



**PAD 4 STORMWATER
CONCEPT PLAN
EASTERN LANDS ERSKINE PARK**

JULY 2006
Report No. W03033.12-06C
Prepared for CSR Limited



BROWN CONSULTING
Engineers & Managers

PEOPLE & PROJECTS



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PAD 4 STORMWATER CONCEPT PLAN
EASTERN LANDS, ERSKINE PARK

FOR CSR LIMITED

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LIST OF ABBREVIATIONS

AEP	Annual Exceedance Probability
AHD	Australian Height Datum
ARI	Average Recurrence Interval
ARR	Australian Rainfall and Runoff
DIPNR	Department of Infrastructure, Planning and Natural Resources
DLWC	Department of Land and Water Conservation NSW
DNR	Department of Natural Resources
DEM	Digital Elevation Model
DTM	Digital Terrain Model
FPDM	Floodplain Development Manual
FPL	Flood Planning Level
FPMM	Floodplain Management Manual
FPRMS	Floodplain Risk Management Study
FSL	Flood Surface Level
GIS	Geographic Information System
ha	Hectare (Area = 10,000m ²)
LEP	Local Environmental Plan
LGA	Local Government Area
MGA	Map Grid Australia
m ³ /s	Cubic meters per second
PMF	Probable Maximum Flood
PMP	Probable Maximum Precipitation
RCP	Reinforced Concrete Pipe
RCBC	Reinforced Concrete Box Culvert
RTA	Roads and Traffic Authority of NSW
SEPP	State Environmental Planning Policy
SMP	Stormwater Management Plan
TIN	Triangular Irregular Network



PAD 4 STORMWATER CONCEPT PLAN

EASTERN LANDS

ERSKINE PARK

FOR CSR LIMITED

1 INTRODUCTION

Brown Consulting has been commissioned to develop a stormwater concept plan for a proposed industrial development on CSR's property located within the Erskine Park Employment Area, see **Figure 1.1**. This concept plan covers stormwater quality and quantity management issues to support the project application for the earthworks, subdivision and associated infrastructure works to create a building pad, followed by the construction of a warehouse, car parks and truck parking areas forming the industrial development on Building Pad 4.

This report should be read in conjunction with the following reports:

- Brown Consulting (2006). *South Eastern Creek Realignment – Hydrology and Hydraulics*, CSR Eastern Lands Erskine Park, for CSR Limited. (Report N^o. W03033.12-05B)
- Brown Consulting (2006). *Stormwater Concept Plan, Eastern Lands Erskine Park*, for CSR Limited. (Report N^o. W03033.12-04B)

These reports have been submitted with the project application.

1.1 OBJECTIVES

The Stormwater Masterplan for the development has considered the objectives of the Development Control Plan for the Erskine Park Employment Area. To meet the objectives of the DCP, this report:

- Describes the operation of the stormwater management for Pad 4.

- Provides a concept sizing for an on-site detention (OSD) system to reduce the developed peak flows off the proposed development site at Pad 4 to ensure no increase in the flows downstream of the development.
- Provides a conceptual stormwater management system that will reduce the post-developed pollutant loads to meet the requirements of the DCP for the area.
- Describes the management of major and minor overland flows from the development.
- Provides a concept sediment and erosion control plan for the bulk earthworks.

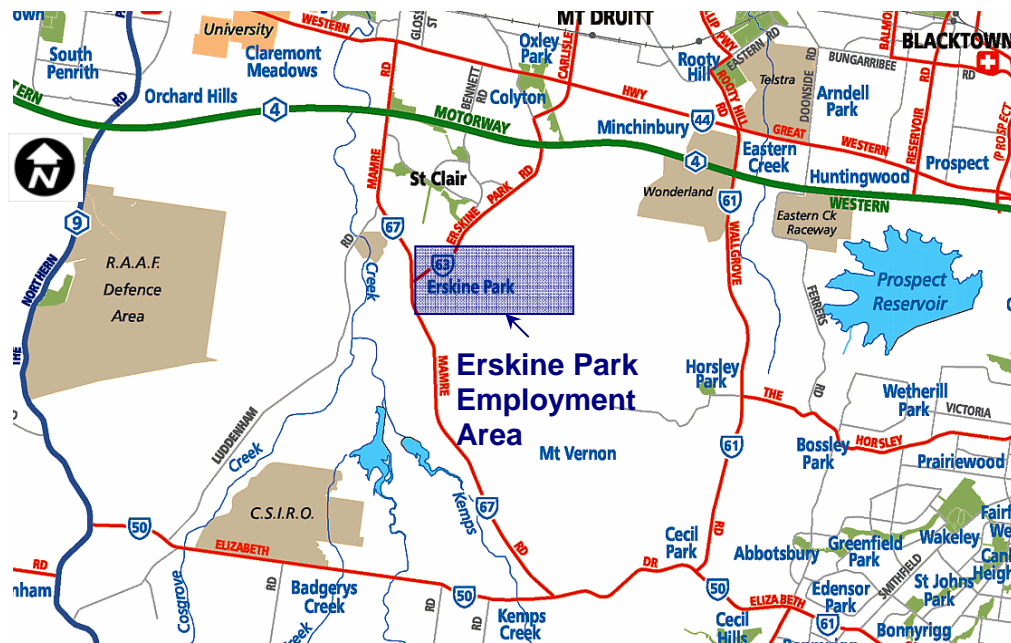


Figure 1.1 Locality Plan (Source: UBD 2004)

1.2 DESCRIPTION OF STUDY AREA

The land to which the applications relate is located off Lenore Lane at Erskine Park, within the Penrith City Council local government area. The land is described as Pad 4 in proposed Lot 23, see **Appendix A** for lot plan. Pad 4 is located in the western half of proposed Lot 23.

The development area on Pad 4 will occupy an area of approximately 8.65 Ha. The associated creekworks spread onto the adjoining Crown road reserve to the south of the site (refer to report *South Eastern Creek Realignment* (Brown Consulting 2006)).

1.3 PREVIOUS STUDIES

The following studies have been undertaken for the site and adjoining properties. These studies have been reviewed as part of the preparation of this Plan.

- Boyden & Partners (1999). *Review of Stormwater Drainage & Water Management Systems Erskine Park Employment Area*, for Penrith City Council.
- Robinson GRC Consulting (2001). *Erskine Park Industrial Subdivision Drainage Requirements*, for CSR Limited.
- Buckton Lysenko (2002). *Stormwater Management Plan Comprising Creek Realignment Proposal for the Stramit Warehouse and Office Development at Corner Erskine Park Road and Mamre Road, Erskine Park*, for McRoss Developments Pty Ltd.
- Buckton Lysenko (2003). *Flood Study for Watercourse "A" for Industrial Development at Corner Erskine Park Road and Mamre Road, Erskine Park Incorporating Bridge Structure*, for Walker Corporation.
- WP Brown & Partners (2004). *Stormwater Masterplan*, for CSR Limited.
- Brown Consulting (2004). *Concept Stormwater Management Plan, Proposed Industrial Development Lot 93 Lenore Lane, Erskine Park*, for CSR Limited.
- Brown Consulting (2005). *Concept Stormwater Management Plan, Proposed Warehouse and Distribution Facility, Erskine Park*, for Walker Corporation.
- Brown Consulting (2005). *Stormwater Concept Plan, Proposed Woolworths Distribution Centre, CSR Lands Erskine Park*, for Australand.
- Brown Consulting (2006). *Stormwater Concept Plan, Eastern Lands Erskine Park*, for CSR Limited. (Report No. W03033.12-04B)

2 MANAGEMENT OF MINOR AND MAJOR FLOWS

The concept stormwater management plan for Pad 4 is shown in the drawings in **Appendix A**. The site has been divided into 7 main sub-catchments and the management of the discharges varies between sub-catchments. The sub-catchments generally refer to the proposed building roof area and to the drainage of the car and truck parking areas, which have been kept separate.

Council's DCP for the area allows for the water collected from the roof to be discharged from the site to the creeks without treatment. Flows from the developed site do need to be attenuated however to ensure post-developed flows do not exceed pre-developed flows. As such, roof runoff will be directed to the on-site detention tank, whilst all other runoff will be directed first to a water quality improvement device (such as an infiltration basin or bio-filtration swale), then to the detention tank or direct to the western swale.

The runoff from the site will be discharged to the swale to the west of the site, which itself discharges to the creek system at the southern boundary of the site. The peak flow discharged from the site does not exceed the existing rate from the site as detailed in **Section 3**.

2.1 MINOR FLOW MANAGEMENT

Runoff from the Pad 4 development area for storms up to the 20 year ARI will be collected by the following systems:

- For the truck parking/ manoeuvring areas, and the overflow car park area, a combination pit and pipe system discharging to the bio-retention basin;
- For the car parking areas to the east of the warehouse, a combination pit and pipe system discharging initially to two bio-filtration swales within the car park area, then to the OSD tank beneath the overflow car park;
- The roof water will be directed to the OSD tank at the south-western corner of the site.

The runoff from the site will be discharged to the swale to the west of the site, which itself discharges to the creek system at the southern boundary of the site.

Details of the proposed drainage system are shown in **Appendix A**.

2.2 MAJOR FLOW MANAGEMENT

Major flows are considered those flows in excess of the 20 year ARI peak flow. Such flows from the truck parking and manoeuvring areas will be directed by pipe and overland to the western corner of the truck area. A sag point at this corner will allow water to pond and enter the pipe system before being conveyed to the bio-retention basin, where detention is provided to help reduce the total site peak flows to pre-development levels, and where water quality improvement occurs.

