

**GEOTECHNICAL INVESTIGATION
AND REPORT FOR SAN HOSPITAL,
WAHROONGA**

Taylor Thomson Whitting
Level 3, 48 Chandos Street, St Leonards, NSW,
2065

GEOTLCOV23462AA-AD
29 April 2008

30 April 2008

Taylor Thomson Whitting
Level 3
48 Chandos Street
ST LEONARDS NSW 2065

Attention: Barry Young

Dear Barry,

RE: Geotechnical Investigation and Report for SAN Hospital, Wahroonga

We are pleased to submit our geotechnical investigation report for SAN Hospital, in Wahroonga, Sydney.

If you have any comments or queries, please contact either Mr Sam Henwood or the undersigned on 99111000.

For and on behalf of Coffey Geotechnics Pty Ltd



Peter Waddell

Principal Geotechnical Engineer

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 4 copies to Taylor Thomson Whitting

4.2.3 Groundwater

Groundwater seepage was only observed in three boreholes surrounding the proposed Building 3 site. Within boreholes CBH1, CBH7 and CBH18 seepage was observed at depths of 3.5m, 1.0m and 5.5m respectively. Within the cored boreholes, water was used as a drilling fluid which prevented groundwater observations.

It should be noted that groundwater levels are subject to variation due to the influence of rainfall, temperature, local drainage and the seasons. There may also be the potential for development of perched groundwater tables following periods of rainfall.

4.3 Laboratory Test Results

The six CBR test were carried out in potential subgrade soils for road pavements. CBR values varied from 2% to 10%.

Testing of pH, Sulphate and Chloride was carried out on six samples from fill and residual soil. Values for pH were found to vary from 4.7 to 8.1. The Sulphate and Chloride levels obtained from the tests were generally low with sulphate levels varying from 33 to 78 mg/kg (SO_4) and chloride levels from 2 to 290 mg/kg (Cl).

5 DISCUSSION AND RECOMMENDATIONS

Comments relevant to each separate building are provided in sections 5.1 to 5.4. Recommendations relevant to Buildings 1 to 3 are presented in sections 5.5 to 5.10. Earthquake load factors are provided for Buildings 1 to 4 in section 5.11.

5.1 Building 1

The subsurface conditions across the Building 1 site generally consist of fill, overlying a thin layer of residual soil, overlying sandstone. The existing car park was constructed by cut and fill techniques, with the eastern side of the car park cut into the natural ground and the western side filled up to 2.5m (within CBH15). The fill generally consists of Sandy Clay and Clayey Sand. In the absence of fill placement records and compaction control test results, the fill should be considered to be uncontrolled.

Preliminary sketches of the proposed car park show the base level to be at 154.6m AHD. With the depth to sandstone varying from 0.9m to 2.5m below current surface levels, it is likely that rock will be exposed or at relatively shallow depth below the proposed car park structure. With foundations spanning rock and soil there is a greater potential for differential settlements, compared to rock foundations. To avoid possible problems with differential settlement we recommend that building loads such as basement retaining walls and column loads be supported on rock. Strip, pad footings or bored piers could be adopted, depending on the bulk excavation levels and the depth to bedrock. Figure 4 shows cross sections through the site with inferred rock levels.

5.2 Building 2

The subsurface conditions across the Building 2 site generally consist of fill, overlying a thin layer of residual soil, overlying sandstone. Although the surface level of the existing car park falls at the eastern end this is where the greatest thickness of fill was observed and probably indicates the presence of a minor gully that was filled as part of the car park construction. Fill thickness varies from 0.2m at the

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Figure 2: Detailed Plan of Building 1 / 3 Showing Borehole Locations

Figure 3: Detailed Plan of Building 2 Showing Borehole Locations

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Appendices

Appendix A: Engineering Logs, Core Photographs and Explanation Sheets

Appendix B: Laboratory Test Reports

A stairway leads to the basement from within the building. Within the basement in rooms titled "South Wing Switch Room" and the "Electrical Store Room", brick strip footings supporting a concrete slab associated with the ground floor were visible. The footings were bearing on shale which was clearly visible in the cut which forms the basement as shown in photo 1 below.



Photo 1: Basement wall to the left and shale bedrock exposure to the right

4.2 Sub surface conditions

4.2.1 Published Geology

The Sydney 1:100,000 Geological Sheet indicates the site locality spans the contact between Ashfield Shale and Hawkesbury Sandstone. Ashfield Shale is described as a black to dark grey shale and laminate, while Hawkesbury Sandstone is described as medium to coarse grained quartz sandstone, very minor shale and laminate lenses.

4.2.2 Sub Surface Conditions

For a description of the subsurface conditions encountered at the borehole locations, refer to the Engineering Logs presented in Appendix A. Based on the information obtained from the boreholes, a general geotechnical model has been developed and is presented in Table 4.1. Sections showing the general geology for each building are also shown on Figures 4, 5 and 6.

1 INTRODUCTION

This report presents the results of a geotechnical investigation carried out by Coffey Geotechnics Pty Ltd (Coffey) for the proposed additions to the Sydney Adventist Hospital (SAN), Wahroonga. The work was commissioned by Barry Young of Taylor Thomson Whiting (TTW) on behalf of Coffey Projects Pty Ltd and was carried out in general accordance with our fee proposal reference GFOTLCOV23464AA-AA, dated 4 February 2008.

This report presents the results of the fieldwork, laboratory testing and a summary of the ground conditions encountered. It also provides geotechnical assessment for each of the proposed structures which form part of the proposed site development.

2 PROJECT APPRECIATION

The existing SAN Hospital is located on the western side of Fox Valley Road and is bounded by The Cornerarra Parkway to the south, Fox Valley Road to the east and Coups Creek to the west and north. Existing developments within the hospital grounds include multi-storey buildings, roads, car parks, sport facilities and landscaped grassed areas. There are four proposed additions to the hospital and these are labelled Building 1, 2, 3 and 4 as shown on the Site Plan in Figure 1. Details of the proposed improvements are as follows:

- **Building 1:** A new five storey multi deck car park to be built in the same area as an existing car park at grade.
- **Building 2:** A new four storey reinforced concrete framed building to replace an existing car park at grade.
- **Building 3:** A new building with a possible three storey basement.
- **Building 4:** An existing three storey brick building with modifications to load bearing internal walls within the eastern corner. The building will appear unchanged from the outside.

The objectives of the geotechnical investigation were to provide information on the subsurface conditions, a geotechnical model, and discussions and recommendations on relevant geotechnical aspects of the project.

An environmental assessment has also been carried out on this site and is detailed in a separate report

3 INVESTIGATION METHODOLOGY

3.1 Fieldwork

3.1.1 Buildings 1, 2, 3

Fieldwork to investigate Buildings 1, 2 and 3 was carried out from 10 to 25 March 2008 and comprised the drilling of 27 boreholes (CBH1 to CBH27).

The boreholes were drilled using a truck mounted drilling rig equipped with a continuous flight auger, to depths ranging between 1m and 12.36m with the exception of CBH26 and CBH27 where a hand auger was used to depths of 0.1m and 0.2m respectively. The boreholes were augered in soils using a solid flight auger and a steel V shaped bit or tungsten carbide bit. Standard Penetration Testing was carried

out in all boreholes to assess strength and to obtain samples for logging and laboratory analysis. Upon encountering rock, diamond coring techniques were used to advance the boreholes and to obtain core for analysis.

A Coffey engineering geologist monitored the fieldwork on a full-time basis and recorded an engineering log of the subsurface profile observed at each location.

Water level readings have been made in the drill holes at times and under conditions stated on the borehole logs. In cored boreholes, water was used as a drilling fluid and groundwater levels could not be monitored. It must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, and other factors.

Borehole locations were measured by tape relative to site boundaries. Test elevations were measured by staff and dumpy level to a datum of 162.54m AHD located within the hospital grounds.

Engineering logs of the boreholes are presented in Appendix A, together with colour core photographs and Explanation Sheets defining the terms and symbols used.

3.1.2 Building 4 Assessment

A site visit to Building 4 was carried out on 28 March 2008. The brick building is generally three stories high with a basement and is inter connected to new structures along the north western and south western walls. The assessment involved walking through the existing building and looking at the existing footings through access doors in the basement. The assessment took into consideration the following:

- Construction materials used in existing structure.
- Condition assessment of the walls and floors of the structure.
- Assessment of topography surrounding the building.
- Assessment of the footings for the existing building.

3.2 Laboratory Testing

Six soaked CBR tests were carried out on bulk samples obtained from CBH7, CBH10, CBH11, CBH14, CBH15 and CBH18. Six samples from CBH1, CBH8, CBH12, CBH13, CBH15 and CBH16 were tested for pH, sulphate and chloride content.

The results of the CBR, pH, Sulphate and Chloride content tests are presented in Appendix C.

