<12	A finger can be pushed well into the soil with little effort.		
Soft	12 - 25	A finger can be pushed into the soil to about 25mm depth.		
Firm	25 - 50	The soil can be indented about 5mm with the thumb, but not penetrated.		
Stiff	50 - 100	The surface of the soil can be indented with the thumb, but not penetrated.		
Very Stiff	100 - 200	The surface of the soil can be marked, but not indented with thumb pressure.		
Hard	>200	The surface of the soil can be marked only with the thumbnail.		
Friable	-	Crumbles or powders when scraped by thumb nail.		

DENSITY OF GRANULAR SOILS

TERM	DENSITY INDEX (%)		
Very Loose	Less than 15		
Loose	15 - 35		
Medium Dense	35 - 65		
Dense	65 - 85		
Very Dense	Greater than 85		

MINOR COMPONENTS

TERM	TERM ASSESSMENT GUIDE		N OF MINOR NENT IN:
		Coarse grained	Fine grained
Trace of	Presence just detectable by feel or eye, but soil properties little or no different to general properties of primary component.	<5%	<15%
With some	Presence easily detected by feel or eye, soil properties little different to general properties of primary component.	5% - 12%	15% - 30%

SOIL STRUCTURE -

	ZONING	CEMENTING			
Layers	Continuous across exposure or sample	Weakly cemented	Easily broken up by hand in air or water		
Lenses	Discontinuous layers of lenticular shape	Moderately cemented	Effort is required to break up the soil by hand in air or water		
Pockets	Irregular inclusions of differential material				

GEOLOGICAL ORIGIN

WEATHERED IN PLACE SOILS

Extremely	Structure and fabric of parent rock visible
veathered material	

Residual soil Structure and fabric of parent rock not

TRANSPORTED SOILS

Aeolian soil	Deposited by wind
Alluvial soil	Deposited by stream and rivers
Colluvial soil	Deposited on slopes (transported downslope by gravity)
Fill	Man made deposit. Fill may be significantly more variable between tested locations than naturally occurring soils.
Lacustrine soil	Deposited by lakes
Marine soil	Deposited in ocean basins, bays, beaches

and estuaries

SOIL CLASSIFICATION INCLUDING IDENTIFICATION AND DESCRIPTION

	/5	Evaluding part		ATION PROCEDURES	ortimated mass)	USC	PRIMARY NAME				
	(1	excluding part	ticles larger than 60mm	and basing fractions on	estimated mass)	-					
rger		coarse r than	CLEAN GRAVELS (Little or no fines)	Wide range in grain size and substantial amount all intermediate particle sizes.		GW	GRAVEL				
n is la	l eye)	GRAVELS Nore than half of coarse fraction is larger than 2.0mm	CLI GRA (Littl no f	Predominantly one size more intermediate size	e or a range of sizes with es missing.	GP	GRAVEL				
LS n 63mr		GRAVELS tan half of on is large 2.0mm	ELS INES able t of	Non-plastic fines (for it ML below)	dentification procedures see	GM	SILTY GRAVEL				
COARSE GRAINED SOILS More than 50% of material less than 63mm is larger than 0.075mm	the nake	GRAVELS More than half of fraction is larger 2.0mm	GRAVELS WITH FINES (Appreciable amount of fines)	Plastic fines (for identi below).	ification procedures see CL	GC	CLAYEY GRAVEL				
RSE GR nateria than 0.	sible to	parse than	CLEAN SANDS (Little or no fines)	Wide range in grain siz all intermediate sizes i	es and substantial amounts of missing.	SW	SAND				
COA	icle vi <u>s</u>	DS If of connaller	CLL SAI (Litt	Predominantly one size or a range of sizes with some intermediate sizes missing.		SP	SAND				
than 5	t parti	SANDS nan half o nn is small 2.0mm	DS H SS iable t of	Non-plastic fines (for identification procedures see ML below).		SM	SILTY SAND				
More	smalles	SANDS More than half of coarse fraction is smaller than 2.0mm	SANE WITI FINE (Apprec amoun fines	SONT SUBJECT OF STATE		SC	CLAYEY SAND				
	IDENTIFICATION PROCEDURES ON FRACTIONS <0.2mm										
_	(A 0.075mm particle is about the smallest particle visible to the naked eye)		DRY STRENGTH	DILATANCY	TOUGHNESS						
FINE GRAINED SOILS More than 50% of material less than 63mm is smaller than 0.075mm		SILTS AND CLAYS Liquid limit less than 50	None to Low	Quick to slow	None	ML	SILT				
SOILS terial l		rs AND uid lim than	rS AND uid lim than	rS AND CL uid limit l than 50	rS AND uid lim than	rS AND uid lim than	Medium to high	None	Medium	CL	CLAY
RAINED of mai		SILT	Low to medium	Slow to very slow	Low	OL	ORGANIC SILT				
FINE GRAINED SOILS ore than 50% of material less th 63mm is smaller than 0.075mm	(A 0.0	CLAYS limit than 50	Low to medium	Slow to none	Low to medium	МН	SILT				
ore tha 63mm		SILTS & CLAYS Liquid limit greater than 50	High	None	High	СН	CLAY				
¥		SILT Lic great	Medium to high	None	Low to medium	ОН	ORGANIC CLAY				
HIGHLY O	RGANI	C SOILS	Readily identified by texture	colour, odour, spongy fe	eel and frequently by fibrous	Pt	PEAT				
Low pla	sticity	- Liquid Limi	t W _L less than 35%. Me	dium plasticity - W_L betw	veen 35% and 50%.						

COMMON DEFECTS IN SOIL

	TERM	DEFINITION	DIAGRAM
	PARTING	A surface or crack across which the soil has little or no tensile strength. Parallel or sub parallel to layering (eg bedding). May be open or closed.	
	ТИІОС	A surface or crack across which the soil has little or no tensile strength but which is not parallel or sub parallel to layering. May be open or closed. The term 'fissure' may be used for irregular joints <0.2m in length	
e 3. Kev.z.	SHEARED ZONE	Zone in clayey soil with roughly parallel near planar, curved or undulating boundaries containing closely spaced, smooth or slickensided, curved intersecting joints which divide the mass into lenticular or wedge shaped blocks.	
FOILING, GEOS./. ISSUE 3. REV.Z	SHEARED SURFACE	A near planar curved or undulating, smooth, polished or slickensided surface in clayey soil. The polished or slickensided surface indicates that movement (in many cases very little) has occurred along the defect.	