Major flows from the car parking areas to the east of the warehouse will be directed by pipe and overland using the internal access-way along the southern boundary to the OSD tank, where detention is provided to reduce the peak flows to pre-development levels. The potential exists for these overland flows in the largest events to also be directed to the bio-retention basin. Major flows from the overflow car park area would similarly be directed to the bio-retention basin that lies adjacent to it, and could also be directed to the underlying OSD tank in the largest events. Both the tank and basin will attenuate flows from the site.

Stormwater flows from the roof areas will be directed to the OSD tank in the south-west corner of the site. The downpipes and drainage network for this system will need to be sized to convey the 100 year ARI flows to the tank.

It is proposed to provide a reconstructed creek system for the part of the overall development site (pads 4, 5 and 7 and the road drainage) draining to the southern boundary of the site. This is covered in detail in the report *South Eastern Creek Realignment, Erskine Park* by Brown Consulting.

3 CONCEPT OSD SYSTEM DESIGN

3.1 PRE-DEVELOPED FLOWS

The pre-developed site flows for Pad 4 have been determined using the *DRAINS* computer package with RAFTS type hydrology. These flows were established to enable comparison between existing and developed site flows.

Table 3.1 below summarises the pre-development catchment characteristics adopted to determine these flows.

Table 3.1 Pre-Development Catchment Characteristics

Variable	Pad 4
Area (ha)	7.76
Slope (%)	1.9
% Imp	5
Manning 'n'	0.035

Table 3.2 below summarises the peak flows from Pad 4 for the pre-development scenario.

Table 3.2 Pre-Development Peak Flows

ARI (Years)	Flow (m³/s)
5	0.84
20	1.24
100	1.89

3.2 POST-DEVELOPED FLOWS

For the post-developed scenario the same pad area adopted for the pre-developed flows was adopted, however the fraction impervious was increased to 90% impervious as per Table 4 of the "Penrith City Council Guidelines for Engineering Works for Subdivision and Developments." The slope was also reduced to 1% as this is the estimated finished grade on all pipes and surfaces for the post-development scenario, and the roughness was reduced to 0.015.

Table 3.3 below summarises the peak flow of the site for the post-developed scenario. The results of the *DRAINS* run have been attached in **Appendix C**.

Table 3.3 Post-Development Peak Flows

ARI (Years)	Flow (m³/s)
5	2.62
20	3.48
100	4.32

As the post-development peak flows exceed the pre-developed flows, On-Site Stormwater Detention will need to be provided.

3.3 POST-DEVELOPED FLOWS WITH OSD SYSTEM

All runoff from non-roof areas will be directed to a water quality device before being discharged from the site. The truck parking and overflow car park areas will drain to the bio-retention basin in the south-west of the site, whilst the other car park areas will drain to central bio-filtration swales then to the OSD tank. The bio-retention basin will store small storm volumes (up to 1 year ARI), with the stored water passing through a bio-filtration medium before being released to the drainage swale to the west of the site. Any flows in excess of the volume of this water quality basin will pass through a high level overflow pipe into Swale 2 to the west of the site.

All roof area runoff will be conveyed directly to the OSD tank. This OSD tank will be equipped with a high early discharge chamber, and both the tank and the bio-retention basin will form the OSD for the site.

The proposed OSD has been designed to limit the post-developed flows to the pre-development flows summarised in **Table 3.2**. This design was undertaken in the *DRAINS* program.

Table 3.4 below summarises the design characteristics adopted for the OSD tank, whilst **Table 4.2** summarises the design characteristics of the basin. The *DRAINS* results for the basin

are attached in **Appendix B**, and the peak flows for the 5, 20, and 100 year ARI are summarised in **Table 3.5**.

Table 3.4 Pad 4 OSD Tank Characteristics

Variable	Detention
Base RL	45.50
Low Level Outlet RL	45.50
Orifice Diameter (mm)	600
Top RL	47.00
Base Area (m ²)	866
Tank Vol (m ³)	1300

Table 3.5 demonstrates that the proposed OSD tank and basin will satisfactorily reduce the post-developed flows to the pre-developed flows.

Table 3.5 Post-Development Peak Flows with OSD

ARI (Years)	Flow (m³/s)
5	0.78
20	0.82
100	1.45

4 STORMWATER TREATMENT

4.1 STORMWATER QUALITY OBJECTIVES

The stormwater treatment objectives for the proposed bio-retention basin have been adopted from the “Erskine Park Employment Area” DCP. The identified target pollutant removal efficiencies from this document are summarised below in **Table 4.1**.

Table 4.1 Pollutant Removal Objectives

Nutrient	Pollutant Removal Criteria (%)
Total Phosphorous	45
Total Nitrogen	45
Total Suspended Solids	80

4.2 STORMWATER TREATMENT STRATEGY

The stormwater treatment strategy for the site includes; bio-retention basins, litter pits and bio-filtration swales. In addition, stormwater reuse will be undertaken to reduce potable water demand. This will take the form of rainwater tanks that will be allocated to the site for potential use for irrigation, toilet flushing and other non-potable uses, possibly such as truck washing.

The clean water from the roof area of the Pad 4 site will be directed to the OSD tank rather than the water quality basin. All other runoff from Pad 4 will be directed to water quality devices before being discharged.

4.3 PAD 4 WATER QUALITY BASIN

The proposed water quality basin has been sized using the MUSIC water quality program. The model data and results have been attached in **Appendix C** and a summary of the designed basin details is shown below in **Table 4.2**.

Table 4.2 Pad 4 Bio-Filtration Basin Details

Parameter	
Basin Base Area (m ²)	520
Bio-filter Area (m ²)	520
Base Level (m AHD)	45.5
Depth of Ponding (m) when overflow begins	1.3
Volume 1 Year ARI (m ³)	600
Peak Flow 1 Year ARI (m ³ /s)	0.38
Volume of Filtration Basin (m ³) at Overflow Level	700
Filter Depth (m)	0.6

The basin has been designed to store greater than the 1 Year ARI storm event and drain this via a subsoil drainage system under the bio-filter layer. All flows which exceed the 1 Year ARI will overflow to the grass buffer strip to the west, then across the buffer strip to the swale.

The basin has been run through the *MUSIC* program to assess whether the design will meet the requirements spelled out in the “Erskine Park Employment Area – Development Control Plan” shown in **Table 4.1**. The input data and results of this model have been attached in **Appendix C**. **Table 4.3** below compares the post-treatment annual pollutant loads with the pre-treatment pollutant loads calculated in the *MUSIC* model, and the calculated removal efficiency these represent.

Table 4.3 Comparison of Pre-treatment and Post-treatment Pollutant Loads for the Developed Site from the MUSIC Model

Site	Loads (kg/y)		
	TSS	TP	TN
Pre-treatment	1620	4.3	31.8
Post-treatment	132	0.88	11.3
Removal Efficiency	91.8%	79.8%	64.5%

Table 4.3 above demonstrates that the treatment train designed will adequately meet the requirements of the Erskine Park Employment Area DCP, and reduce the post-development pollutant loads by more than the amounts shown in **Table 4.1**.

5 SOIL & WATER MANAGEMENT DURING CONSTRUCTION

Sedimentation and erosion controls will be constructed prior to commencement of any work to minimise the discharge of sediment from the site. The controls will be designed and installed in accordance with the requirements of the NSW Department of Housing ‘Soils & Construction’ manual.

5.1 TEMPORARY SEDIMENT & EROSION CONTROLS

The engineering bulk earthworks drawings show the concept sediment and erosion control plan for the development.

- A single all weather access way at the front of the property consisting of 50-75mm aggregate or similar material at a minimum thickness of 150mm, laid over geo-fabric and constructed prior to commencement of works.
- A shaker pad will be used at the entrance to the site to remove clay from vehicles leaving the site so as to maintain public roads in a clean condition.
- This sediment control basin should be located where the proposed water quality basin is to be constructed immediately to the west of the site. Once the majority of the site has been constructed the basin should then be converted to its ultimate use as a water quality control basin.
- Disturbed areas will be rehabilitated with indigenous plant species, landscaped and treated by approved methods of erosion mitigation such as mulching, revegetation with native grasses or other suitable stabilising processes within fifteen days of the completion of works.
- All runoff and erosion controls will be installed before any works are carried out at the site.
- Upslope clean surface runoff will be diverted via diversion drains and sediment fencing around the disturbed areas.
- Installing *SoilLocker* at the down-slope of the disturbed areas to capture sediment and debris escaping from the site.

- *SoilLocker* shall be installed on the boundary of the creek buffer area.
- Topsoil stockpiling stripped from the construction site shall be diverted away from drainage lines, stormwater inlets and be suitably covered by impervious membrane material and screened by sediment fencing.
- Sediment end erosion controls shall be inspected weekly or after each storm event for litter, sediment, and organic waste accumulation. All sediment/debris shall be removed within two (2) working days.

5.2 SEDIMENT BASIN CONCEPT DESIGN

The sediment basin has been designed to capture the first 25mm runoff from the 75th percentile, 5-day rainfall event, as per the NSW Department of Housing Guidelines. An additional 50% capacity has been provided for storage of sediment.

The concept design is based on the equation: $V = 10.C_v.A.R_{5day\ 75th\ \% \ ile}$

As recommended by the *NSW Department of Housing (1998)*, a volumetric runoff coefficient (C_v) of 0.5 has been adopted for the construction phase. The outlet to each of the basins will be a slow control discharge. A spillway will be incorporated into the basin design for an overflow.

5.3 SEDIMENT BASIN FLOCCULATION & DISCHARGE WATER QUALITY CRITERIA

Runoff captured in the sediment basin will be treated with an approved flocculating agent before discharging water, as the catchment contains soils that are classified as fine dispersible, which do not readily settle from suspension. The flocculation should ensure that discharges contain no more than 50 mg/L of suspended solids or 30 NTU before being discharged. Furthermore, dewatering should preferably be over existing stable, grassed areas and not directly into the creek.