Rock point load strength index tests were carried out on rock core and the results are presented on the engineering logs.

4 RESULTS OF THE INVESTIGATION

4.1 Site Descriptions

4.1.1 Building 1

The proposed Building 1 site is located along the western perimeter of the hospital where currently a level car park is situated. The land adjacent to the car park generally slopes downwards to the west, with the car park having been cut into the slope along the eastern and filled along the western boundaries respectively. The fill was estimated to be 2m high at the north western end of the car park. Batter angles of 18° and 19° were measured for the cut and fill sections respectively using a hand held clinometer.

To the west of the car park was a well maintained grassed strip of land approximately 20m wide. Further west the land falls sharply and the vegetation consists of bushes and mature trees.

4.1.2 Building 2

The proposed Building 2 site is located along the central northern perimeter of the hospital where a car park is situated. In this area, the land falls to the north at an angle of 3° to 4° with the car park terraced over 3 levels to accommodate the slope. There was minor cut and fill earthworks estimated at 1m height associated with the terracing. The eastern end of the car park is lower than the western end and has been filled where a former gully was located.

Adjacent to the north west of the car park is a grassed drainage basin. The basin is approximately 2m deep and in the base is a galvanised steel grill probably associated with a drainage system. Beyond the basin the land slopes downwards to the north towards Coups Creek where dense vegetation is present.

4.1.3 Building 3

The detail and location of proposed Building 3 was not finalised at the time this report was prepared, however we understand it is to be located adjacent and to the south of the proposed Building 1 site. In this area is a grassed drainage basin similar to that found in the Building 2 area. The basin is 2m deep and has a galvanised steel grill and manhole in the base. At the western end of the basin is a 6m wide well maintained grassed crest. Beyond this, the land falls at an angle of approximately 18° to the west and is vegetated with thick grass. At the base of the slope are mature trees and bushes. Fragments of broken brick observed on the surface at the northern end of the basin suggest that the basin walls may have been constructed using fill material.

Adjacent to the south of the basin is a car park. The south western end of the car park has been raised approximately 1.5m above the surrounding ground level. To the east of the basin are two single storey buildings. An in-ground swimming pool is located to the northeast of the basin.

4.1.4 Building 4

Building 4 is an existing three storey brick structure located in the eastern area of the hospital. The building has a basement along its south eastern side and is inter-connected to new structures along the north western and south western walls. The land surrounding the building generally slopes down to the east.

TABLE 1: SUBSURFACE PROFILE AT TEST LOCATIONS AND GEOTECHNICAL MODEL

Unit	Description	Thickness of Unit (m) ⁽¹⁾	R.L. Top of Layer (m AHD) ⁽¹⁾
Unit 1 – Fill	Bitumen and Roadbase for boreholes excavated in car parks overlying silty sand, clayey sand, sandy clay and clay, with some sandstone gravel up to cobbles size, concrete rubble, organic fragments and tree roots.	0.2 to 6.8	156.5 to 162.9
Unit 2 – Residual	Typically <ul style="list-style-type: none"> Sandy Clay and Clay: stiff, low to high plasticity, orange brown, pale grey and red Silty Sand and Sand: fine to medium grained, brownish grey 	0 to 1.2	154.2 to 162.7
Unit 3 – Sandstone	Unit 3A typically: <ul style="list-style-type: none"> Very low to medium strength, yellow, red, orange, grey, extremely to moderately weathered Class V and IV sandstone⁽²⁾ 	0 to 3.7	151.8 to 162.2
	Unit 3B typically: <ul style="list-style-type: none"> Medium to high strength, grey, yellow, orange, red and brown, moderately weathered to fresh Class I, II or better sandstone⁽²⁾ 	-	149.7 to 161.0
Unit 4 – Shale	Found only beneath Building 4. Very low to medium strength, highly to moderately weathered, grey and orange shale. Estimate Class IV shale ⁽²⁾	-	Not measured

Notes:

- (1) The unit thickness and base of unit values are based on the boreholes and may not represent the extremes (maximum or minimum) values across the site.
- (2) Rock classified in accordance with Pells *et al* (1998) "Foundations on Sandstone and Shale in the Sydney Region" Aust. Geomech. Jnl, Dec 1998.

western end up to 3.14m (within CBH17) at the eastern end. The fill consists of Clay, Sandy Clay, Sand, Silty Sand and Clayey Sand. In the absence of fill placement records and compaction control test results, the fill should be considered to be uncontrolled.

The level of the base of proposed Building 2 was not defined at the time this report was compiled. With the depth to sandstone varying from 0.6m to 3.6m below current surface levels, the base level of the proposed structure may lie within both soil and rock. With foundations spanning rock and soil there is a greater potential for differential settlements, compared to rock foundations. To avoid possible problems with differential settlement we recommend that building loads such as basement retaining walls and column loads be supported on rock. Strip, pad footings or bored piers could be adopted, depending on the bulk excavation levels and the depth to bedrock. Figure 5 shows cross sections through the site with inferred rock levels.

5.3 Building 3

The subsurface conditions across the Building 3 site consist of a relatively thick layer of fill overlying either a thin layer of residual soil or bearing directly on sandstone. Fill thickness varies from 2.7m (within CBH7) at the north eastern area of the proposed structure to 6.8m (within CBH18) at the south western end. The fill consists of Clay, Sandy Clay, Sand, Silty Sand and Clayey Sand. In the absence of fill placement records and compaction control test results, the fill should be considered to be uncontrolled.

Uncontrolled fill is not suitable for supporting building loads and as such, we recommend building loads be supported on rock using either piled footings or a shallow footing system. Strip, pad footings or bored piers could be adopted, depending on the bulk excavation levels and the depth to bedrock. Figure 6 shows cross sections through the site with inferred rock levels.

The proposed Building 3 may contain a three storey basement and as such will require retaining structures as part of the development. Retaining structures may take the form of a soldier piled wall with timber infill panels or shotcrete panels, although groundwater seepage could cause ground loss, requiring careful construction with infill panels being constructed in relatively short depth increments. Alternatively, contiguous piles could be used with provision for grouting between piles in the event that seepage and ground loss occurs between piles.

5.4 Building 4

Improvements to Building 4 will consist of modifications to load bearing internal walls within the eastern corner of the existing structure. Based on site observations, shale was observed beneath the existing concrete ground floor slab in the area where the improvements are proposed.

We recommend an allowable bearing pressure for the shale exposed beneath Building 4 of 1000kPa. Footings should be embedded at least 0.3m into the rock and the base cleaned of debris.

The existing basement in the eastern corner of the building was cut into the shale creating a near vertical unsupported rock cutting up to approximately 2m high in places. New footings for load bearing walls will need to be placed a distance of at least 2 footing widths from the edge of any rock cutting. If this is not feasible, our preference would be to excavate the shale to the base of the existing cut and extend the footing. Alternatively, a reduction in the allowable bearing pressure to 600kPa and an inspection by a geotechnical engineer to observe the condition of the near vertical rock face will be

required. Following the inspection, further recommendations such as the removal of any loose rock, placement of rock dowels or shotcreting of exposed face may be required.

Settlement of footings should be less than 1% of the least footing dimension.

5.5 Site Preparation and Excavation Conditions

If fill is used to support structures or pavements it will need to be excavated and re-compacted if suitable, or replaced with an imported fill. Re-compacted clayey sands, sandy clays or imported granular fills that are to support floor slabs or pavements should be placed and compacted in maximum 200mm thick layers to at least 98% Standard Density Ratio at a moisture content within $\pm 2\%$ of Standard Optimum Moisture Content. Fill within 0.5m of pavement subgrade level should be compacted to at least 100% Standard Density Ratio.

Soils should be readily excavated using a tracked loader. The upper weathered sandstone bedrock is likely to be able to be excavated using a tracked excavator. The less weathered sandstone at depth will require ripping or the use of an impact hammer. Contractors should be provided with the borehole logs and core photographs and be required to make their own assessment of the suitability and productivity of specific plant.

5.6 Dewatering

Groundwater seepage was observed in three boreholes within the proposed Building 3 area during the investigation at ground levels varying from 153mAHD to 156.7mAHD. No groundwater seepage was observed in the other boreholes during the investigation, however, due to water being used as a drilling medium during rock coring, groundwater maybe present in excavations. Dewatering, if required, should be able to be achieved using standard sump and pump methods.

5.7 Support Requirements

5.7.1 Cut and Fill Batters and Slope Stability Issues

Excavations within compacted fill and residual soils are likely to stand temporarily at relatively steep slopes (between 1H:1V and 1.5H:1V). Such batters will be of marginal stability and are likely to suffer instability, particularly in wet weather. We recommend that allowance be made for laying back temporary excavations at 1.5H:1V where there is limited access required to the base of the excavation or 2H:1V where workers require access. Surcharge loads should be kept well clear of the crest of cuts.