TERM	DEFINITION	DIAGRAM
SOFTENED ZONE	A zone in clayey soil, usually adjacent to a defect in which the soil has a higher moisture content than elsewhere.	
TUBE	Tubular cavity. May occur singly or as one of a large number of separate or inter-connected tubes. Walls often coated with clay or strengthened by denser packing of grains. May contain organic matter.	
TUBE CAST	Roughly cylindrical elongated body of soil different from the soil mass in which it occurs. In some cases the soil which makes up the tube cast is cemented.	
INFILLED SEAM	Sheet or wall like body of soil substance or mass with roughly planer to irregular near parallel boundaries which cuts through a soil mass. Formed by infilling of open joints.	

Rock Description

Explanation Sheet

AS1726-1993 - The descriptive terms used by Coffey are given below. They are broadly consistent with Australian Standard AS1726-1993

DEFINITIONS:

Rock substance, defect and mass are defined as follows:

Defect Mass

Effectively homogeneous material, may be isotropic or anisotropic Discontinuity or break in the continuity of a substance or substances

Any body of material which is not effectively homogeneous. It can consist of two or more substances without defects, or one or

more substances with one or more defects.

In engineering terms rock substance is any naturally occurring aggregate of minerals and organic material which cannot be disintegrated or remoulded by hand in air or in water. Other material is described using soil descriptive terms.

SUBSTANCE DESCRIPTIVE TERMS:

ROCK NAME -Simple rock names are used rather than precise

geological classification

PARTICLE SIZE -Grain size terms for sandstone are:

Coarse grained Medium grained Fine grained

0.6mm to 2mm

0.2mm to 0.6mm

0.6mm (just visible) to 0.2mm

FARRIC -Terms for layering or penetrative fabric (eg.

bedding, cleavage) are:

No layering or penetrative fabric

Poorly developed Layering or fabric just visible. Little effect on

properties.

Layering or fabric distinct. Rock breaks more Well developed

easily parallel to layering or fabic

CLASSIFICATION OF WEATHERING PRODUCTS Abbreviation Definition

Residual Soil RS Soil derived from the weathering of rock; the mass structure and substance fabric

> are no longer evident; there is a large change in volume but the soil has not

been significantly transported.

XW Extremely Weathered

Material is weathered to such an extent that it has soil properties, ie, it either disintegrates or can be remoulded, in

water. Fabric of original rock still visible

Distinctly nw Weathered

Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching, or may be decreased due to deposition of

weathering products in pores

SW Slightly Weathered

Rock is slightly discoloured but shows little or no change of strength from fresh

Fresh FR Rock shows no sign of decomposition or

Note: Where physical and chemical changes were caused by hot gases and liquids associated with igneous rocks the terms slightly altered (SA), distinctly altered (DA) and extremely altered (XA) may be used.

ROCK SUBSTANCE STRENGTH TERMS

Term Abbreviation Point Load Index, I_S50 (MPa)

Field Guide to Strength

Very Low ٧L Less than 0.1 Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxial sample by

hand. Pieces up to 30mm thick can be broken by finger

pressure.

0.1 to 0.3

Easily scored with a knife; indentations 1mm to 3mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150mm long by 50mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.

Medium 0.3 to 1 Readily scored with a knife; a piece of core 150mm long by 50mm diameter can be broken by hand with difficulty.

1 to 3

A piece of core 150mm long by 50mm diameter can not be broken by hand but can be broken by a pick with a single firm blow; rock rings under

hammer

Very High VH 3 to 10

Hand specimen breaks with pick after more than one blow;

rock rings under hammer.

Extremely EH More than 10 High

Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

Notes:

Hiah

- In anisotropic rocks the field guide to strength applies to the strength perpendicular to the anisotropy. High strength anisotropic rocks may break readily parallel to the planar anisotropy.
- The term extremely low is not used as a rock substance strength term. The term is used in AS1726-1993 but the field guide to
- strength makes it clear that it is a soil in engineering terms. The unconfined compressive strength to isotropic rocks and anisotropic rocks which do not fail parallel to the planar anisotropy is typically 10 to 25 times the point load index. The ratio may vary for different rock types and lower strength rocks often have lower ratios than higher strength rocks.



Coffey



Rock Description Explanation Sheet

COMMON D	DEFECTS IN ROCK MASS	ES			ge	ological terms.
Term	Definition	Diagram	Мар	Graphic	DEFECT SH	IAPE TERMS
D. M	A	J	Symbol	Log (Note 1)	Planar	The defect does not vary in orientation
Parting	A surface or crack across which the rock has little or no tensile strength.				Curved	The defect has a gradual change in orientation
	Parallel or sub parallel to layering (eg bedding) or a planar anisotropy in the		20 Bedding		Undulating	The defect has a wavy surface
	rock substance (eg, cleavage). May be open		Cleavage	(Note 2)	Stepped	The defect has one or morwell defined steps
Joint	or closed. A surface or crack across				Irregular	The defect has many sharp changes in orientation
Joint	which the rock has little or no tensile strength but which is not parallel or sub parallel to layering or planar anisotropy in the rock substance. May be open or closed.		60	(Note 2)		nt of defect shape is partly the scale of observation.
Sheared	Zone of rock substance				ROUGHNES	S TERMS
Zone (Note 3)	with roughly parallel near planar, curved or undulating boundaries				Slickensided	Grooved or striated surface; usually polished
	cut by closely spaced	13.26			Polished	Shiny smooth surface
	joints, sheared surfaces or other defects. Some of the defects are usually		35		Smooth	Smooth to touch; few or no surface irregularities
	curved and intersect to divide the mass into lenticular or wedge shaped blocks.	,,		1,51	Rough	Many small surfaxce irregularities (amplitude generally less than 1mm); feels like fine to coarse sand paper
Sheared Surface Note 3)	A near planar, curved or undulating surface which is usually smooth, polished or slickensided.		40	3000	Very rough	Many large surface irregularities (amplitude generally more than 1mm); feels like, or coarser than, very coarse
Crushed Seam Note 3)	Seam with roughly parallel almost planar boundaries, composed of disoriented, usually angular fragments of the host rock substance which may be more weathered than the host		50		COATING T	sand paper
	rock. The seam has soil			17 1	Clean	No visible coating
	properties.				Stained	No visible coating but surfaces are discoloured
Infilled Seam	Seam of soil substance usually with distinct roughly parallel bounda-	_			Veneer	A visible coating of soil or mineral too thin to measure; may be patchy
	ries formed by the migration of soil into an open cavity or joint. Infilled seams less than 1mm thick may be described as veneer or coating on joint surface.		65		Coating	A visible coating up to 1mm thick. Thicker soil material is described using appropriate defect terms (eg, infilled seam). Thicke rock strength material is usually described as a vein
Extremely Weathered Seam	Seam of soil substance, often with gradational boundaries. Formed by weathering of the rock substance in places.		32 700000	DIA.	DI GOV OU	ADE TEDMS

Notes on defects:

Borehole logs show the true dip of defects and face sketches and sections the apparent dip.

substance in places.