6 CONCLUSION

This Stormwater Concept Plan describes the management of stormwater within Pad 4. The report sets out the basic stormwater parameters that need to be met by the future development of the site.

The proposal satisfies the requirements for stormwater quality and quantity control identified by Penrith Council in the DCP for the area.

7 REFERENCES

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8 APPENDICES

Appendix A	Drawings
Appendix B	Post-Development Flows with Detention - Pad 4
Appendix C	Water Quality Results Pad 4





APPENDIX A

DRAWINGS

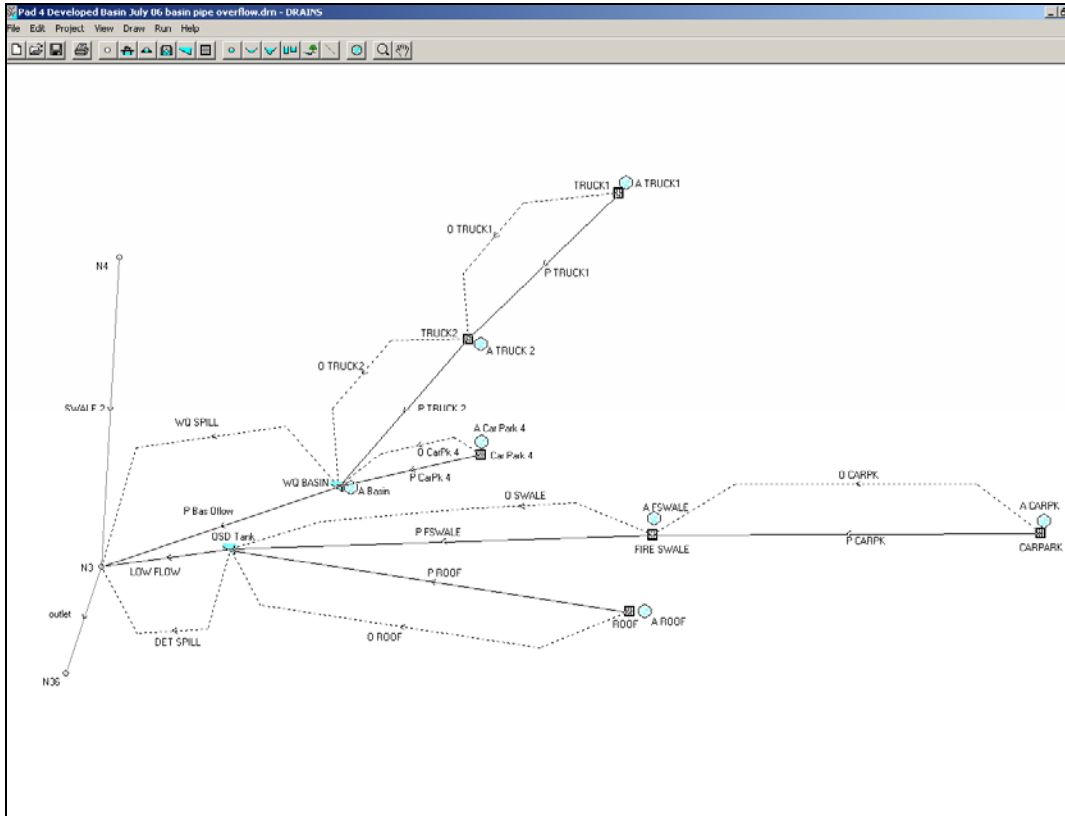




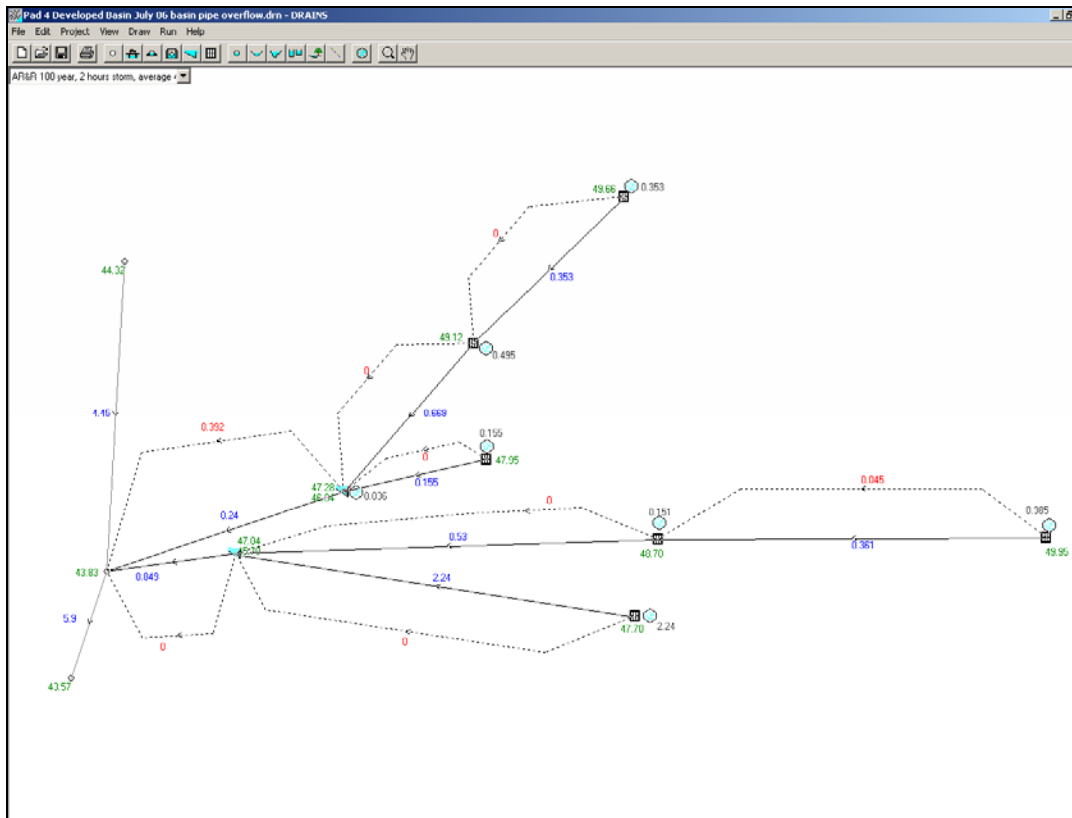
APPENDIX B

Post-Development Flows with Detention Pad 4

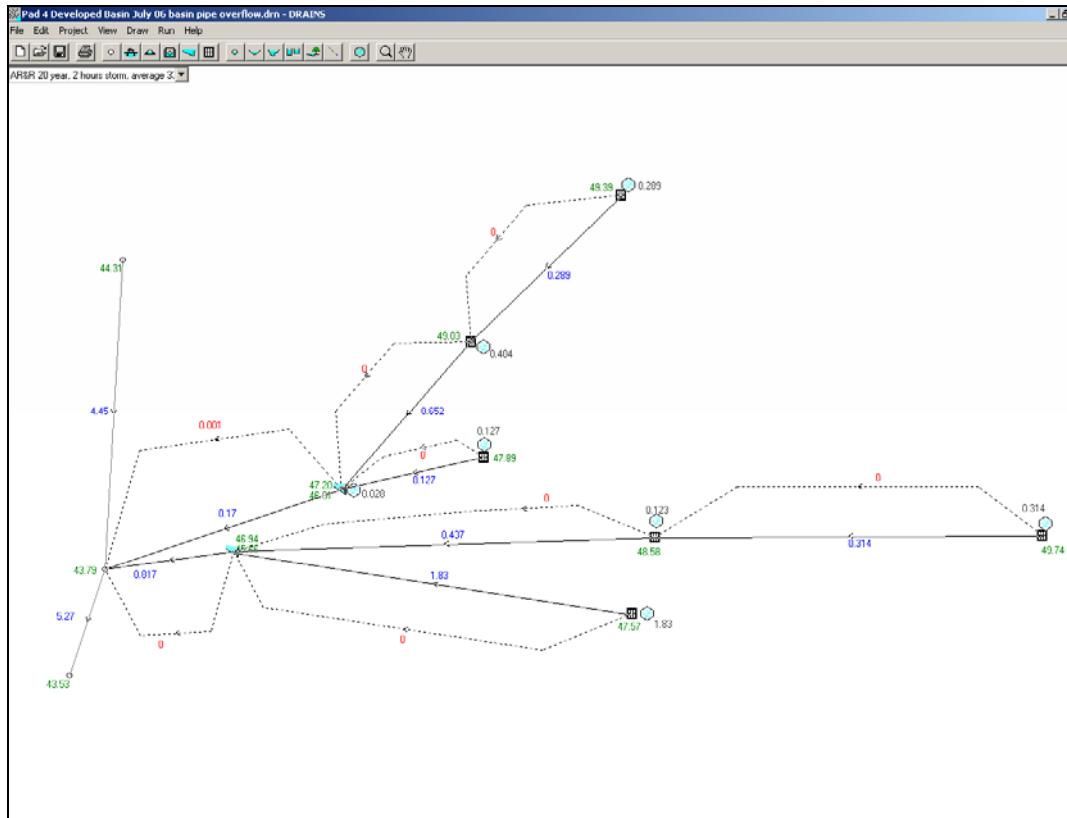




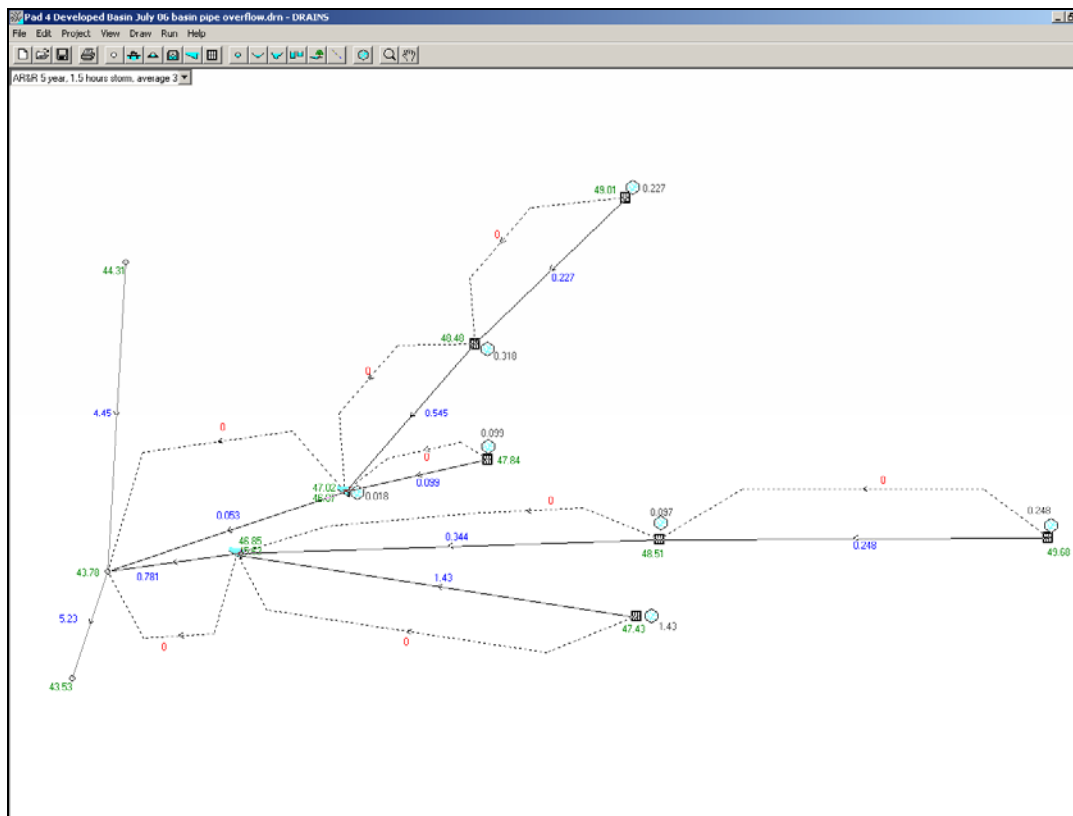
DRAINS MODEL FOR DEVELOPED SITE WITH BASIN AND OSD TANK



100 YEAR ARI RESULTS



20 YEAR ARI RESULTS



5 YEAR ARI RESULTS

DRAINS DATA

PIT / NODE DETAILS													Version 9						
Name	Type	Family	Size	Ponding Volume (cu.m)	Pressure Change Coeff. Ku	Surface Elev (m)	Max Pond Depth (m)	Base Inflow (cu.m/s)	Blocking Factor	x	y	Bolt-down lid	id	Part Full Shock Loss					
N4	Node					46.5		4.45		295828.8	6256007		130						
N3	Node					46		0		295813.7	6255742		129						
N36	Node					46		0		295783.2	6255650		38293						
CARPARK	OnGrade	UNLIMITED	UNLIMITED INLET		1.5	49.95		0	0	296617.4	6255770	No	139	1 x Ku					
FIRE SWALE	OnGrade	UNLIMITED	UNLIMITED INLET		1.5	48.7		0	0	296285.3	6255769	No	141	1 x Ku					
TRUCK1	OnGrade	UNLIMITED	UNLIMITED INLET		1.5	49.93		0	0	296256.5	6256062	No	143	1 x Ku					
TRUCK2	Sag	UNLIMITED	UNLIMITED	100	1.5	49	0.2	0	0	296127.6	6255937	No	144	1 x Ku					
ROOF	OnGrade	UNLIMITED	UNLIMITED INLET		1.5	48.5		0	0	296265.6	6255704	No	152	1 x Ku					
Car Park 4	OnGrade	UNLIMITED	UNLIMITED INLET		1.5	48.5		0	0	296138.9	6255837	No	1801972	1 x Ku					
DETENTION BASIN DETAILS																			
Name	Elev	Volume	Init Vol. (cu)	Outlet Type	K	Dia(mm)	Centre RL	Pit Family	Pit Type	x	y	HED	Crest RL	Crest Leng	id				
OSD Tank	45.5	0	0	Orifice		600	45.8			295924.4	6255757	Yes	46.5	3	127				
	46.5	866																	
	47	1300																	
WQ BASIN	45.5	0	0	Culvert	0.5					296016.9	6255810	No			126				
	46.5	540																	
	47	810																	
SUB-CATCHMENT DETAILS																			
Name	Pit or Node	Total Area	Impervious Area	Avg Slope(%)	Hydrological Model														
A CARPK	CARPARK	0.783	73.3	0.5	EP RAFTS														
A FSWALE	FIRE SWALE	0.306	90	0.5	EP RAFTS														