A batter angle of 26° (approximately 2H:1V) is recommended for permanent works. Retaining walls will be required where there is insufficient room to form unsupported batters.

5.7.2 Retaining Structures

Preliminary sketches of the proposed Building 1 car park show retaining structures associated with cut and fill earthworks. Buildings 2 and 3 are also likely to require retaining structures.

Where retaining walls are cantilevered or supported by a single row of anchors, and some wall movements can be tolerated, walls can be designed assuming a triangular earth pressure distribution using an earth pressure coefficient, K , of 0.4. A bulk unit weight of 20kN/m^3 should be assumed for Unit 1 and 2 materials. For weathered rock a bulk unit weight of 22kN/m^3 is recommended. Passive

pressure coefficients, K_p , of 2.5 may be assumed for the Unit 1 Fill and Unit 2 Residual Soil. A passive pressure coefficient, K_p , of 3.7 may be assumed for Unit 3A extremely weathered sandstone bedrock.

Lateral and vertical ground movements will be dependent on the design and construction of the retention system. For example, the use of higher earth pressure coefficients, tie-back anchor loads and stiffer walls will reduce lateral deflections.

Minimum wall movements of about 1% of retained wall height are required to cause the earth pressure coefficient to reduce to the active condition. Vertical movements could be expected to be of a similar order to the lateral movements. The extent of the horizontal movement behind the excavation face is typically between 1.5 and 3 times the excavated height.

Where ground anchors restrain retaining wall movement, or where significant movements cannot be tolerated, higher earth pressure coefficients should be adopted. We recommend an earth pressure coefficient of 0.5 for propped or anchored retaining walls where movements are restrained. However, it should be understood that walls designed for this higher coefficient would still undergo some lateral movements, depending on the nature of the wall and the construction sequences. To assess the extent of lateral movements, a detailed soil structure analysis (using programmes such as WALLAP) should be undertaken.

For preliminary design of retaining walls, which are anchored or strutted at several levels, design can be based on the trapezoidal earth pressure distribution as shown in Table 2.

TABLE 2: TRAPEZOIDAL PRESSURE DISTRIBUTION

Depth (m)	Horizontal Pressure (kPa)
0	$K_p p_s$
0.25 H	$K (0.8 \gamma H + p_s)$
0.75 H	$K (0.8 \gamma H + p_s)$
H	$K_p p_t$

Where:

K = Earth pressure coefficient which depends upon material type; whether movement needs to be limited as discussed above.

p_s = Design surcharge pressure (kPa).

H = Thickness of layer being retained (m).

γ = Unit weight (kN/m^3)

Hydrostatic pressures should be added to earth pressures unless walls can be provided with effective drainage, and pressures due to adjacent footings will also need to be taken into account. The above pressures assume level ground above the retaining wall. Surcharge loads should be added to earth pressures, as appropriate.

For the preliminary design of anchors, an allowable bond stress of 800kPa may be adopted for Class III or better (Unit 3B) sandstone where anchors have a bond length of between 3m and 7m in medium strength sandstone. Anchors should be checked for an anchor pullout failure mechanism assuming a 45° failure cone in addition to bond strength.

Where structures sensitive to ground movements lie close to the site, dilapidation surveys should be carried out prior to excavation. Numerical analysis should be carried out to assess the potential ground movement and interaction with the shoring wall design to control deflection to tolerable limits. Survey monitoring should also be carried out to confirm that movements are within the predicted range.

5.7.3 Vertical Excavations In Rock

Provision for the installation of support will be required where vertical excavations are made in rock. Specific rock support requirements in un-shored sections of excavations can only be assessed during excavation. An experienced geotechnical engineer/engineering geologist should carry out regular inspections as excavation progresses (at least every 2m depth of excavation). For preliminary design purposes the support guidelines presented in table 3 are recommended:

TABLE 3: VERTICAL EXCAVATION FACE SUPPORT REQUIREMENTS

Rock Class	Support
Class V and IV Sandstone (Unit 3A)	<ul style="list-style-type: none"> Shoring wall; or Anchors or Soil Nails, mesh supported by 0.5m long dowels and shotcrete (minimum 75 mm thick) or fibre reinforced shotcrete of fractured zones below shoring walls.
Class III Sandstone or better (Unit 3B)	<ul style="list-style-type: none"> Generally only isolated rock bolting to support potentially unstable wedges. Localised pattern rock bolting, mesh supported by 0.5m long dowels and shotcrete (minimum 75 mm thick) or fibre reinforced shotcrete of fractured zones. (Within CBH16, a 0.6m thick clay seam was observed at approximately 52mAHD which will likely require shotcrete and dowel support)

Where long-term support is required below the site retention system, anchors and rock bolts must be provided with a high level of corrosion protection if they cannot be maintained (i.e. inspected and replaced, if necessary). Stainless steel bolts or multiple layers of corrosion protection such as encapsulating plain or galvanised bolts in both grout and PVC sheaths may be required.

5.8 Foundations

Foundation design parameters for sandstone are provided in Table 4.

Open bored piles should be practical, although dewatering and temporary liners may be required for drilling in sand and/or if groundwater is encountered.

TABLE 4: ROCK FOUNDATION DESIGN PARAMETERS

Unit	Allowable Shaft Adhesion (kPa) ^(a)	Allowable Bearing Pressure (kPa) ^(b)
Unit 3A Class V and Class IV Sandstone	100	1000
Unit 3B Class III Sandstone or better	350	2000 – 5000 ^(c)

Note: (a) Assumes minimum embedment of 3 pile diameters into the relevant stratum
 (b) Assumes a minimum embedment of 0.3m into the relevant bearing stratum.
 (c) Value dependant on level of assessment carried out during construction (see Table 5).

For uplift capacity, the shaft adhesion should be multiplied by 0.6. In addition to shaft adhesion, the uplift capacity should be checked for a cone pullout failure mode assuming a cone angle of 70° considering the submerged weight of the soil or rock and adopting a factor of safety of 1 against pullout.

An experienced geotechnical engineer should observe the boring of the piles in order to assess the rock levels and to confirm the rock is suitable for the adopted design parameters. Within CBH10, located in the south eastern corner of proposed Building 3, a 0.6m thick clay seam was observed within the Unit 3B sandstone at a depth of approximately 9m below existing ground level. We recommend bored footings be carried through this seam. Where footings are designed to bear directly onto bedrock, the footing inspection and assessment requirements are provided in Table 5.

Footings designed using the parameters presented in Table 4 should result in settlements less than 1% of the footing width or diameter.

TABLE 5: FOOTING INSPECTION AND ASSESSMENT REQUIREMENTS

Rock Unit	Testing Requirements
Unit 3A	<ul style="list-style-type: none"> • Visual inspection of all pad footings • Observation of piling and correlation with borehole information
Unit 3B Design Bearing Pressure up to 2,000kPa	<ul style="list-style-type: none"> • Visual inspection of all pad footings • Observation of piling and correlation with borehole information
Unit 3B Design Bearing Pressure greater than 2,000kPa	<ul style="list-style-type: none"> • Visual inspection of all pad footings • Observation of piling and correlation with borehole information • Spoon testing or coring of at least 1/3 of footing locations

5.9 Pavement Design

CBR testing on potential subgrade soils for road pavements indicate values ranging from 2% to 10%. For design purposes, we recommend a CBR value of 2% be adopted subject to confirmation by a geotechnical engineer during construction.

Pavement areas should be prepared by:

- Stripping all topsoil.
- Stripping all fill. Where fill is exposed at a depth of 1m below proposed subgrade level, remove to this level and proof roll in the presence of an experienced geotechnical engineer with a minimum of 6 passes of a smooth drum, 10 tonne roller. Soft or heaving areas will require further excavation and replacement.
- For other areas, proof roll at subgrade level with a minimum of 6 passes of a smooth drum, 10 tonne roller.
- Remove and replace soft or heaving areas.

5.10 Soil Aggressivity

Test results from Building 1 and 3 sites indicate that the fill and natural soils are not highly acidic and have low sulphate and chloride concentrations. Within the Building 2 site, all soils are mildly acidic, with pH values of 4.7 and 5.5, however, the tested sulphate and chloride concentrations were low. In consideration of this, we recommend a non-aggressive exposure classification in accordance with AS 2159-1995 for concrete in contact with all soils across the site.

5.11 Earthquake Loading Factor

Based on Australian Standard AS 1170.4-2007, *Structural Design Actions – Part 4: Earthquake Actions in Australia*, the site is assessed as having a sub soil class C_e – Shallow soil site.

6 LIMITATIONS

The findings within this report are the result of discrete/specific investigations methodologies used in accordance with normal practices and standards. Subsurface conditions can change over relatively short distances and the subsurface conditions revealed at the test locations may not be representative of subsurface conditions across the site. We recommend that a geotechnical engineer be engaged during construction to confirm the subsurface conditions are consistent with design assumptions.