- Partings and joints are not usually shown on the graphic log unless considered significant.
- Sheared zones, sheared surfaces and crushed seams are faults in

BLOCK SHAPE TERMS

Blocky Approximately equidimensional

Thickness much less than Tabular

length or width

Columnar Height much greater than cross section

Sheet

Checked by:

Engineering log - Excavation

UCCALPLAN PTY LTD

Office Job No.: CH1132/1

Date started: 8.12.2003

Principal:

Date completed: **8.12.2003**

1 of 1

Project: PROPOSED DEVELOPMENT NEAR HEARNS LAKE

Logged by: **AT**

Test pit location: Refer to Figure 1

Client:

equipment type and model: JCB 4CX Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetratic notes bo material structure and moisture condition samples support graphic additional observations water tests, etc kPa depth soil type: plasticity or particle characteristics, RL metres colour, secondary and minor components. 200 p 400 p 400 p TOPSOIL: Silty Clay, low to medium plasticity, dark St TOPSOIL CL brown, some coarse grained sand, some fine to RESIDUAL SOIL \coarse grained gravel and rootlets
Sandy Gravelly CLAY: low to medium plasticity, 0.<u>5</u> orange-brown, fine to coarse grained gravel, trace of CL Н cobble

Silty Gravelly CLAY: low to medium plasticity, pale grey, orange mottling, coarse gravel and some cobble of silt stone 1.<u>0</u> 1.<u>5</u> Highly weathered rock at 1.5 m. D М Test pit TP1 terminated at 2m 2.5 3.<u>0</u>

Sketch

Method
N natural exposure
X existing excavation
BH backhoe bucket
B bulldozer blade
R ripper
E excavator

support S shoring	N	nil
ra ra	n o resistar inging to ifusal	nce
water		
water le		

water inflow

water outflow

3.5

notes, sa	mples, tests
U ₅₀	undisturbed sample 50mm diameter
U ₆₃	undisturbed sample 63mm diameter
D	disturbed sample
V	vane shear (kPa)
Bs	bulk sample
E	environmental sample

refusal

2000	based on unified classification system											
mois	sture											
D	dry											
M	moist											
W	wet											
Wp	plastic limit											
W_L	liquid limit											

classification symbols and

soil description

	-	
	consiste	ncy/density index
	VS	very soft
	S	soft
	F	firm
_	St	stiff
	VSt	very stiff
	Н	hard
	Fb	friable
	VL	very loose

medium dense

very dense

dense

MD

VD

Coffey

1 of 1

Sheet

Office Job No.:

Engineering log - Excavation

CH1132/1 LOCALPLAN PTY LTD Date started: 8.12.2003

Client: Principal:

8.12.2003 Date completed:

Project:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE

ΑT Logged by:

Refer to Figure 1 Test pit location: Checked by:

quipment	type	and	model: J	ICB 4CX				Pit Orientation: Easting: r	n		R.L	. Surface: Not measi	ured
xcavation				2m long	0.5	m wid			n		dat	um: -	
_	ion	info	rmation		_	mate	erial s	ubstance					
Thetriod 7 benefication	support	water	notes samples, tests, etc	de RL met		graphic log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	100 pocket 200 d penetro- 300 w meter	structure an additional observ	
	N				-	31131	CH	TOPSOIL: Silty Clay, high plasticity, brown-black, organic rich	M	F		TOPSOIL	
			D D	1. 1. 2 2 3	.5 .5		СН	CLAY: high plasticity, grey, with tree roots and silty layers CLAY: high plasticity, blue-grey, with some gravel of silt stone Sandy CLAY: high plasticity, orange-brown, fine to coarse grained sand and some silt stone gravel, blue-grey mottling Test pit TP2 terminated at 3m		St	× × × · · · · · · · · · · · · · · · · ·	RESIDUAL SOIL	
				4	.0								

GEO 5.2 Issue 3 Rev.2	method N X BH B	natural exposure existing excavation backhoe bucket bulldozer blade	support S shoring N nil penetration 1 2 3 4	notes, s U ₅₀ U ₆₃ D	amples, tests undisturbed sample 50mm diameter undisturbed sample 63mm diameter disturbed sample vane shear (kPa)	classification symb soil description based on unified clas system		
	R	ripper excavator	water water level on date shown	Bs E R	valle shear (kra) bulk sample environmental sample refusal	mois D M W Wp	dry moist wet plastic limit	
E G			water inflow			, ···		

■ water outflow

classification symbols and	consiste	ency/density index
soil description	VS	very soft
based on unified classification	S	soft
system	F	firm
•	St	stiff
moisture	VSt	very stiff
D dry	Н	hard
M moist	Fb	friable
W wet	VL	very loose
Wp plastic limit	L	loose
W, liquid limit	MD	medium dense
	D	dense
	VD	very dense

TESTPIT CH1132-1.GPJ COFFEY.GDT 10.31.05

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Sheet

Office Job No.:

Engineering log - Excavation

Client:

LOCALPLAN PTY LTD Date started: 8.12.2003

Principal: Date completed: **8.12.2003**

Project: PROPOSED DEVELOPMENT NEAR HEARNS LAKE Logged by: AT

Refer to Figure 1 Test pit location: Checked by: JCB 4CX equipment type and model: Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetratic notes material graphic log structure and moisture condition samples support additional observations tests, etc depth RL metres kPa soil type: plasticity or particle characteristics, colour, secondary and minor components. 200 300 400 123 TOPSOIL: Clay, medium to high plasticity, black, TOPSOIL CH organic rich with rootlets

CLAY: high plasticity, grey/orange-brown ALLUVIAL SOIL 0.5 1.<u>0</u> Minor seepage. 1.<u>5</u> 2.0 CLAY: high plasticity, pale grey, with rootlets VSt 2.5 3.0 CLAY: high plasticity, orange-brown, with pockets Minor seepage of black clay and rootlets
Test pit TP3 terminated at 3.1m 3.5 Sketch

L						
Г	method	support	notes, samples, tests	classification symbols and	consisten	cy/density index
	N natural exposure X existing excavatio	S shoring N nil	U ₅₀ undisturbed sample 50mm diameter U ₆₂ undisturbed sample 63mm diameter	soil description based on unified classification	VS S	very soft soft
į	BH backhoe bucket B bulldozer blade	penetration	D disturbed sample V vane shear (kPa)	system	F	firm stiff
5	R ripper	no resistance ranging to	Bs bulk sample	moisture	St VSt	very stiff
200	E excavator	water	E environmental sample R refusal	D dry M moist	H Fb	hard friable
2		water level on date shown		W wet Wp plastic limit	VL L	very loose loose
		water inflow		W _∟ liquid limit	MD D	medium dense dense
Ŀ		─ water outflow			VD	very dense