A TRUCK1	TRUCK1	0.7122	95	0.5	EP RAFTS														
A TRUCK 2	TRUCK2	0.9978	95	0.5	EP RAFTS														
A Basin	WQ BASIN	0.1	10	0.5	EP RAFTS														
A ROOF	ROOF	4.4577	100	2	EP RAFTS														
A Car Park 4	Car Park 4	0.31	95	0.5	EP RAFTS														
PIPE DETAILS																			
Name	From	To	Length (m)	U/S IL (m)	D/S IL (m)	Slope (%)	Type	Dia (mm)	I.D. (mm)	Rough	Pipe Is	No. Pipes	Chg From	At Chg	Chg (m)	RI (m)	Chg (m)	RL (m)	etc (m)
P CARPK	CARPARK	FIRE SWAL	250	49.05	47.8	0.5	Concrete, t	525	525	0.3	New	1	CARPARK		0				
P FSWALE	FIRE SWALE	OSD Tank	250	47.8	46.55	0.5	Concrete, t	600	600	0.3	NewFixed	1	FIRE SWA		0				
LOW FLOW	OSD Tank	N3	25	45	44.875	0.5	Concrete, t	675	675	0.3	NewFixed	1	OSD Tank		0				
P TRUCK1	TRUCK1	TRUCK2	185	48.525	47.6	0.5	Concrete, t	600	600	0.3	New	1	TRUCK1		0				
P TRUCK 2	TRUCK2	WQ BASIN	185	47.525	46.6	0.5	Concrete, t	600	600	0.3	NewFixed	1	TRUCK2		0				
P Bas Oflow	WQ BASIN	N3	50	46.8	43.5	6.6	Concrete, t	600	600	0.3	NewFixed	1	WQ BASIN		0				
P ROOF	ROOF	OSD Tank	50	46.5	46	1	Concrete, t	1500	1524	0.3	NewFixed	1	ROOF		0				
P CarPk 4	Car Park 4	WQ BASIN	50	47.5	47	1	Concrete, t	450	450	0.3	NewFixed	1	Car Park 4		0				
DETAILS of SERVICES CROSSING PIPES																			
Pipe	Chg (m)	Bottom Elev (m)	Height of S (m)	Chg (m)	Bottom Elev (m)	Height of S (m)	Chg (m)	Bottom Elev (m)	Height of S (m)	Setc etc									
CHANNEL DETAILS																			
Name	From	To	Type	Length (m)	U/S IL (m)	D/S IL (m)	Slope (%)	Base Width (m)	L.B. Slope (1:?)	R.B. Slope (1:?)	Manning n	Depth (m)	Roofed						
SWALE 2 outlet	N4	N3	Prismatic	100	43.55	43.05	0.5	3	4	4	0.05	1.4	No						
	N3	N36	Prismatic	10	43.05	43	0.5	3	4	4	0.05	1.4	No						
OVERFLOW ROUTE DETAILS																			
Name	From	To	Travel Time (min)	Spill Level (m)	Crest Length (m)	Weir Coeff. C	Cross Section	Safe Depth (m)	SafeDepth Major Stori (m)	SafeDepth Minor Stori (m)	Safe DxV (sq.m/sec)	Bed Slope (%)	D/S Area Contributing	id					
O CARPK	CARPARK	FIRE SWAL	1				Dummy us	0.2	0.05	0.6	1	0	528217						
O SWALE	FIRE SWALE	OSD Tank	1				Dummy us	0.2	0.05	0.6	1	0	528221						
DET SPILL	OSD Tank	N3	0.5	47	2	1.7	Dummy us	0.2	0.05	0.6	1	0	161						
O TRUCK1	TRUCK1	TRUCK2	1				Dummy us	0.2	0.05	0.6	1	0	528213						
O TRUCK2	TRUCK2	WQ BASIN	1				Dummy us	0.2	0.05	0.6	1	0	528219						
WQ SPILL	WQ BASIN	N3	0.1	47.2	10	1.7	Dummy us	0.2	0.05	0.6	1	0	160						
O ROOF	ROOF	OSD Tank	2				Dummy us	0.2	0.05	0.6	1	0	262853						
O CarPk 4	Car Park 4	WQ BASIN	1				Dummy us	0.2	0.05	0.6	1	0	1801980						