Retaining wall design is complex and detailed soil structure interaction analysis may be required to assess shear stresses, bending moments and anchor loads in retaining walls. Coffey would be happy to assist in a detailed analysis of retaining walls for basements.

The reader's attention is drawn to the attached document entitled 'Important Information about your Coffey Report', which presents additional information on the uses and limitations of this report.

For and on behalf of Coffey Geotechnics Pty Ltd



Peter Waddell

Principal Geotechnical Engineer

Important information about your Coffey Report

As a client of Coffey you should know that site subsurface conditions cause more construction problems than any other factor. These notes have been prepared by Coffey to help you interpret and understand the limitations of your report.

Your report is based on project specific criteria

Your report has been developed on the basis of your unique project specific requirements as understood by Coffey and applies only to the site investigated. Project criteria typically include the general nature of the project; its size and configuration; the location of any structures on the site; other site improvements; the presence of underground utilities; and the additional risk imposed by scope-of-service limitations imposed by the client. Your report should not be used if there are any changes to the project without first asking Coffey to assess how factors that changed subsequent to the date of the report affect the report's recommendations. Coffey cannot accept responsibility for problems that may occur due to changed factors if they are not consulted.

Subsurface conditions can change

Subsurface conditions are created by natural processes and the activity of man. For example, water levels can vary with time, fill may be placed on a site and pollutants may migrate with time. Because a report is based on conditions which existed at the time of subsurface exploration, decisions should not be based on a report whose adequacy may have been affected by time. Consult Coffey to be advised how time may have impacted on the project.

Interpretation of factual data

Site assessment identifies actual subsurface conditions only at those points where samples are taken and when they are taken. Data derived from literature and external data source review, sampling and subsequent laboratory testing are interpreted by geologists, engineers or scientists to provide an opinion about overall site conditions, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist, because no professional, no matter how qualified, can reveal what is hidden by

earth, rock and time. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. For this reason, owners should retain the services of Coffey through the development stage, to identify variances, conduct additional tests if required, and recommend solutions to problems encountered on site.

Your report will only give preliminary recommendations

Your report is based on the assumption that the site conditions as revealed through selective point sampling are indicative of actual conditions throughout an area. This assumption cannot be substantiated until project implementation has commenced and therefore your report recommendations can only be regarded as preliminary. Only Coffey, who prepared the report, is fully familiar with the background information needed to assess whether or not the report's recommendations are valid and whether or not changes should be considered as the project develops. If another party undertakes the implementation of the recommendations of this report there is a risk that the report will be misinterpreted and Coffey cannot be held responsible for such misinterpretation.

Your report is prepared for specific purposes and persons

To avoid misuse of the information contained in your report it is recommended that you confer with Coffey before passing your report on to another party who may not be familiar with the background and the purpose of the report. Your report should not be applied to any project other than that originally specified at the time the report was issued.

Important information about your **Coffey Report**

Interpretation by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a report. To help avoid misinterpretations, retain Coffey to work with other project design professionals who are affected by the report. Have Coffey explain the report implications to design professionals affected by them and then review plans and specifications produced to see how they incorporate the report findings.

Data should not be separated from the report*

The report as a whole presents the findings of the site assessment and the report should not be copied in part or altered in any way.

Logs, figures, drawings, etc. are customarily included in our reports and are developed by scientists, engineers or geologists based on their interpretation of field logs (assembled by field personnel) and laboratory evaluation of field samples. These logs etc. should not under any circumstances be redrawn for inclusion in other documents or separated from the report in any way.

Geoenvironmental concerns are not at issue

Your report is not likely to relate any findings, conclusions, or recommendations about the potential for hazardous materials existing at the site unless specifically required to do so by the client. Specialist equipment, techniques, and personnel are used to perform a geoenvironmental assessment. Contamination can create major health, safety and environmental risks. If you have no information about the potential for your site to be contaminated or create an environmental hazard, you are advised to contact Coffey for information relating to geoenvironmental issues.

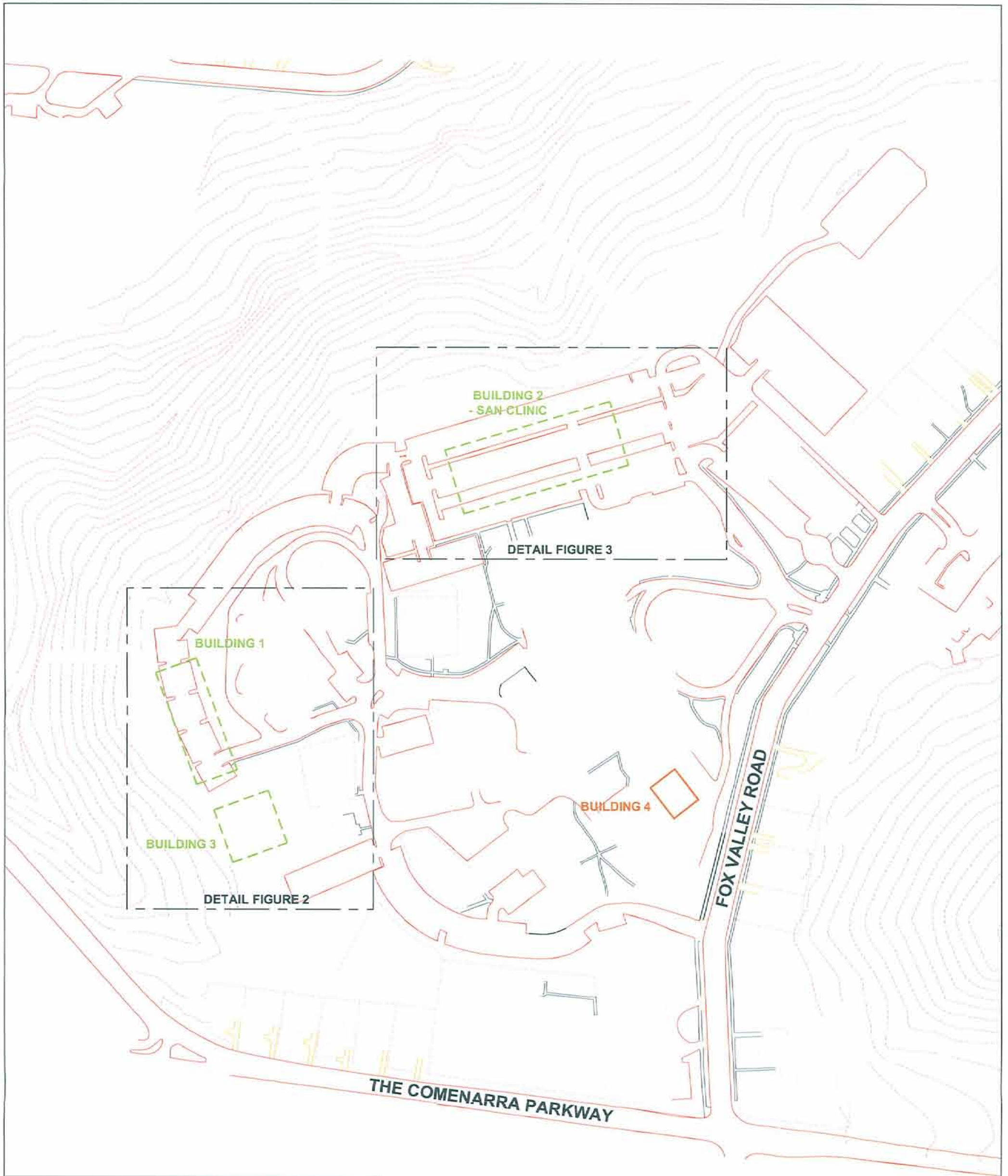
Rely on Coffey for additional assistance

Coffey is familiar with a variety of techniques and approaches that can be used to help reduce risks for all parties to a project, from design to construction. It is common that not all approaches will be necessarily dealt with in your site assessment report due to concepts proposed at that time. As the project progresses through design towards construction, speak with Coffey to develop alternative approaches to problems that may be of genuine benefit both in time and cost.

Responsibility

Reporting relies on interpretation of factual information based on judgement and opinion and has a level of uncertainty attached to it, which is far less exact than the design disciplines. This has often resulted in claims being lodged against consultants, which are unfounded. To help prevent this problem, a number of clauses have been developed for use in contracts, reports and other documents. Responsibility clauses do not transfer appropriate liabilities from Coffey to other parties but are included to identify where Coffey's responsibilities begin and end. Their use is intended to help all parties involved to recognise their individual responsibilities. Read all documents from Coffey closely and do not hesitate to ask any questions you may have.

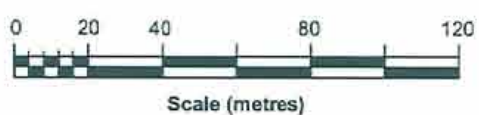
* For further information on this aspect reference should be made to "Guidelines for the Provision of Geotechnical Information in Construction Contracts" published by the Institution of Engineers Australia, National Headquarters, Canberra, 1987.