TESTPIT CH1132-1.GPJ COFFEY.GDT 10.31.05

Engineering log - Excavation

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LOCALPLAN PTY LTD Client:

8.12.2003 Date started:

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Principal:

8.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Refer to Figure 1 Test pit location:

Checked by:

equip	ment	type	and	l model:	JCB 4	CX			Pit Orientation:	Easting:	m			R.L	Surface:	Not measured
excavation dimensions: 2m long 0						ng 0.5	5m wid	le		Northing:	m			dat	um:	-
excavation information							mat	erial s	ubstance							
	5 penetration	support	water	notes samples, tests, etc	RL ı	depth metres	graphic log	classification symbol	materia soil type: plasticity or partic colour, secondary and mi	cle characteristics, nor components.		moisture condition	consistency/ density index	100 x pocket 200 x penetro- 300 m meter		structure and tional observations
H8		N				1. <u>0</u>		CL CL CH	TOPSOIL: Clay, medium plast CLAY: medium plasticity, blac CLAY: medium to high plasticity grey/orange-brown, with rootless grey/orange-brown, grey/orange-brown, with rootless grey/orange-brown, grey/ora	ty,		M	H VSt	**	TOPSOIL ALLUVIAL	- SOIL -
			>	D	-	2.5 3.0 3.5 4.0		SP	SAND: fine to medium grained black organic smelling pockets Indurated below 2.8 m. Test pit TP4 terminated at 3.1n	l, red/brown, with		w	МЫ		Coffee roo	- k? -

method N X BH B natural exposure existing excavation backhoe bucket bulldozer blade ripper excavator

support S shoring water level on date shown

water inflow

water outflow

notes, samples, tests undisturbed sample 50mm diameter U₆₃ disturbed sample vane shear (kPa) Bs bulk sample

undisturbed sample 63mm diameter environmental sample refusal

classification symbols and soil description based on unified classification system moisture dry moist D М

wet

plastic limit

liquid limit

Wp

S F

VD

consistency/density index VS very soft soft firm St stiff VSt very stiff H Fb hard friable VLvery loose L MD medium dense dense

very dense

Coffey

Sheet

Office Job No.:

Engineering log - Excavation

CH1132/1 LOCALPLAN PTY LTD 8.12.2003 Date started:

Principal:

Client:

8.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Refer to Figure 1 Test pit location:

Checked by:

1 of 1

Test	pit lo	ocat	ion:	Refe	er to l	Figu	ire 1					(Checke	d by:			
equipr	equipment type and model: JCB 4CX								Pit Orientation: Easting: m					R.I	Surface:	rface: Not measured	
excav	excavation dimensions: 2m long 0.5m wide						īm wid	е		Northing:	m			da	ium:	-	
exca		ion	info	rmation			mat	erial s	ubstance								
method 1	ν penetration ε	support	water	notes samples, tests, etc	C RL m	depth etres	graphic log	classification symbol	materia soil type: plasticity or parti colour, secondary and m	icle characteristics, inor components.		moisture condition	consistency/ density index	100 x pocket 200 x penetro- 300 w meter	addi	structure and ional observa	
НВ		N	\	D D		1. <u>0</u> - 1. <u>5</u>		SP	CLAY: medium to high plastic rootlets Clayey SAND: fine to medium medium to high plasticity clay to sand the same organic odour SAND: fine to medium grained organic odour Indurated layer about 1.5 m. SAND: fine to medium grained layer at 2.0 - 2.	grained, pale grey, fines d, orange-brown, d, dark brown 15 m.	,	W	St MD D	*		ACK TOPSOIL SOIL	- - -
metho N X BH	1	natui existi back	ng ex hoe b	posure cavation ucket	supp S sh	3.5 4.0 4.0		nil	notes, samples, tests U ₅₀ undisturbed sample 50 U ₆₃ undisturbed sample 63 D disturbed sample V vane shear (RPa)	mm diameter soi mm diameter bas	il desc	ription	mbols a		VS S F	ency/density ind very soft soft firm stiff	ex
B R E	1	bulld rippe exca		olade	wate	er water le	evel eshowr)	V vane shear (kPa) Bs bulk sample E environmental sample R refusal	mo D M W Wp W _L		ist			St VSt H Fb VL L MD D	stiff very stiff hard friable very loose loose medium de dense very dense	ense

Sheet

Office Job No.:

Engineering log - Excavation

LOCALPLAN PTY LTD 8.12.2003 Date started:

Client: Principal:

8.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Refer to Figure 1 Test pit location:

Checked by:

1 of 1

CH1132/1

equipment type and model: JCB 4CX Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetratic notes bo material structure and moisture condition samples support graphic additional observations water tests, etc kPa depth soil type: plasticity or particle characteristics, RL metres 100 200 400 400 colour, secondary and minor components. TOPSOIL: Silty Clay, medium to high plasticity, VSt TOPSOIL ALLUVIAL SOIL 표 \dark brown, with rootlets

CLAY: medium to high plasticity, grey, with orange mottling, tiny pockets of fine pale grey sand 0.5 1.<u>0</u> **CLAY:** medium to high plasticity, pale grey/orange, occassional orange silt stone gravel Н 1.<u>5</u> 2.0 2.5 Pocket of sandy clay. 3.0 Test pit TP6 terminated at 3m 3.5 Sketch

method natural exposure X BH existing excavation backhoe bucket В bulldozer blade R ripper excavator

support S shoring water level

water inflow

water outflow

notes, samples, tests undisturbed sample 50mm diameter U₆₃ undisturbed sample 63mm diameter D disturbed sample vane shear (kPa) Bs E R

environmental sample refusal

classification symbols and soil description based on unified classification system moisture D dry

M moist wet Wp plastic limit W, liquid limit

consister	ncy/density inde
VS	very soft
S	soft
F	firm
St	stiff
VSt	very stiff
Н	hard
Fb	friable
VL	very loose

medium dense

very dense

dense

MD

VD

D

Engineering log - Excavation

Sheet 1 of 1 Office Job No.:

LOCALPLAN PTY LTD Client:

CH1132/1 8.12.2003 Date started:

Principal:

8.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Refer to Figure 1 Test pit location:

Checked by:

equi	pment	type	and	model:	JCB 4	ICX	Pit Orientation: Easting: m R.L. Surface: Not measured					ured						
excavation dimensions: 2m long 0.5m wide Northing: m datum:							um:	-										
ex	cavat	ion	info	rmation			mat	erial s	ubstance									
method	5 penetration	support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particl colour, secondary and min			moisture condition	consistency/ density index	100 pocket 200 pocket	a		structure an	
НВ		N				0.5 1.0 1.5 2.0		CH CH	TOPSOIL: Silty Clay, medium to dark brown Silty CLAY: medium to high pla mottled red CLAY: medium to high plasticity trace of orange silt stone gravel	sticity, brown,	ge,	М	VSt H	;	**	TOPSOIL ALLUVIAL	SOIL	- - -
			-			2. <u>5</u> - - - 3. <u>0</u>		SP SP	Clayey SAND: fine to medium g with medium to high plasticity fin SAND: fine to medium grained,	nes	′,	W	D					-
						3. <u>5</u>			Test pit TP7 terminated at 3.3m									
						4.0												
S	ketch																	