DRAINS 100YR RESULTS

PIT / NODE DETAILS		Version 8							
Name	Max HGL	Max Pond HGL	Max Surface Flow Arrival (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint		
N4	44.32		0						
N3	43.83		0						
N36	43.57		0						
CARPARK	49.95		0.385		0	0.045	Outlet System		
FIRE SWALE	48.7		0.189		0	0	Outlet System		
TRUCK1	49.66		0.353		0.27	0	None		
TRUCK2	49.12	49.12	0.495	44.7	-0.12	0	Outlet System		
ROOF	47.7		2.24		0.8	0	None		
Car Park 4	47.95		0.155		0.55	0	None		
SUB-CATCHMENT DETAILS									
Name	Max Flow (cu.m/s)	Due to Storm							
A CARPK	0.385	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A FSWALE	0.151	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A TRUCK1	0.353	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A TRUCK 2	0.495	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A Basin	0.036	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A ROOF	2.24	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
A Car Park 4	0.155	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1							
PIPE DETAILS									
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm				
P CARPK	0.361	1.7	49.762	48.7	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P FSWALE	0.53	2.2	48.431	47.035	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
LOW FLOW	0.849	2.5	45.696	45.467	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P TRUCK1	0.353	1.2	49.545	49.121	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P TRUCK 2	0.669	2.4	48.701	47.281	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P Bas Oflow	0.24	5	46.935	43.827	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P ROOF	2.24	3.9	47.036	47.035	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
P CarPk 4	0.155	2.1	47.71	47.281	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
CHANNEL DETAILS									
Name	Max Q (cu.m/s)	Max V (m/s)	Chainage (m)	Max HGL (m)	Due to Storm				
SWALE 2	4.45	1.8			AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
outlet	5.901	2			AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1				
OVERFLOW ROUTE DETAILS									
Name	Max Q U/S (cu.m/s)	Max Q D/S (cu.m/s)	Safe Q (cu.m/s)	Max D (m)	Max DxV	Max Width	Max V	Due to Storm	
O CARPK	0.045	0.045	7.665	0.026	0.01	8.83	0.38	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1	
O SWALE	0	0	7.665	0	0	0	0		
DET SPILL	0	0	7.665	0	0	0	0		
O TRUCK1	0	0	7.665	0	0	0	0		
O TRUCK2	0	0	7.665	0	0	0	0		
WQ SPILL	0.392	0.392	7.665	0.06	0.04	15.94	0.73	AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1	
O ROOF	0	0	7.665	0	0	0	0		
O CarPk 4	0	0	7.665	0	0	0	0		
DETENTION BASIN DETAILS									
Name	Max WL	Max Vol	Max Q Total	Max Q Low Level	Max Q High Level				
OSD Tank	47.04	1272.7	0.849	0.849	0				
WQ BASIN	47.28	961.7	0.632	0.24	0.392				
CONTINUITY CHECK for AR&R 100 year, 2 hours storm, average 44.3 mm/h, Zone 1									
Node	Inflow (cu.m)	Outflow (cu.m)	Storage Change (cu.m)	Difference %					
N4	0	49394.85	0	0					
N3	55248.28	55114.18	0	0.2					
N36	55114.18	55114.18	0	0					
CARPARK	655.98	656.01	0	0					
FIRE SWALE	918.6	918.49	0	0					
OSD Tank	4814.21	4778.57	48.32	-0.3					
TRUCK1	618.78	618.78	0	0					
TRUCK2	1485.24	1481.92	0	0.2					
WQ BASIN	1824.02	1074.92	750.23	-0.1					
ROOF	3895.71	3895.71	0	0					
Car Park 4	269.47	269.47	0	0					
Run Log for Pad 4 Developed Basin July 06 basin pipe overflow.drn run at 11:30:44 on 5/7/2006									
No water upwelling from any pit.									
Freeboard was less than 0.15m at TRUCK2, FIRE SWALE, CARPARK									
To see more detailed results select the Edit/Copy Results to Spreadsheet menu item, and paste them into a spreadsheet.									

DRAINS 20YR RESULTS

PIT / NODE DETAILS				Version 8				
Name	Max HGL	Max Pond HGL	Max Surface Flow Arrival (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint	
N4	44.31		0					
N3	43.79		0					
N36	43.53		0					
CARPARK	49.74		0.314		0.21	0	None	
FIRE SWALE	48.58		0.123		0.12	0	None	
TRUCK1	49.39		0.289		0.54	0	None	
TRUCK2	49.03	49.03	0.404	8	-0.03	0	Outlet System	
ROOF	47.57		1.825		0.93	0	None	
Car Park 4	47.89		0.127		0.61	0	None	
SUB-CATCHMENT DETAILS								
Name	Max Flow (cu.m/s)	Due to Storm						
A CARPK	0.314	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A FSWALE	0.123	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A TRUCK1	0.289	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A TRUCK 2	0.404	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A Basin	0.028	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A ROOF	1.825	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
A Car Park 4	0.127	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1						
PIPE DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm			
P CARPK	0.314	1.6	49.505	48.583	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P FSWALE	0.437	2	48.223	46.973	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
LOW FLOW	0.817	2.5	45.661	45.456	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P TRUCK1	0.289	1	49.316	49.032	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P TRUCK 2	0.652	2.3	48.625	47.202	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P Bas Oflow	0.17	4.7	46.912	43.786	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P ROOF	1.825	3.7	46.976	46.944	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
P CarPk 4	0.127	2	47.688	47.202	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
CHANNEL DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)	Chainage (m)	Max HGL (m)	Due to Storm			
SWALE 2	4.45	1.8			AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
outlet	5.267	1.9			AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1			
OVERFLOW ROUTE DETAILS								
Name	Max Q U/S (cu.m/s)	Max Q D/S (cu.m/s)	Safe Q (cu.m/s)	Max D (m)	Max DxV	Max Width	Max V	Due to Storm
O CARPK	0	0	0.256	0	0	0	0	
O SWALE	0	0	0.256	0	0	0	0	
DET SPILL	0	0	0.256	0	0	0	0	
O TRUCK1	0	0	0.256	0	0	0	0	
O TRUCK2	0	0	0.256	0	0	0	0	
WQ SPILL	0.001	0.001	0.256	0.007	0	2.25	0.15	AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1
O ROOF	0	0	0.256	0	0	0	0	
O CarPk 4	0	0	0.256	0	0	0	0	
DETENTION BASIN DETAILS								
Name	Max WL	MaxVol	Max Q Total	Max Q Low Level	Max Q High Level			
OSD Tank	46.94	0	0.817	0.817	0			
WQ BASIN	47.2	0	0.171	0.17	0.001			
CONTINUITY CHECK for AR&R 20 year, 2 hours storm, average 33.6 mm/h, Zone 1								
Node	Inflow (cu.m)	Outflow (cu.m)	Storage Ct (cu.m)	Difference %				
N4	0	49394.85	0	0				
N3	53626.63	53492.63	0	0.2				
N36	53492.63	53492.63	0	0				
CARPARK	489.07	489.07	0	0				
FIRE SWALE	686.44	685.79	0	0.1				
OSD Tank	3630.38	3601.72	41.31	-0.3				
TRUCK1	467.06	467.06	0	0				
TRUCK2	1120.9	1121.71	0	-0.1				
WQ BASIN	1376.91	630.09	747.69	-0.1				
ROOF	2944.59	2944.59	0	0				
Car Park 4	203.39	203.39	0	0				
Run Log for Pad 4 Developed Basin July 06 basin pipe overflow.drn run at 11:28:57 on 5/7/2006								
No water upwelling from any pit.								
Freeboard was less than 0.15m at TRUCK2, FIRE SWALE								
To see more detailed results select the Edit/Copy Results to Spreadsheet menu item, and paste them into a spreadsheet.								

DRAINS RESULTS 5YR

PIT / NODE DETAILS			Version 8					
Name	Max HGL	Max Pond HGL	Max Surface Flow Arrival (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint	
N4	44.31		0					
N3	43.78		0					
N36	43.53		0					
CARPARK	49.68		0.248		0.27	0	None	
FIRE SWALE	48.51		0.097		0.19	0	None	
TRUCK1	49.01		0.227		0.92	0	None	
TRUCK2	48.48	49	0.318	0	0.52	0	None	
ROOF	47.43		1.434		1.07	0	None	
Car Park 4	47.84		0.099		0.66	0	None	
SUB-CATCHMENT DETAILS								
Name	Max Flow (cu.m/s)	Due to Storm						
A CARPK	0.248	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A FSWALE	0.097	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A TRUCK1	0.227	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A TRUCK 2	0.318	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A Basin	0.018	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A ROOF	1.434	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
A Car Park 4	0.099	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1						
PIPE DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm			
P CARPK	0.248	1.8	49.362	48.514	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P FSWALE	0.344	2	48.151	46.901	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
LOW FLOW	0.781	2.4	45.627	45.442	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P TRUCK1	0.227	1.8	48.802	48.484	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P TRUCK 2	0.545	2.2	48.2	47.087	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P Bas Oflow	0.053	3	46.868	43.784	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P ROOF	1.434	3.6	46.911	46.847	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
P CarPk 4	0.099	1.9	47.665	47.165	AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
CHANNEL DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)	Chainage (m)	Max HGL (m)	Due to Storm			
SWALE 2	4.45	1.8			AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
outlet	5.231	1.9			AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1			
OVERFLOW ROUTE DETAILS								
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
O CARPK	0	0	0.256	0	0	0	0	0
O SWALE	0	0	0.256	0	0	0	0	0
DET SPILL	0	0	0.256	0	0	0	0	0
O TRUCK1	0	0	0.256	0	0	0	0	0
O TRUCK2	0	0	0.256	0	0	0	0	0
WQ SPILL	0	0	0.256	0	0	0	0	0
O ROOF	0	0	0.256	0	0	0	0	0
O CarPk 4	0	0	0.256	0	0	0	0	0
DETENTION BASIN DETAILS								
Name	Max WL	Max Vol	Max Q Total	Max Q Low Level	Max Q High Level			
OSD Tank	46.85	475.9	0.781	0.781	0			
WQ BASIN	47.02	819.6	0.053	0.053	0			
CONTINUITY CHECK for AR&R 5 year, 1.5 hours storm, average 30.3 mm/h, Zone 1								
Node	Inflow (cu.m)	Outflow (cu.m)	Storage Change (cu.m)	Difference %				
N4	0	41384.94	0	0				
N3	43953.85	43819.83	0	0.3				
N36	43819.83	43819.83	0	0				
CARPARK	321.14	321.14	0	0				
FIRE SWALE	452.59	451.12	0	0.3				
OSD Tank	2426.21	2396.89	39.87	-0.4				
TRUCK1	312.29	312.29	0	0				
TRUCK2	749.46	749.46	0	0				
WQ BASIN	916.86	172.05	744.93	0				
ROOF	1975.09	1975.09	0	0				
Car Park 4	136.04	136.04	0	0				
Run Log for Pad 4 Developed Basin July 06 basin pipe overflow.drn run at 11:31:47 on 5/7/2006								
No water upwelling from any pit. Freeboard was adequate at all pits.								
To see more detailed results select the Edit/Copy Results to Spreadsheet menu item, and paste them into a spreadsheet.								