LEGEND:

--- PROPOSED BUILDING
(LOCATIONS TO BE CONFIRMED)

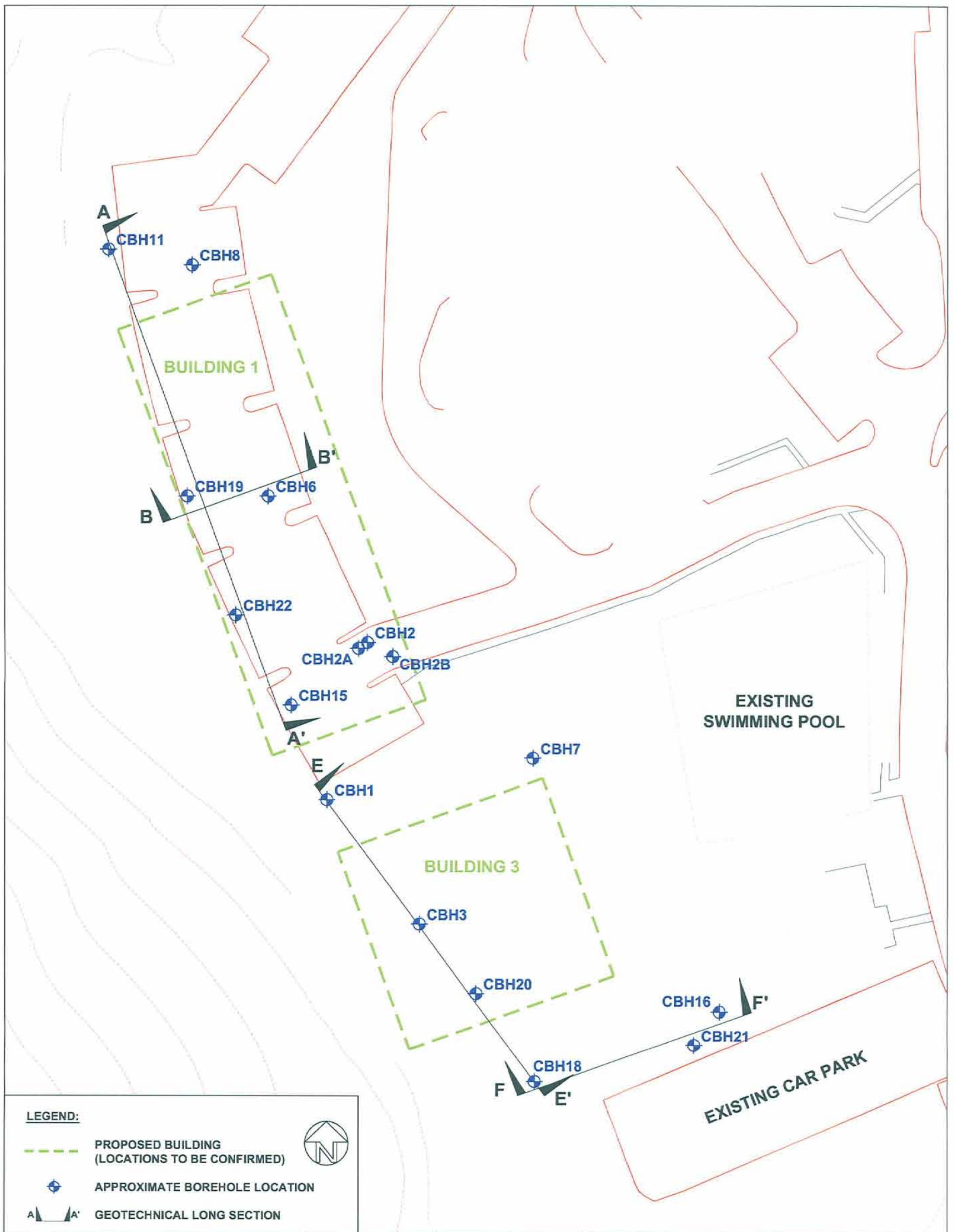
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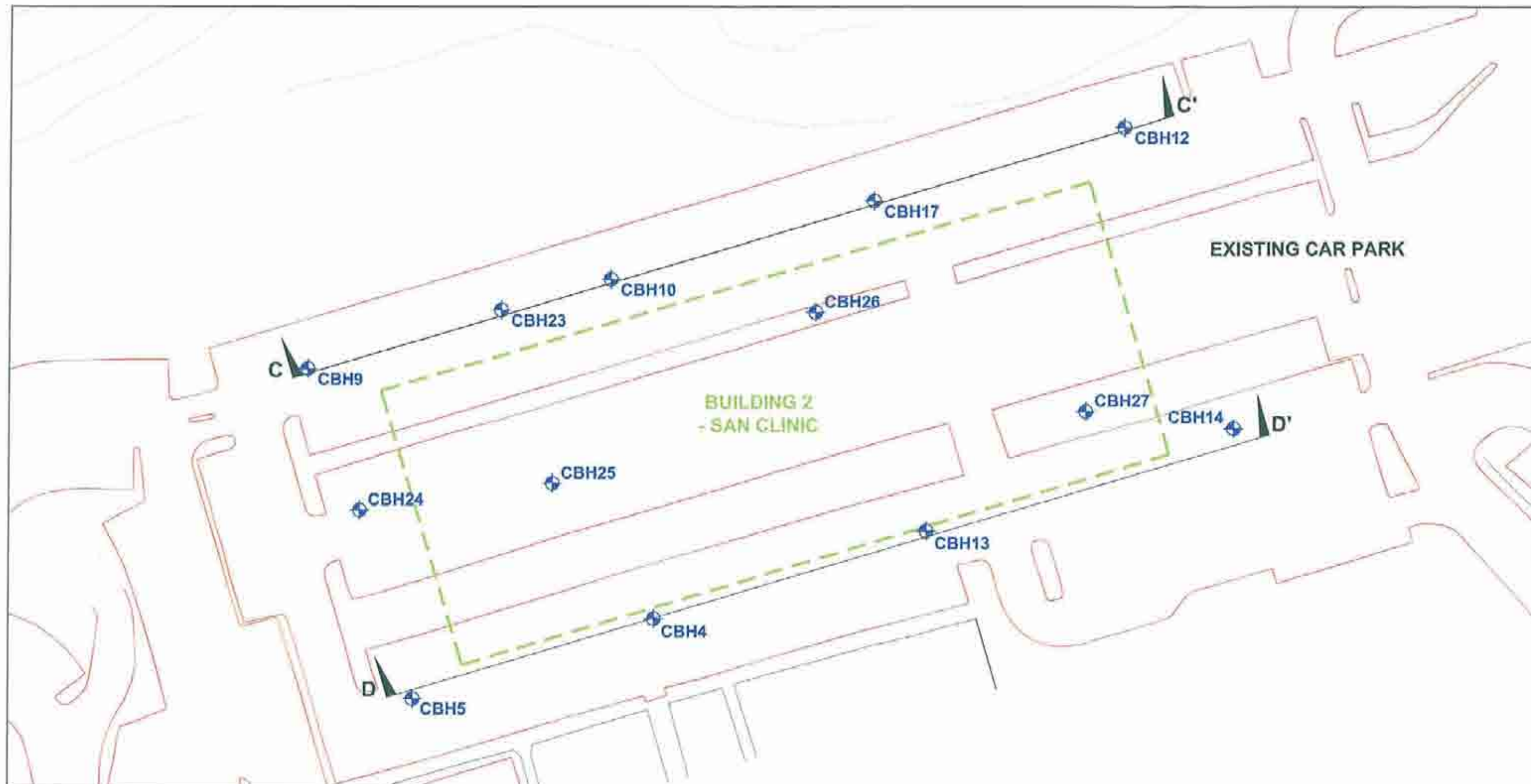
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approved	<i>PSW</i>
date	<i>4/11/2008</i>
scale	1:2000
original size	A3

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geotechnics
SPECIALISTS MANAGING
THE EARTH

client:	TAYLOR THOMSON WHITTING	
project:	GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL FOX VALLEY ROAD, WAHROONGA, NSW	
title:	SITE PLAN	
project no:	GEOTLCOV23462AA	figure no: FIGURE 1