٦					
	method N natural exposure X existing excavation	support S shoring N nil	$\begin{array}{ll} \text{notes, samples, tests} \\ \text{U_{S0}} & \text{undisturbed sample 50mm diameter} \\ \text{U_{E3}} & \text{undisturbed sample 63mm diameter} \end{array}$	classification symbols and soil description based on unified classification	consistency/density index VS very soft S soft
e o Rev.z	BH backhoe bucket B bulldozer blade R ripper	penetration 1 2 3 4 no resistance ranging to	D disturbed sample V vane shear (kPa) Bs bulk sample	system moisture	F firm St stiff VSt very stiff
EU 0.4 Ibou	E excavator	water water level on date shown	E environmental sample R refusal	D dry M moist W wet Wp plastic limit W, liquid limit	H hard Fb friable VL very loose L loose MD medium dense
פ		water inflow water outflow		W∟ liquid limit	D dense VD very dense

TESTPIT CH1132-1.GPJ COFFEY.GDT 10.31.05

Engineering log - Excavation

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LOCALPLAN PTY LTD Client:

8.12.2003 Date started:

1 of 1

Principal:

8.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Refer to Figure 1 Test pit location:

Checked by:

equipme	ent ty	ре	and	model: J	ICB 4	CX			Pit Orientation:	Easting:	m			R.	L. Surface:	Not measured	
excavation dimensions: 2m long 0.5					2m lor	ng 0.5	5m wic	le		Northing:	m			da	tum:	-	
excavation information							mat	erial s	ubstance								
method 1 5 penetration		support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	material soil type: plasticity or particle colour, secondary and mino			moisture condition	consistency/ density index	100 pocket 200 penetro- 300 meter		structure and tional observations	i
Н		7		D D		1.0 1.5 2.0 3.0 3.5		CH CH	TOPSOIL: Sandy Clay, medium dark brown, fine grained sand and Silty CLAY: medium to high plas orange-brown Sandy CLAY: medium to high plas fine to medium grained sand SAND: fine to medium grained, be organic odour, some indurated lateral to the same same same same same same same sam	d rootlets ticity, asticity, pale gre		M	VSt	*			
Sketo	ch																

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method	
N	natural exposure
X	existing excavation
BH	backhoe bucket
В	bulldozer blade
R	ripper
E	excavator

support		
S shoring	N nil	
penetration		
1 2 3 4	resistance	
	ging to	
refu		
water		
water lev	el	
on date s	shown	

water inflow water outflow

notes	, samples, tests
U_{50}	undisturbed sample 50mm diameter
U_{63}	undisturbed sample 63mm diameter
D	disturbed sample
V	vane shear (kPa)
Bs	bulk sample
E	environmental sample
R	refusal

soil	sification symbols and description ed on unified classification em	
moi	sture	
D	dry	
M	moist	
W	wet	

plastic limit liquid limit

consist	ency/density ind
VS	very soft
S	soft
F	firm
St	stiff
VSt	very stiff
Н	hard
Fb	friable
VL	very loose
L	loose

v O	very soit
S	soft
F	firm
St	stiff
√St	very stiff
Н	hard
Fb	friable
٧L	very loose
L	loose
MD	medium dense
D	dense
VD	very dense

1 of 1

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Office Job No.:

Engineering log - Excavation

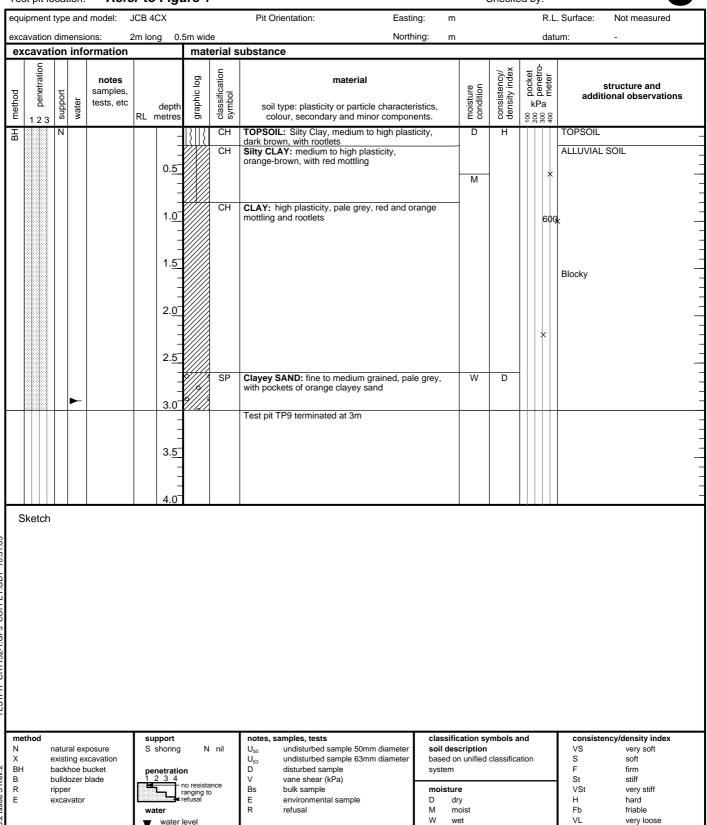
Client:

LOCALPLAN PTY LTD 8.12.2003 Date started:

8.12.2003 Principal: Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE ΑT Project: Logged by:

Refer to Figure 1 Test pit location: Checked by:



Wp

W,

plastic limit

liquid limit

MD

VD

medium dense

very dense

dense

CH1132-1.GPJ COFFEY.GDT 10.31.05 **TESTPIT**

water inflow

water outflow

1 of 1

Sheet

Engineering log - Excavation

Office Job No.: CH1132/1

Client:LOCALPLAN PTY LTDDate started:8.12.2003Principal:Date completed:8.12.2003

Project: PROPOSED DEVELOPMENT NEAR HEARNS LAKE Logged by: AT

Test pit location: Refer to Figure 1 Checked by:

JCB 4CX equipment type and model: Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetratic notes material graphic log structure and moisture condition samples method support additional observations water tests, etc depth RL metres kPa soil type: plasticity or particle characteristics, 200 300 400 colour, secondary and minor components. TOPSOIL: medium to high plasticity, dark brown, St TOPSOIL 표 fine grained sand and rootlets Clayey SAND: fine to medium grained, orange-brown, medium to high plasticity clay AEOLIAN/ALLUVIAL SOIL MD 0.5 1.<u>0</u> SAND: fine to medium grained, white W 1.<u>5</u> 2.0 Clayey SAND: fine to medium grained, 2.5 СН Sandy CLAY: medium to high plasticity, dark brown, fine grained sand SAND: fine to medium grained, orange/yellow/grey SP 3.<u>0</u> 3.5 Test pit TP10 terminated at 3.5m

C	V.	٠.	٦ŀ	
	ĸе	-10		ı

TESTPIT CH1132-1.GPJ COFFEY.GDT 10.31.05

	method		support	notes, samples, tests		clas	sification symbols and	consistency/density index		
	N	natural exposure	S shoring N nil	U ₅₀	undisturbed sample 50mm diameter	soil	description	VS	very soft	
	X	existing excavation		U ₆₃	undisturbed sample 63mm diameter	base	ed on unified classification	S	soft	
7.7	BH	backhoe bucket	penetration	D	disturbed sample	syste	em	F	firm	
è.	В	bulldozer blade	1 2 3 4	V	vane shear (kPa)			St	stiff	
က	R	ripper	ranging to	Bs	bulk sample	moi	sture	VSt	very stiff	
ene	E	excavator	refusal	Е	environmental sample	D	dry	Н	hard	
<u>88</u>			water	R	refusal	M	moist	Fb	friable	
5.2			water level			W	wet	VL	very loose	
0			on date shown			Wp	plastic limit	L	loose	
GEO						WL	liquid limit	MD	medium dense	
٤			water inflow					D	dense	
Pol			water outflow					VD	very dense	

1 of 1

CH1132/1

Sheet

Office Job No.:

Engineering log - Excavation

Client:

LOCALPLAN PTY LTD 8.12.2003 Date started:

8.12.2003 Principal: Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE ΑT Project: Logged by:

Refer to Figure 1 Test pit location: Checked by: JCB 4CX equipment type and model: Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetratic material notes bo structure and moisture condition samples support graphic additional observations tests, etc kPa depth soil type: plasticity or particle characteristics, RL metres colour, secondary and minor components. 200 p 400 p 400 p TOPSOIL: Sandy Clay, medium to high plasticity, St TOPSOIL 표 dark brown, with fine grained sand and rootlets SAND: fine to medium grained, orange-brown, with MD AEOLIAN/ALLUVIAL SOIL 0.5 some clay fines SAND: fine to medium grained, white AEOLIAN/ALLUVIAL SOIL 1.0 1.<u>5</u> 2.0 W SAND: fine to medium grained, grey Seepage at 2.3m. 2.5 SP SAND: fine to medium grained, brown/black 3.0 Test pit TP11 terminated at 3m

Sketch

method X BH В

natural exposure existing excavation backhoe bucket bulldozer blade ripper excavator

support S shoring water level

water inflow

water outflow

3.5

notes, samples, tests undisturbed sample 50mm diameter U₆₃ undisturbed sample 63mm diamete D disturbed sample vane shear (kPa) Bs

environmental sample refusal

classification symbols and soil description based on unified classification system moisture D dry M moist

wet

plastic limit

liquid limit

Wp

consistency/density index ٧S St Fb

very soft soft firm stiff VSt very stiff hard friable VL very loose MD medium dense dense VD very dense

R

1 of 1

CH1132/1

8.12.2003

Engineering log - Excavation

Client:

LOCALPLAN PTY LTD 8.12.2003 Date started:

Principal:

ΑT Logged by:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

Office Job No.:

Sheet

Checked by:

Date completed:

Refer to Figure 1 Test pit location: equipment type and model: JCB 4CX Pit Orientation: Easting: R.L. Surface: Not measured excavation dimensions: 2m long 0.5m wide Northing: m datum: excavation information material substance pocket penetro-meter consistency/ density index classification symbol penetration material notes bo structure and samples support graphic additional observations water tests, etc kPa depth soil type: plasticity or particle characteristics, RL metres colour, secondary and minor components. 200 p 400 p 400 p **TOPSOIL:** Gravelly Sandy Clay, medium to high plasticity, brown, fine to coarse grained sand, fine to $\overline{1}$ St MD 표 TOPSOIL AEOLIAN SOIL medium grained gravel

SAND: medium grained, grey, with a trace of clay 0.5 SP L \fines
SAND: fine to medium grained, yellow-white 1.0 SAND: fine grained, black/red-brown, with some D clay fines, indurated at top 1.<u>5</u> 2.0 2.5 SAND: fine to medium grained, grey/brown/black, W with some clay fines 3.0 Test pit TP12 terminated at 3.1m 3.5

Sketch

method natural exposure X BH existing excavation backhoe bucket В bulldozer blade R ripper excavator

support S shoring water level

water inflow

water outflow

notes, samples, tests undisturbed sample 50mm diameter U₆₃ undisturbed sample 63mm diameter D disturbed sample vane shear (kPa) Bs bulk sample Ε environmental sample

refusal

classification symbols and soil description based on unified classification system moisture D dry M moist wet plastic limit Wp

liquid limit

consistency/density index ٧S very soft S soft firm St stiff VSt very stiff н hard Fb friable VL very loose

medium dense

very dense

dense

MD

VD

Borehole No. **GW1**

Engineering Log - Borehole

Sheet 1 of 1

Client: LOCALPLAN PTY LTD

Office Job No.: **CH1132/1**Date started: **8.12.2003**

Principal:

Date completed: **8.12.2003**

Project: PROPOSED DEVELOPMENT NEAR HEARNS LAKE

Logged by: AT

Borehole Location: Refer to Figure 1

Checked by:

drill	Irill model and mounting: MD200 4WD		Easting: slope: -90°			R.L. Surface: Not measured												
_	e diam				100 m	ım			· ·			dat	um:	-				
dr	illing	info	orma	ation	ı		mat	material substance										
method	5 penetration	support	water	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol	soil type: plasticity	material or particle character y and minor compone		moisture condition	consistency/ density index	100 200 3 pocket	Pa		structure an ional observ	
ADV		N				1 2		SP SP	SAND: fine to medium silt fines SAND: fine to medium fines	grained, pale yellow,	trace of	M D				ALLUVIAL	SOIL	- - - - - - - -
			19.12.03 / 1500			3 3 - - 4		SC	Clayey SAND: fine to rhigh plasticity fines			W						- - - - - -
BOKEHOLE CHITISZ-1.GFJ COFFEY.GDJ 10.31.05						5 6			Borehole GW1 termina	ited at 4m	чериі.							- - - - - - - - - -
mer AS AD RRM 2 Kev.7 AD RR W CT AT AT A DT B V T	shown	ai w ca ha di bl V Ti by su	uger of aller/tri ashbo able to and au atube ank b bit C bit	ore ool uger	M C pe 1	nter 10/1/9	on no resista ranging to refusal 8 water e shown	level	U ₆₃ undisturbed sam D disturbed sam	tration test (SPT) recovered cone Pa)	soil des based of system moistur D d M m W w Wp p	cation sy scription on unified re lry noist yet lastic limit quid limit	classifica			consiste VS S F St VSt H Fb VL L MD D VD	ency/density in very sof soft firm stiff very stiff hard friable very loo loose medium dense very der	se dense