APPENDIX C

Water Quality Results Pad 4



PAD 4 MUSIC RESULTS

Source nodes

Location	Truck area	Car Park 4	Car Park 1&2	Car Park 3				
ID	1	3	4	5				
Node Type	UrbanSourceNode	UrbanSourceNode	UrbanSourceNode	UrbanSourceNode				
Total Area (ha)	1.710	0.310	0.455	0.328				
Area Impervious (ha)	1.233	0.224	0.238	0.200				
Area Pervious (ha)	0.477	0.086	0.217	0.128				
Field Capacity (mm)	80	50	50	50				
Pervious Area Infiltration Capacity coefficient - a	200	50	50	50				
Pervious Area Infiltration Capacity exponent - b	1	2	2	2				
Impervious Area Rainfall Threshold (mm/day)	1	1	1	1				
Pervious Area Soil Storage Capacity (mm)	120	150	150	150				
Pervious Area Soil Initial Storage (% of Capacity)	25	25	25	25				
Groundwater Initial Depth (mm)	50	50	50	50				
Groundwater Daily Recharge Rate (%)	25	0.65	0.65	0.65				
Groundwater Daily Baseflow Rate (%)	5	0.85	0.85	0.85				
Groundwater Daily Deep Seepage Rate (%)	0	0	0	0				
Stormflow Total Suspended Solids Mean (log mg/L)	1.92	2.2	2.2	2.2				
Stormflow Total Suspended Solids Standard Deviation (log mg/L)	0.44	0.32	0.32	0.32				
Stormflow Total Suspended Solids Estimation Method	Mean	Mean	Mean	Mean				
Stormflow Total Suspended Solids Serial Correlation	0	0	0	0				
Stormflow Total Phosphorus Mean (log mg/L)	-0.59	-0.45	-0.45	-0.45				
Stormflow Total Phosphorus Standard Deviation (log mg/L)	0.36	0.25	0.25	0.25				
Stormflow Total Phosphorus Estimation Method	Mean	Mean	Mean	Mean				
Stormflow Total Phosphorus Serial Correlation	0	0	0	0				
Stormflow Total Nitrogen Mean (log mg/L)	0.25	0.42	0.42	0.42				
Stormflow Total Nitrogen Standard Deviation (log mg/L)	0.32	0.19	0.19	0.19				
Stormflow Total Nitrogen Estimation Method	Mean	Mean	Mean	Mean				
Stormflow Total Nitrogen Serial Correlation	0	0	0	0				
Baseflow Total Suspended Solids Mean (log mg/L)	0.78	1.1	1.1	1.1				
Baseflow Total Suspended Solids Standard Deviation (log mg/L)	0.45	0.17	0.17	0.17				
Baseflow Total Suspended Solids Estimation Method	Mean	Mean	Mean	Mean				
Baseflow Total Suspended Solids Serial Correlation	0	0	0	0				
Baseflow Total Phosphorus Mean (log mg/L)	-1.11	-0.82	-0.82	-0.82				
Baseflow Total Phosphorus Standard Deviation (log mg/L)	0.48	0.19	0.19	0.19				
Baseflow Total Phosphorus Estimation Method	Mean	Mean	Mean	Mean				
Baseflow Total Phosphorus Serial Correlation	0	0	0	0				
Baseflow Total Nitrogen Mean (log mg/L)	0.14	0.32	0.32	0.32				
Baseflow Total Nitrogen Standard Deviation (log mg/L)	0.2	0.12	0.12	0.12				
Baseflow Total Nitrogen Estimation Method	Mean	Mean	Mean	Mean				
Baseflow Total Nitrogen Serial Correlation	0	0	0	0				
OUT - Mean Annual Flow (ML/yr)	9.74	1.79	2.18	1.72				
OUT - TSS Mean Annual Load (kg/yr)	754	276	326	261				
OUT - TP Mean Annual Load (kg/yr)	2.37	0.625	0.747	0.594				
OUT - TN Mean Annual Load (kg/yr)	17	4.69	5.66	4.47				
OUT - Gross Pollutant Mean Annual Load (kg/yr)	301	54.5	65.4	52.1				

No Imported Data Source nodes

USTM treatment nodes

Location	Infiltration Basin	Bio-Retention	Bio-Retention				
ID	2	6	7				
Node Type	BioRetentionNode	BioRetentionNode	BioRetentionNode				
Lo-flow bypass rate (cum/sec)	0	0	0				

PAD 4 MUSIC RESULTS

Hi-flow bypass rate (cum/sec)	100	100	100				
Inlet pond volume							
Area (sqm)	565	135	248				
Extended detention depth (m)	1.5	0	0				
Permanent pool volume (cum)							
Proportion vegetated							
Equivalent pipe diameter (mm)							
Overflow weir width (m)	2	2	2				
Notional Detention Time (hrs)							
Orifice discharge coefficient							
Weir coefficient	1.7	1.7	1.7				
Number of CSTR cells	3	3	3				
Total Suspended Solids k (m/yr)	1000	1000	1000				
Total Suspended Solids C* (mg/L)	12	12	12				
Total Suspended Solids C** (mg/L)							
Total Phosphorus k (m/yr)	500	500	500				
Total Phosphorus C* (mg/L)	0.13	0.13	0.13				
Total Phosphorus C** (mg/L)							
Total Nitrogen k (m/yr)	50	50	50				
Total Nitrogen C* (mg/L)	1.3	1.3	1.3				
Total Nitrogen C** (mg/L)							
Threshold hydraulic loading for C** (m/yr)							
Extraction for Re-use	Off	Off	Off				
Annual Re-use Demand - scaled by daily PET (ML)							
Constant Daily Re-use Demand (kL)							
User-defined Annual Re-use Demand (ML)							
Percentage of User-defined Annual Re-use Demand Jan							
Percentage of User-defined Annual Re-use Demand Feb							
Percentage of User-defined Annual Re-use Demand Mar							
Percentage of User-defined Annual Re-use Demand Apr							
Percentage of User-defined Annual Re-use Demand May							
Percentage of User-defined Annual Re-use Demand Jun							
Percentage of User-defined Annual Re-use Demand Jul							
Percentage of User-defined Annual Re-use Demand Aug							
Percentage of User-defined Annual Re-use Demand Sep							
Percentage of User-defined Annual Re-use Demand Oct							
Percentage of User-defined Annual Re-use Demand Nov							
Percentage of User-defined Annual Re-use Demand Dec							
Filter area (sqm)	500	135	240				
Filter depth (m)	0.6	0.6	0.6				
Filter median particle diameter (mm)	1	5	5				
Saturated hydraulic conductivity (mm/hr)	120	100	100				
Voids ratio	0.3	0.3	0.3				
Length (m)							
Bed slope							
Base Width (m)							
Top width (m)							
Vegetation height (m)							
Proportion of upstream impervious area treated							
Seepage Rate (mm/hr)	35	0	0				
Evap Loss as proportion of PET							
Depth in metres below the drain pipe	0	0	0				
IN - Mean Annual Flow (ML/yr)	11.5	2.18	1.72				
IN - TSS Mean Annual Load (kg/yr)	1.03E+03	326	261				

PAD 4 MUSIC RESULTS

IN - TP Mean Annual Load (kg/yr)	3	0.747	0.594					
IN - TN Mean Annual Load (kg/yr)	21.7	5.66	4.47					
IN - Gross Pollutant Mean Annual Load (kg/yr)	355	65.4	52.1					
OUT - Mean Annual Flow (ML/yr)	4.82	2.2	1.76					
OUT - TSS Mean Annual Load (kg/yr)	33.3	63.5	35.3					
OUT - TP Mean Annual Load (kg/yr)	0.361	0.304	0.213					
OUT - TN Mean Annual Load (kg/yr)	4.92	3.64	2.75					
OUT - Gross Pollutant Mean Annual Load (kg/yr)	0	0	0					