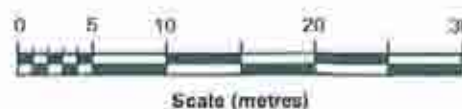


<div> <div>drawn</div> <div>SH/LT</div> </div>	<div> <div>client:</div> <div>TAYLOR THOMSON WHITTING</div> </div>	
<div> <div>approved</div> <div><i>PSW</i></div> </div>	<div> <div>project:</div> <div>GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL FOX VALLEY ROAD, WAHROONGA, NSW</div> </div>	
<div> <div>date</div> <div>1/4/2008</div> </div>	<div> <div>title:</div> <div>DETAILED PLAN OF BUILDING 1 / 3 SHOWING BOREHOLE LOCATIONS</div> </div>	
<div> <div>scale</div> <div>1:500</div> </div>	<div> <div>project no:</div> <div>GEOTLCOV23462AA</div> </div>	
<div> <div>original size</div> <div>A3</div> </div>	<div> <div>figure no:</div> <div>FIGURE 2</div> </div>	



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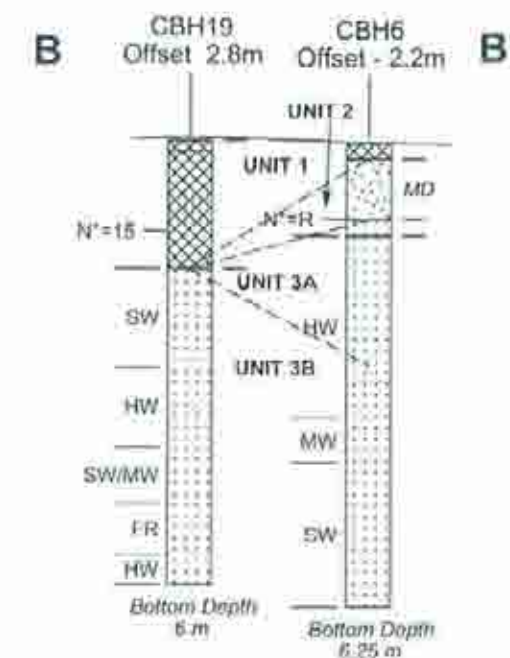
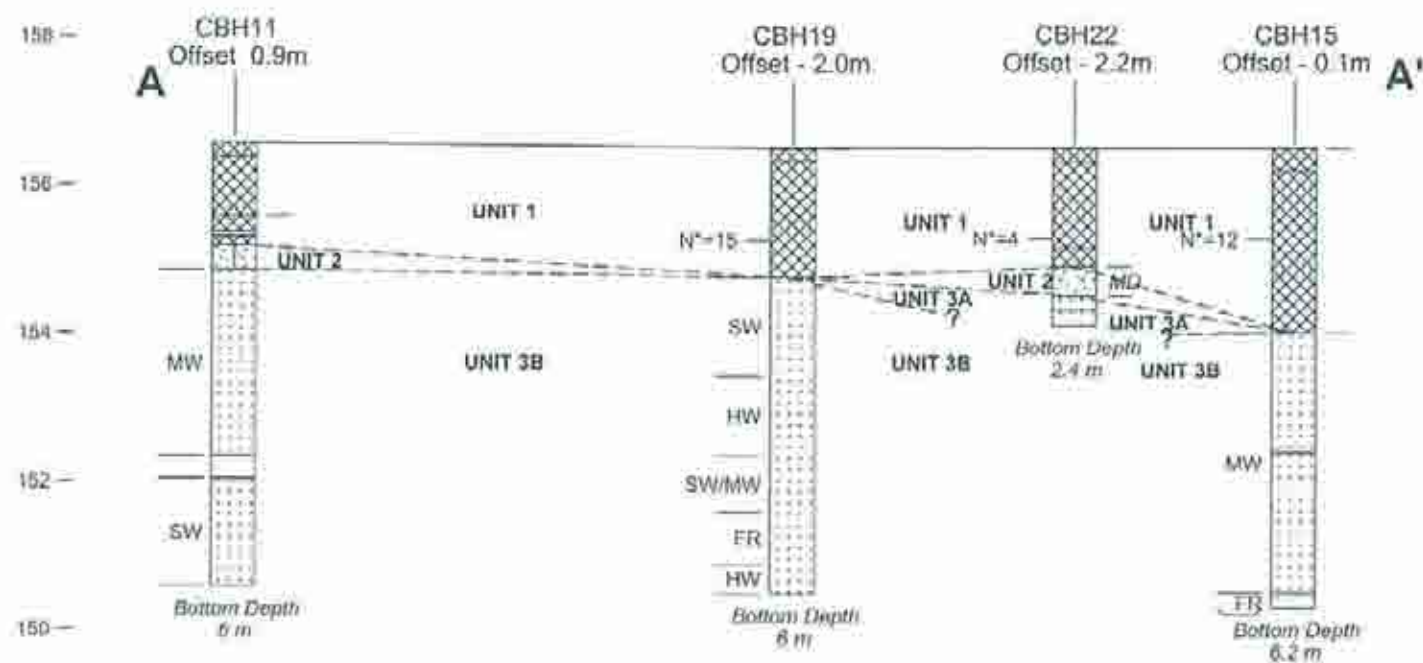
- PROPOSED BUILDING
(LOCATIONS TO BE CONFIRMED)
- APPROXIMATE BOREHOLE LOCATION
- A—A' GEOTECHNICAL LONG SECTION



drawn	SH/LT
approved	<i>[Signature]</i>
date	4/4/2020
scale	1:500
original size	A3

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geotechnics
SPECIALISTS MANAGING
THE EARTH

client:	TAYLOR THOMSON WHITTING	
project:	GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL FOX VALLEY ROAD, WAHROONGA, NSW	
title:	DETAILED PLAN OF BUILDING 2 SHOWING BOREHOLE LOCATIONS	
project no:	GEOTLCOV23462AA	figure no: FIGURE 3

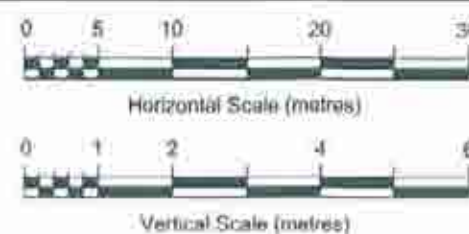


LEGEND

- FILL
- SILTY SAND
- SAND
- SANDSTONE
- NO CORE

- IV ROCK CLASSIFICATION (PELLS ET AL, 1998)
- DX WEATHERING (SEE EXPLANATION SHEETS)
- WATER LEVEL
- N*=17 STANDARD PENETRATION TEST RESULT