Coffey *******

Borehole No. GW₂

Sheet 1 of 1

CH1132/1 Office Job No.:

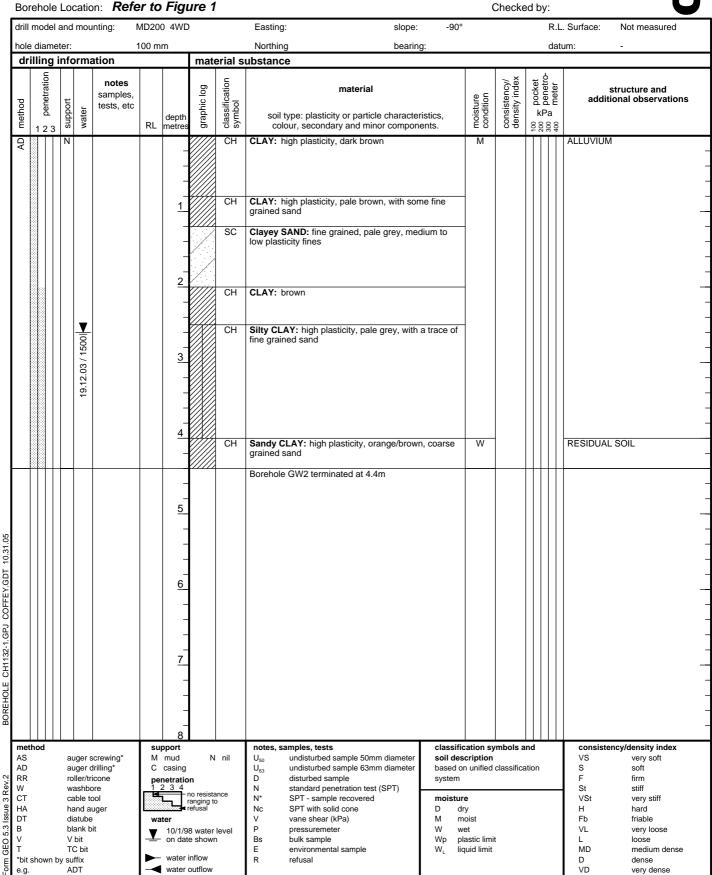
LOCALPLAN PTY LTD 19.12.2003 Client: Date started:

19.12.2003 Principal: Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE ΑT Project: Logged by:

Borehole Location: Refer to Figure 1

Engineering Log - Borehole





Borehole No. GW2A

Sheet 1 of 1

CH1132/1 Office Job No.:

LOCALPLAN PTY LTD 19.12.2003 Date started:

19.12.2003 Principal: Date completed:

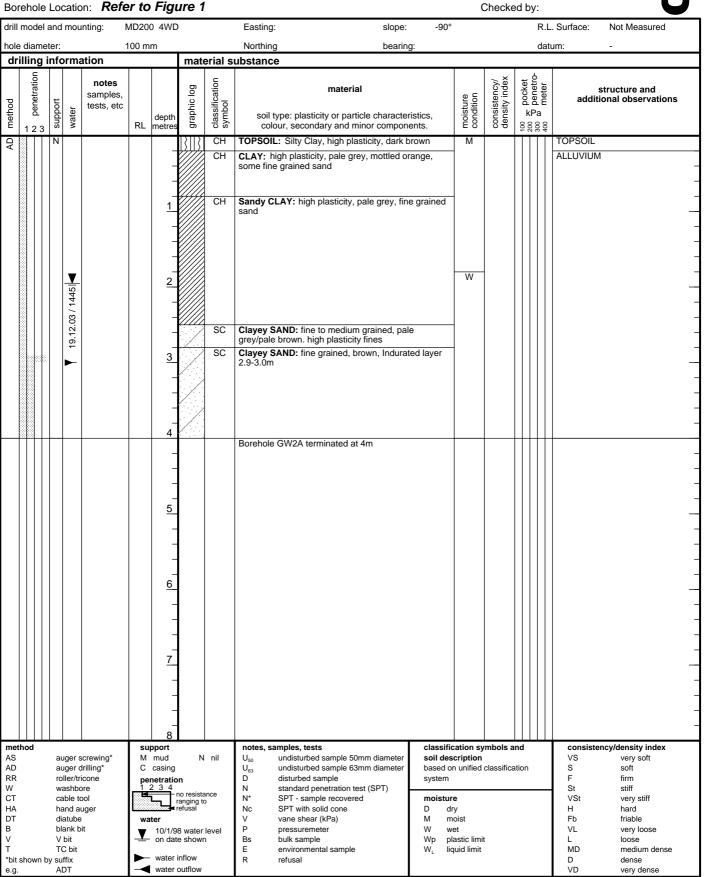
PROPOSED DEVELOPMENT NEAR HEARNS LAKE ΑT Project: Logged by:

Borehole Location: Refer to Figure 1

Engineering Log - Borehole

COFFEY.GDT

CH1132-1.GPJ



Borehole No. GW3

Engineering Log - Borehole

1 of 1 Office Job No.:

Sheet

Date started:

LOCALPLAN PTY LTD Client:

CH1132/1 19.12.2003

Principal:

19.12.2003 Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE Project:

ΑT Logged by:

Borehole Location: Refer to Figure 1

Checked by:

drill model and mounting: MD200 4WD Easting: slope: -90° R.L. Surface: Not Measured					
hole diameter: 1 drilling information					
poddns samples, tests, etc	transmitted that the same of t	material soil type: plasticity or particle characte colour, secondary and minor compon	ristics, ents.	consistency/ density index 100 pocket 200 penetro- 300 meter	structure and additional observations
AD Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	SC 2 SC 2 3 4	Sandy CLAY: high plasticity, pale yellow-brine grained sand Clayey SAND: fine grained, pale grey, high plasticity fines Clayey SAND: fine grained, brown, high plasticity fines Clayey SAND: fine grained, brown, high plasticity fines	rown, M		ALLUVIUM
method AS auger screwing* AR auger drilling* RR roller/tricone W washbore CT cable tool HA hand auger DT diatube B blank bit V V V bit T TC bit *bit shown by suffix e.g. ADT	support M mud N nil C casing penetration 1 2 3 4 no resistance ranging to refusal water 10/1/98 water level on date shown water inflow	notes, samples, tests U _{so} undisturbed sample 50mm diameter U _{sis} undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone V vane shear (kPa) P pressuremeter Bs bulk sample E environmental sample R refusal	classification sy soil description based on unified system moisture D dry M moist W wet Wp plastic limi W_ liquid limit	classification	consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense

Borehole No. GW4

Sheet 1 of 1

CH1132/1 Office Job No.:

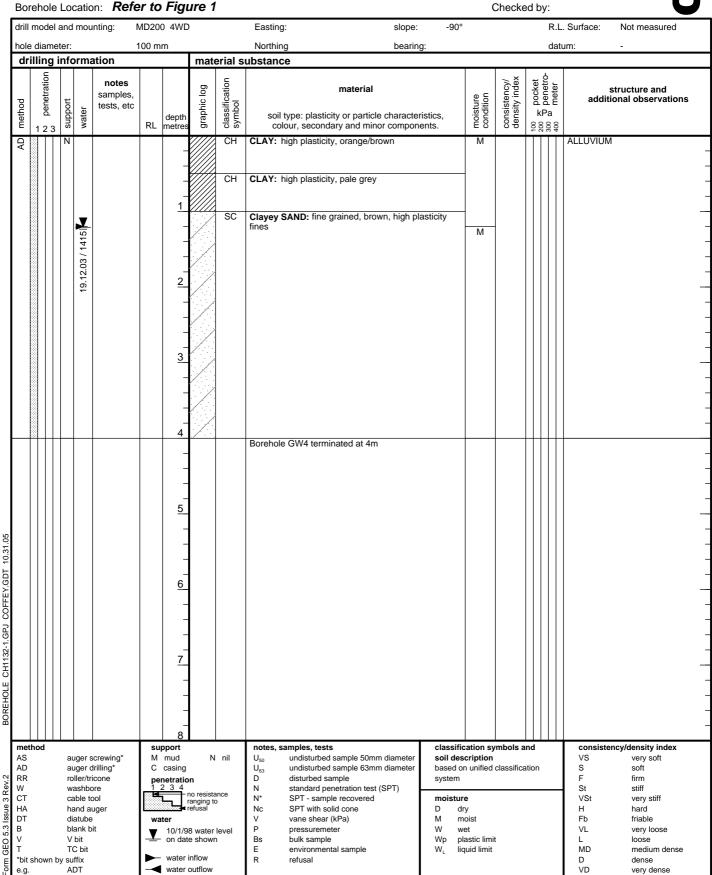
LOCALPLAN PTY LTD 19.12.2003 Date started:

19.12.2003 Principal: Date completed:

PROPOSED DEVELOPMENT NEAR HEARNS LAKE ΑT Project: Logged by:

Borehole Location: Refer to Figure 1

Engineering Log - Borehole





APPENDIX B

LABORATORY TEST RESULTS



CH1132/1 LOCALPLAN PTY LTD PROPOSED DEVELOPMENT HEARNS LAKE SANDY BEACH

TABLE 1 - RESULTS OF ACID SULFATE SOIL SCREENING TESTS

Location	Depth (m)	pH in Distilled Water	pH in Hydrogen Peroxide
TP2	0.5	6.6	6.7
TP2	1.0	6.5	5.4
TP2	2.0	6.7	5.2
TP5	0.2	7.0	3.9
TP5	0.7	6.8	3.4
TP5	2.0	6.5	3.2
TP8	0.5	5.6	4.7
TP8	1.0	6.2	6.4
TP8	2.5	5.7	6.3
TP11	1.0	5.1	6.3
TP11	2.3	5.3	6.2
TP11	2.7	5.2	3.2

DETERMINATION OF ACID SULFATE SOIL PROPERTIES

CERTIFICATE OF ANALYSIS



781 Mt. Glorious Road Highvale, Brisbane, Australia, 4520 Ph.

Analysis By: Bio-Track Pty Ltd ABN 91 056 237 275

Page 1 of 1 Report Pages. C/O COFFEY GEOSCIENCES PTY LTD 29 JANUARY 2004 MR DAVID PARKER C/O COFFEY GEOSC PO BOX 704 COFFS HARBOUR NSW 2450 CH1132/1

CLIENT ADDRESS OF REPORT

SAMPLING DATE DATE RECEIVED

PACKAGING

PROJECT NAME

NUMBER OF SAMPLES 4 SAMPLE TYPE:SOIL SAMPLE FOR ACID SULFATE STUDY
ABELLED - INTACT - BAGGED - CHILLED IN INSULATED PACKAGING ** SAMPLES DISPOSED ON 1/7/2004
7 2004 LAB REF. LR1814.117 YOUR PROJECT/JOB REFERENCE CH1132/1 SAMPLES LABELLED 18 JANUARY 2004

METHODOLOGY: As per

10LOGY: As per SPOCAS (DNR QASSIT June 2003) for <850 um fraction, S,Ca & Mg by ICP; CLAY (H) for >40% clay or (L) for <5% clay (approximate estimation only)
LIME1 rates calculated to neutralise TPA (or TAA if >TPA), LIME2 rates calculated from TAA+aS POS- carbonate buffer (aCa A + aMg A)/fineness factor (1.51.5).
NB. Lime rates assume 97% lime neutralisation and Bulk Density = 1.6 cbut DO NOT include any safety factors. Suggested factor=1.5-1.8.
Equivalent Sulphur (%S eq)= sTAA (%S) + S POS (%S) where sTAA (%S)=TAA/624. [Reported as oven dry (85'C) mass]
Carbonate POS = moles carbonate alkalinity released by oxidation assuming (Ca POS - Ca KCl) + (Mg POS - Mg KCl) is due to carbonate solution. This buffers TPA. Carbonate POS 1 1 2 2 2 2 Mg KCL Mg/kg 365 150 175 175 Ca P mg/kg 230 235 345 Ca KCL 189/kg 160 220 300 95 % % 0.02 0.16 0.06 LIME2 kg/m³ 0.5 8.1 2.9 2.9 kg/m3 0.5 18.5 3.5 0.7 POS ACID の死处の x x x x 0.01 0.12 0.05 0.05 S P 0.02 0.04 0.06 % KCL 0.01 0.01 0.01 0.01 7SA 7 7 0 203 40 5 \$\$~2×m SKIFT 0.5 0.0 -0.3 5.53 5.53 5.63 5.63 ቜጷ 5.37 4.49 5.63 5.78 포苡 2555 COARSE CCARCE 0.2 FINE 0.7 COMPS DEPTH 2.0

For and behalf of Bio-Track Pty Ltd

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<u>:</u>