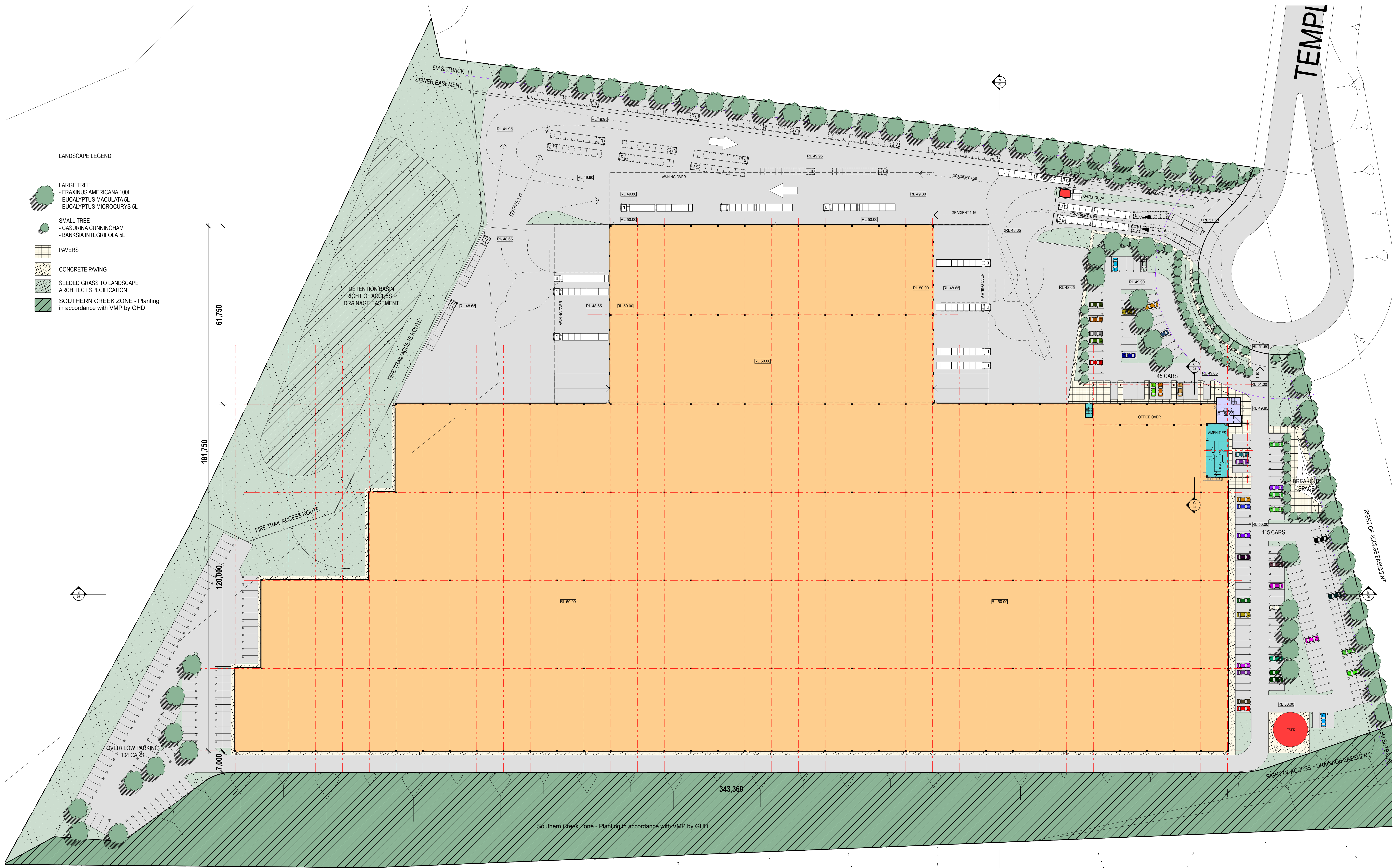
No Generic treatment nodes

Other nodes

Location	Junction	Receiving Node						
ID	8	9						
Node Type	JunctionNode	ReceivingNode						
IN - Mean Annual Flow (ML/yr)	8.78	8.78						
IN - TSS Mean Annual Load (kg/yr)	132	132						
IN - TP Mean Annual Load (kg/yr)	0.878	0.878						
IN - TN Mean Annual Load (kg/yr)	11.3	11.3						
IN - Gross Pollutant Mean Annual Load (kg/yr)	0	0						
OUT - Mean Annual Flow (ML/yr)	8.78	0						
OUT - TSS Mean Annual Load (kg/yr)	132	0						
OUT - TP Mean Annual Load (kg/yr)	0.878	0						
OUT - TN Mean Annual Load (kg/yr)	11.3	0						
OUT - Gross Pollutant Mean Annual Load (kg/yr)	0	0						

Links

Location	Drainage Link	Drainage Link	Drainage Link	Drainage Link	Drainage Link	Drainage Link	Drainage Link	Drainage Link
Source node ID	1	4	5	2	6	7	3	8
Target node ID	2	6	7	8	8	8	2	9
Muskingum-Cunge Routing	Not Routed	Not Routed	Not Routed	Not Routed	Not Routed	Not Routed	Not Routed	Not Routed
Muskingum K								
Muskingum theta								
IN - Mean Annual Flow (ML/yr)	9.74	2.18	1.72	4.82	2.2	1.76	1.79	8.78
IN - TSS Mean Annual Load (kg/yr)	754	326	261	33.3	63.5	35.3	276	132
IN - TP Mean Annual Load (kg/yr)	2.37	0.747	0.594	0.361	0.304	0.213	0.625	0.878
IN - TN Mean Annual Load (kg/yr)	17	5.66	4.47	4.92	3.64	2.75	4.69	11.3
IN - Gross Pollutant Mean Annual Load (kg/yr)	301	65.4	52.1	0	0	0	54.5	0
OUT - Mean Annual Flow (ML/yr)	9.74	2.18	1.72	4.82	2.2	1.76	1.79	8.78
OUT - TSS Mean Annual Load (kg/yr)	754	326	261	33.3	63.5	35.3	276	132
OUT - TP Mean Annual Load (kg/yr)	2.37	0.747	0.594	0.361	0.304	0.213	0.625	0.878
OUT - TN Mean Annual Load (kg/yr)	17	5.66	4.47	4.92	3.64	2.75	4.69	11.3
OUT - Gross Pollutant Mean Annual Load (kg/yr)	301	65.4	52.1	0	0	0	54.5	0



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		SCALE: 1:500 DRAWN BY: MB DATE: 4/07/2006 CHECKED: GA	JOB No: 06056 DRAWING NUMBER: DA-03 ISSUE: P08					



0 20 40 60 80 100 120 140 160 180 200
SCALE 1:2000 (A1)
SCALE 1:4000 (A3)

LIMIT OF WORKS

LOT 1
PREVIOUSLY
APPROVED
DA/04/1599

LOT 2
PREVIOUSLY
APPROVED
DA/04/1599

LOT 3
PREVIOUSLY
APPROVED
DA/04/1599

LOT 21
PREVIOUSLY
APPROVED
DA-284-11-2004-1
UNDER CONSTRUCTION

LEGEND

EXTENT OF WORKS

THIS DRAWING HAS
BEEN REDUCED

01	23/06/06	ISSUE FOR PROJECT APPLICATION	DH	RAP		
02	08/07/06	ISSUE FOR PROJECT APPLICATION-RESUBMITTED LAYOUT	DH	RAP		
REV	DATE	DESCRIPTION	BY	VER	APP	

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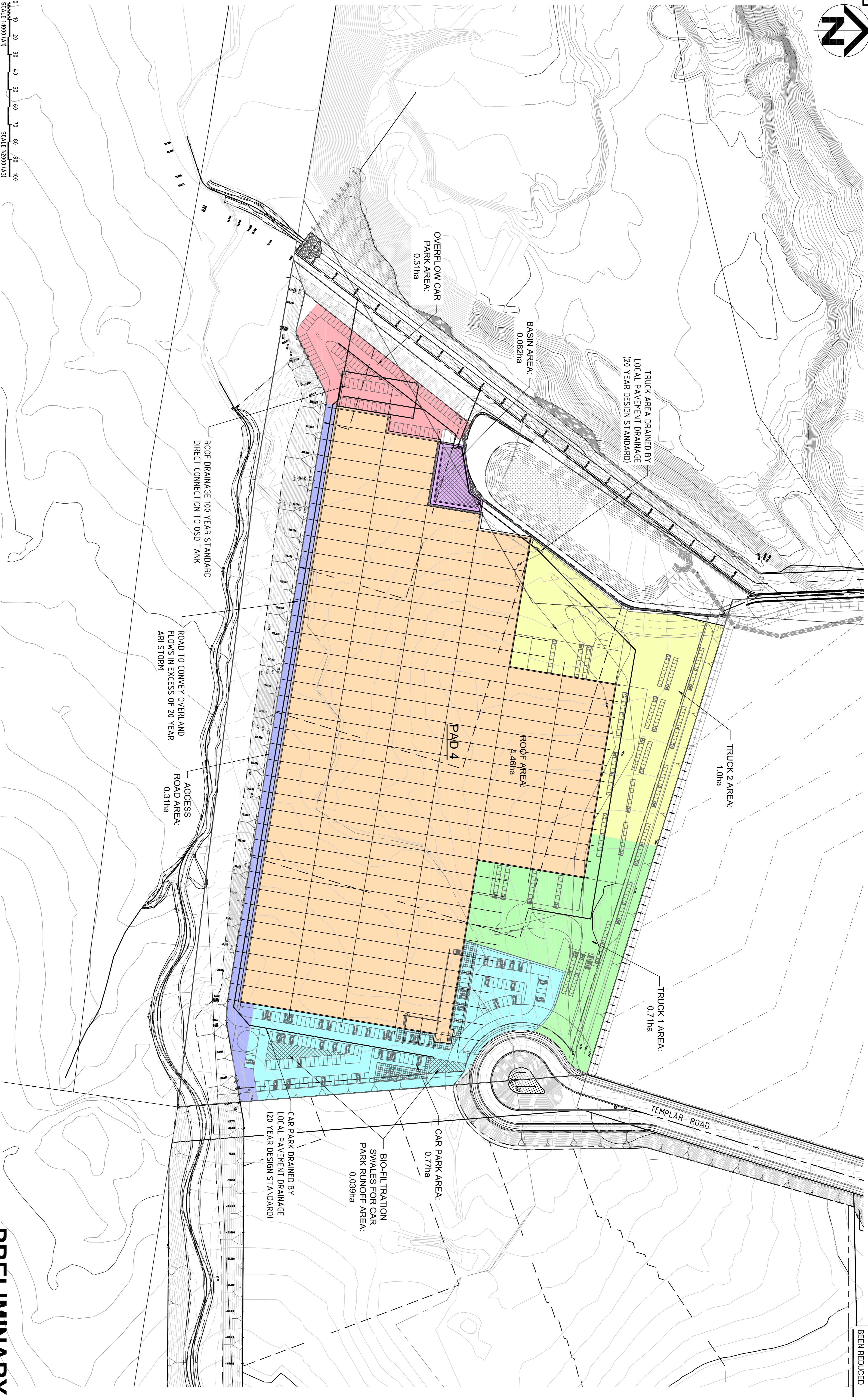
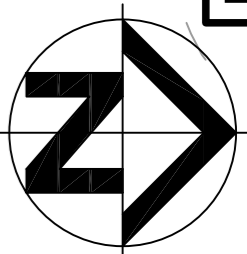
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VERIFICATION	
INITIALS	SIGNATURE
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DESIGN	
VERIFY	
APPROVED	