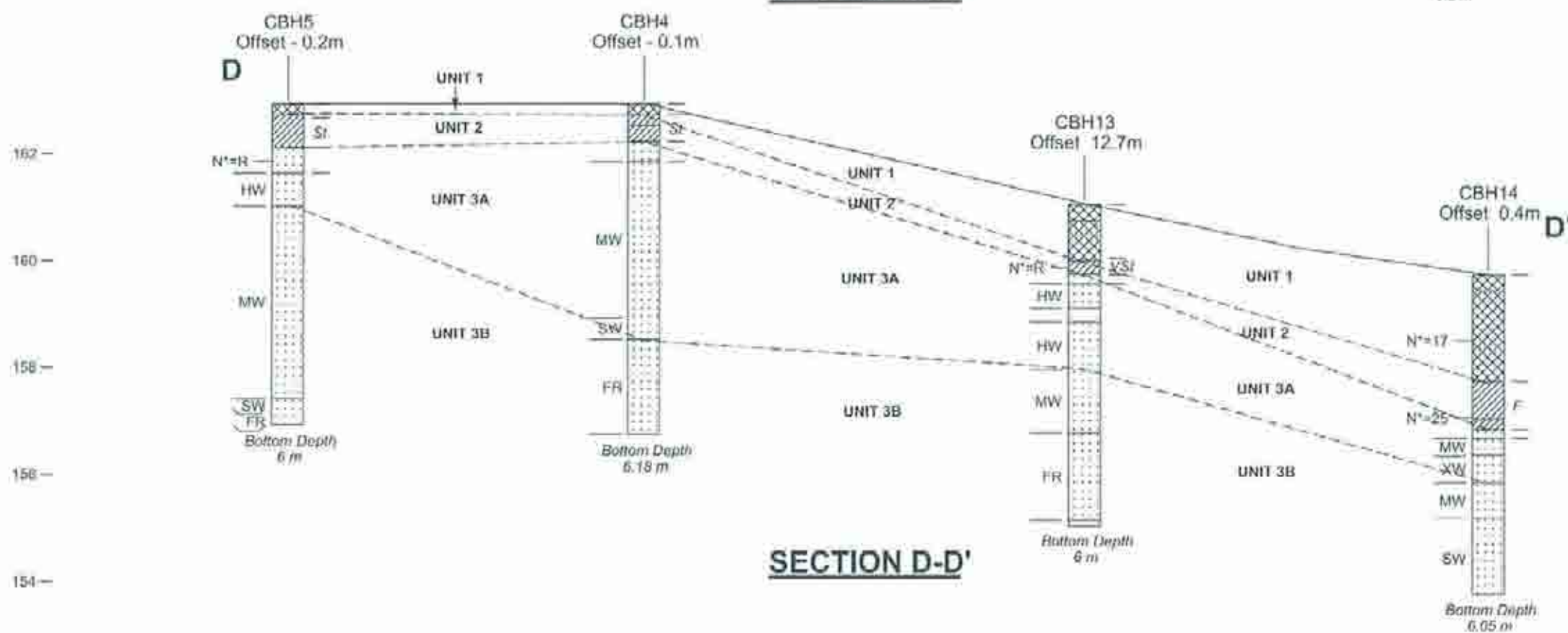
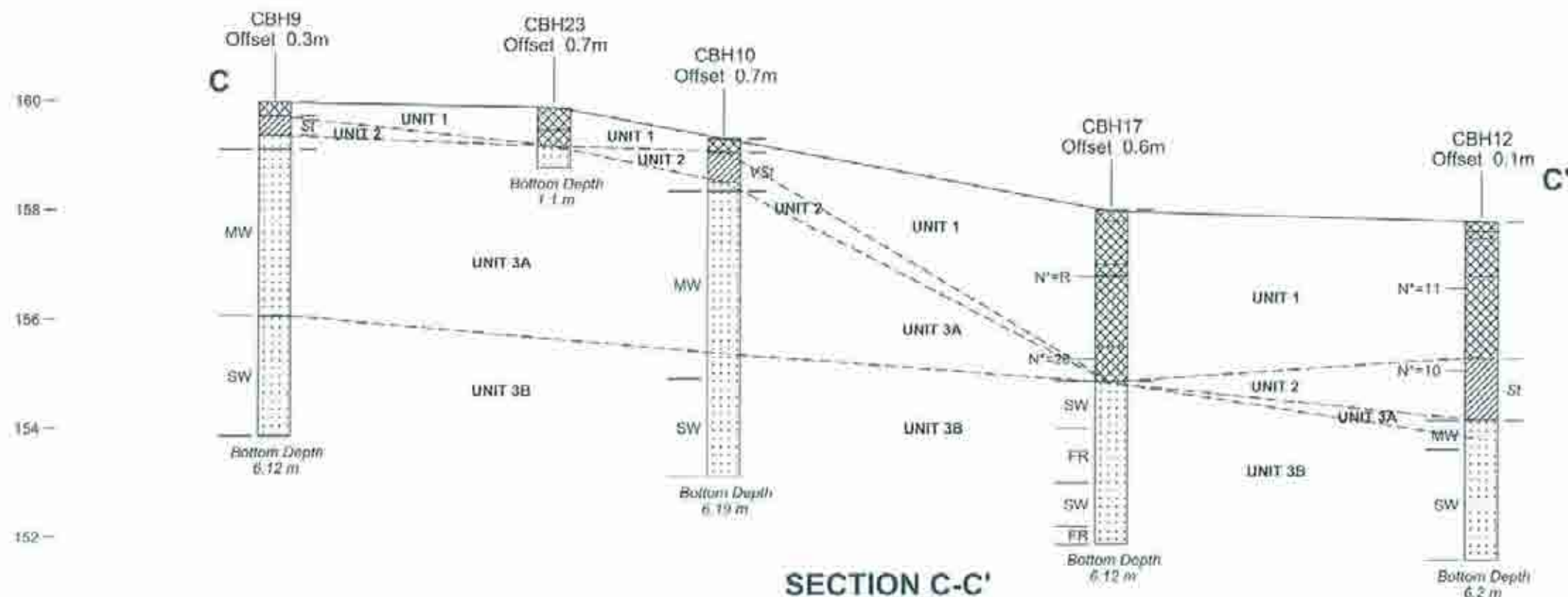
revision	description	drawn	approved	date



drawn	SHLT
approved	<i>Per</i>
date	4/9/2008
scale	AS SHOWN
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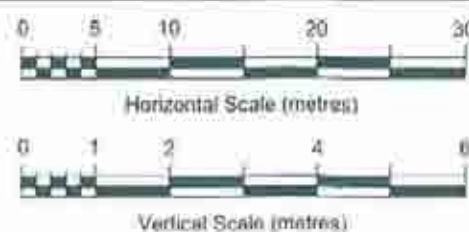
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client	TAYLOR THOMSON WHITTING
project	GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL FOX VALLEY ROAD, WAHROONGA, NSW
title	GEOTECHNICAL LONG SECTIONS A-A' AND B-B'
project no.	GEO1LCOV23462AA
drawing no.	FIGURE 4



LEGEND

- FILL
- SANDY CLAY
- CLAY
- SANDSTONE
- NO CORE
- IV** ROCK CLASSIFICATION (PELLS ET AL, 1998)
- DX** WEATHERING (SEE EXPLANATION SHEETS)
- WATER LEVEL
- N*=17** STANDARD PENETRATION TEST RESULT

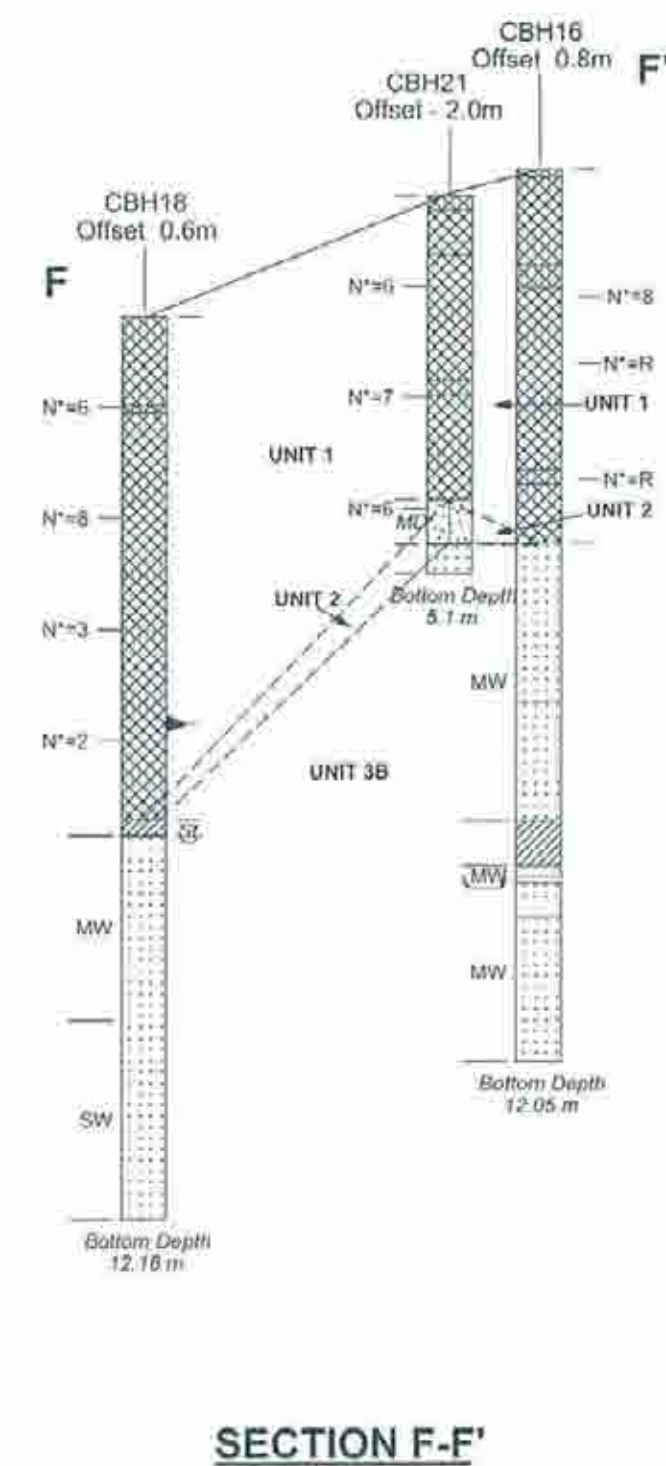
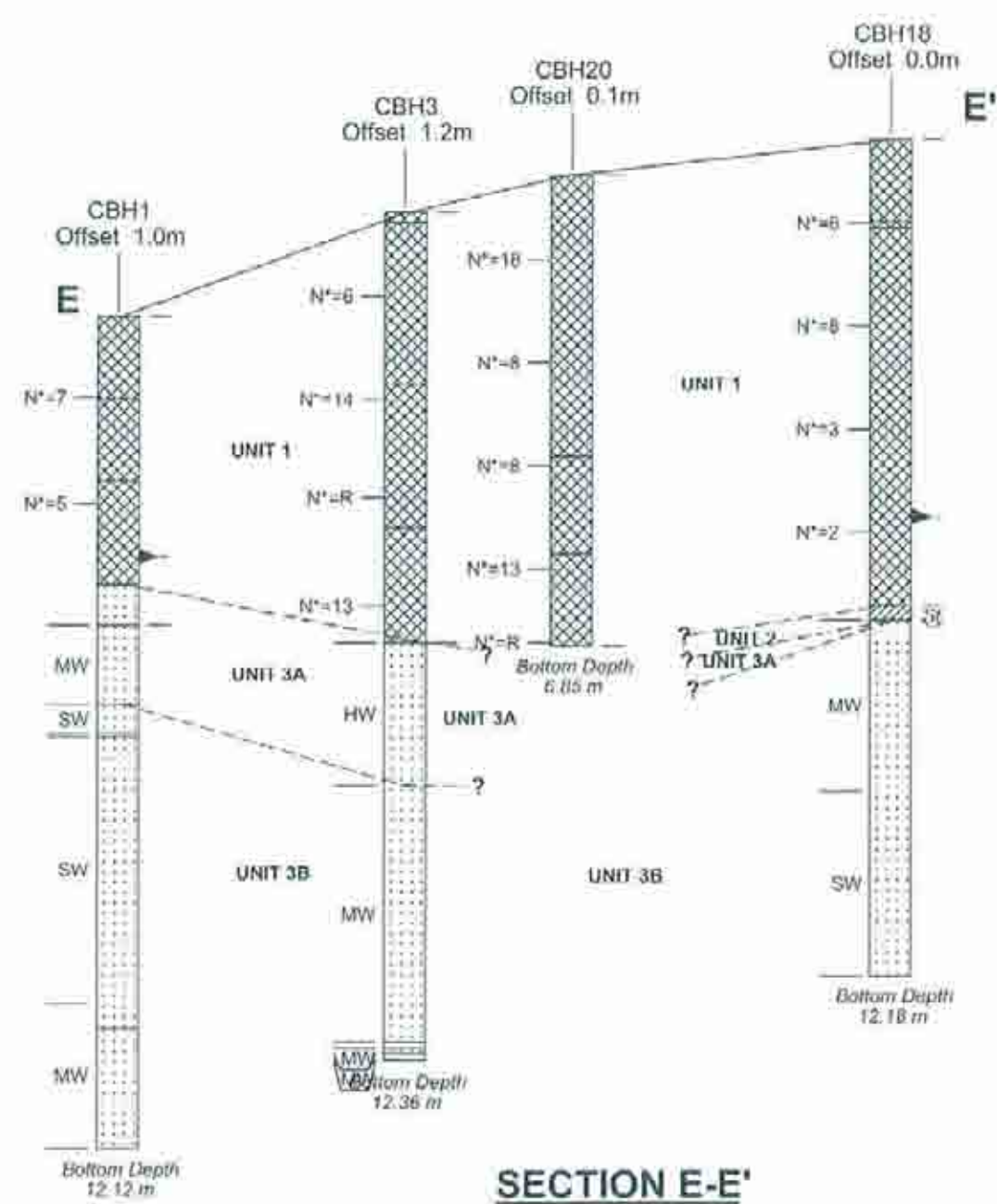