Client: **CSR LIMITED**
 Project: **PROPOSED INDUSTRIAL DEVELOPMENT**

Drawing: **OVERALL ENGINEERING PLAN**
 Drawn by: AK
 Design by: AK/WA
 Project No: M03033.12
 Drawing No: DA401
 Sheet: 1 OF 4
 Scale: 1:2000
 Ref: 02

PRELIMINARY



02	08/07/06	ISSUE FOR PROJECT APPLICATION-PRESSUED LAYOUT	DH	RAP	
01	23/06/06	ISSUE FOR PROJECT APPLICATION	DH	RAP	
REV	DATE	DESCRIPTION	BY	VER	APP

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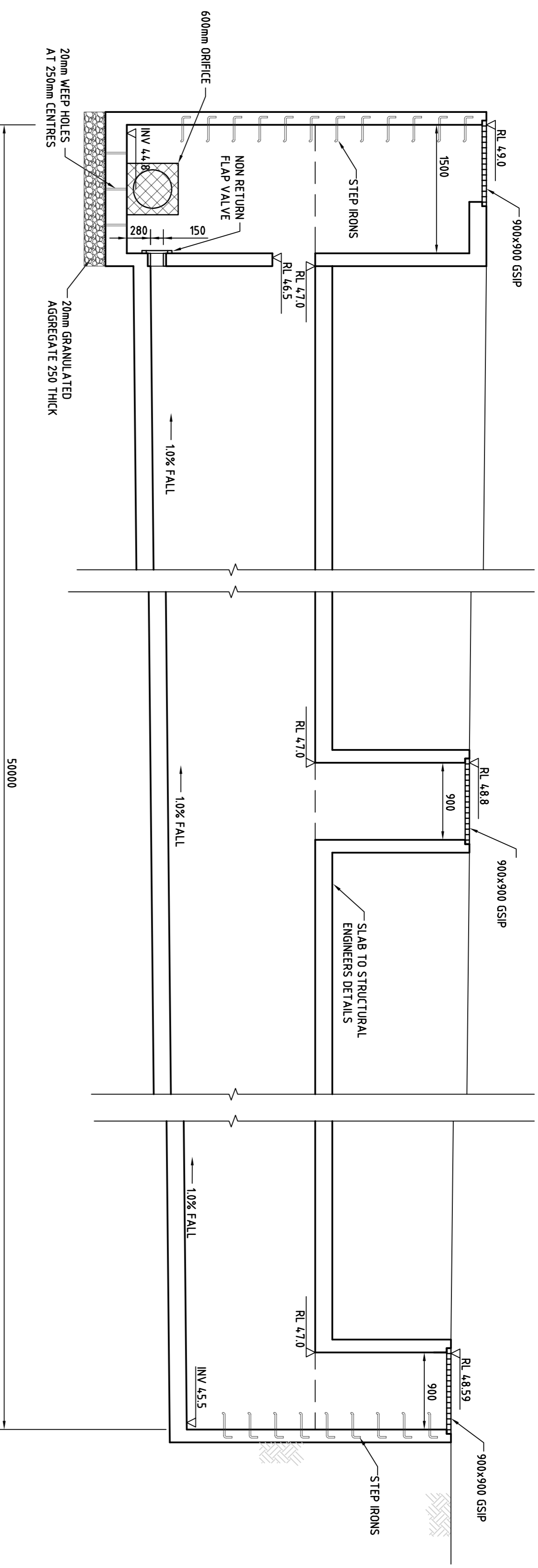
INITIALS	SIGNATURE	DATE

Client: **CSR LIMITED**
 Project: **PROPOSED INDUSTRIAL DEVELOPMENT**

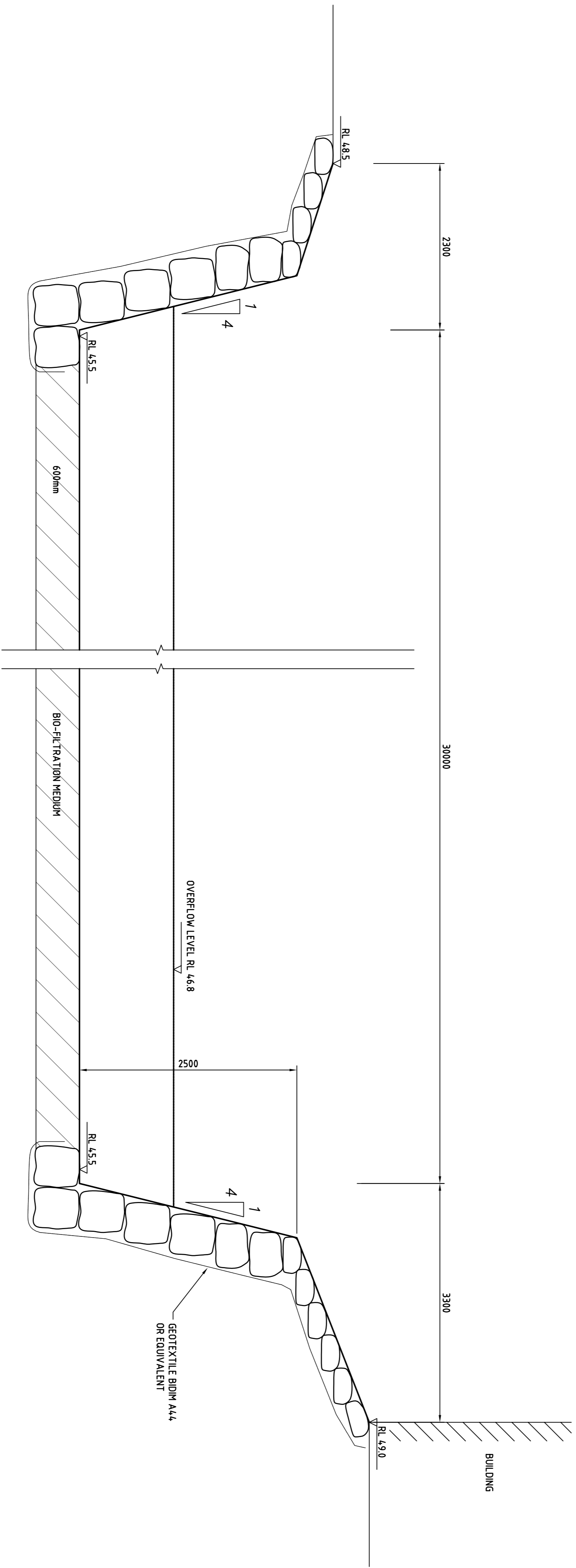
Drawing: **PAD 4 STORMWATER CONCEPT PLAN**
 Drawn by: AK
 Design by: AK/WA
 Project No: M03033.12
 Drawing No: DAK02
 Sheet: 2 OF 4
 Scale: 1:1000
 Rev: 02

PRELIMINARY

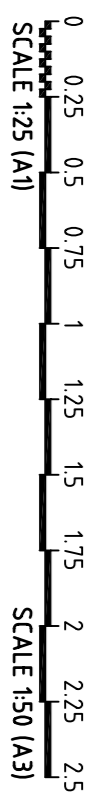
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SECTION 2
SCALE 1:25
DA403

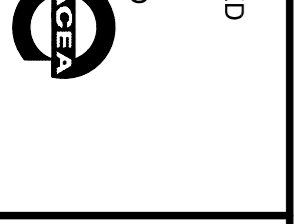


SECTION 1
SCALE 1:25
DA403



REV	DATE	DESCRIPTION	BY	VER	APP
02	08/07/06	ISSUE FOR PROJECT APPLICATION-RESUBMITTED LAYOUT	DH	RAP	
01	23/06/06	ISSUE FOR PROJECT APPLICATION	DH	RAP	
		AMENDMENTS			

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VERIFICATION	INITIALS	SIGNATURE	DATE
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DESIGN			
VERIFY			
APPROVED			

Client: **CSR LIMITED**
Project: **PROPOSED INDUSTRIAL DEVELOPMENT**

Drawing: **PAD 4 OSD TANK & WQ BASIN LONGITUDINAL SECTIONS 1 & 2**
Drawn by: AK
Design by: AK/WA
Project No: W030303.12
Drawing No: DA404
Sheet: 4 OF 4
Scale: 1:200
Rev: 02

PRELIMINARY