drawn SH/LT
 approved *Bm*
 date 1/4/2008
 scale AS SHOWN
 original size A3

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 geotechnics
 SPECIALISTS MANAGING
 THE EARTH

client: TAYLOR THOMSON WHITTING
 project: GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL
 FOX VALLEY ROAD, WAHROONGA, NSW
 title: GEOTECHNICAL LONG SECTIONS C-C' AND D-D'
 project no: GEOTLCOV23462AA
 drawing no: FIGURE 5

162 —
160 —
158 —
156 —
154 —
152 —
150 —
148 —
146 —
144 —
142 —



- LEGEND**
- FILL
 - CLAY
 - SANDY CLAY
 - SILTY SAND
 - SANDSTONE
 - NO CORE

- IV ROCK CLASSIFICATION (PELLS ET AL, 1998)
DX WEATHERING (SEE EXPLANATION SHEETS)
▼ WATER LEVEL
N*=17 STANDARD PENETRATION TEST RESULT

revision	description	drawn	approved	date	<div>0 5 10 20 30</div> <div>Horizontal Scale (metres)</div> <div>0 1 2 4 6</div> <div>Vertical Scale (metres)</div>	drawn	SH/LT	<div>coffey</div> <div>geotechnics</div> <div>SPECIALISTS MANAGING THE EARTH</div>	client	TAYLOR THOMSON WHITTING	
						approved	<i>[Signature]</i>		project	GEOTECHNICAL INVESTIGATION AND REPORT FOR SAN HOSPITAL FOX VALLEY ROAD, WAHRDONGA, NSW	
						date	4/4/2008		title	GEOTECHNICAL LONG SECTIONS E-E' AND F-F'	
						scale	AS SHOWN		project no.	GEOTLCOV23462AA	drawing no.
						original size	A3		FIGURE 6		

Appendix A

Engineering Borehole Logs, Core Photographs and Explanation Sheets

Soil Description Explanation Sheet (1 of 2)

DEFINITION:

In engineering terms soil includes every type of unconsolidated or partially cemented inorganic or organic material found in the ground. In practice, if the material can be remoulded or disintegrated by hand in its field condition or in water it is described as a soil. Other materials are described using rock description terms.

CLASSIFICATION SYMBOL & SOIL NAME

Soils are described in accordance with the Unified Soil Classification (USC) as shown in the table on Sheet 2

PARTICLE SIZE DESCRIPTIVE TERMS

NAME	SUBDIVISION	SIZE
Boulders		>200 mm
Cobbles		63 mm to 200 mm
Gravel	coarse	20 mm to 63 mm
	medium	6 mm to 20 mm
	fine	2.36 mm to 6 mm
Sand	coarse	600 µm to 2.36 mm
	medium	200 µm to 600 µm
	fine	75 µm to 200 µm

MOISTURE CONDITION

- Dry:** Looks and feels dry. Cohesive and cemented soils are hard, friable or powdery. Uncemented granular soils run freely through hands.
- Moist:** Soil feels cool and darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.
- Wet:** As for moist but with free water forming on bands when handled.

CONSISTENCY OF COHESIVE SOILS

TERM	UNDRAINED STRENGTH S_u (kPa)	FIELD GUIDE
Very Soft	< 15	A finger can be pushed well into the soil with little effort.
Soft	15 - 25	A finger can be pushed into the soil to about 25 mm depth.
Firm	25 - 50	The soil can be indented about 5mm with the thumb, but not penetrated.
Stiff	50 - 100	The surface of the soil can be indented with the thumb, but not penetrated.
Very Stiff	100 - 200	The surface of the soil can be marked but not indented with thumb pressure.
Hard	> 200	The surface of the soil can be marked only with the thumbnail.
Friable	-	Crumbles or powders when scraped by thumbnail.

DENSITY OF GRANULAR SOILS

TERM	DENSITY INDEX (%)
Very loose	Less than 15
Loose	15 - 35
Medium Dense	35 - 55
Dense	65 - 85
Very Dense	Greater than 85

MINOR COMPONENTS

TERM	ASSESSMENT GUIDE	PROPORTION OF MINOR COMPONENT (%)
Trace of	Presence just detectable by tool or eye, but soil properties little or no different to general properties of primary component.	Coarse grained soils: <5% Fine grained soils: <15%
With some	Presence easily detected by tool or eye, soil properties little different to general properties of primary component.	Coarse grained soils: 5 - 12% Fine grained soils: 15 - 30%

SOIL STRUCTURE

ZONING		CEMENTING	
Layers	Continuous across exposure or sample.	Weakly cemented	Easily broken up by hand in air or water.
Lenses	Discontinuous layers of lentic shapes.	Moderately cemented	Effort is required to break up the soil by hand in air or water.
Pockets	Irregular inclusions of different material.		

GEOLOGICAL ORIGIN

WEATHERED IN PLACE SOILS

- Extremely weathered material:** Structure and fabric of parent rock visible.
- Residual soil:** Structure and fabric of parent rock not visible.

TRANSPORTED SOILS

- Aeolian soil:** Deposited by wind.
- Alluvial soil:** Deposited by streams and rivers.
- Colluvial soil:** Deposited on slopes (transported downslope by gravity).
- Fill:** Man made deposit. Fill may be significantly more variable between tested locations than naturally occurring soils.
- Lacustrine soil:** Deposited by lakes.
- Marine soil:** Deposited in ocean basins, bays, beaches and estuaries.









Soil Description Explanation Sheet (2 of 2)

SOIL CLASSIFICATION INCLUDING IDENTIFICATION AND DESCRIPTION

FIELD IDENTIFICATION PROCEDURES (Excluding particles larger than 60 mm and basing fractions on estimated mass)				USC	PRIMARY NAME	
COARSE GRAINED SOILS More than 50% of materials less than 63 mm is larger than 0.075 mm	GRAVELS More than half of coarse fraction is larger than 2.0 mm	CLEAN GRAVELS (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate particle sizes.	GW	GRAVEL	
			Predominantly one size or a range of sizes with more intermediate sizes missing.	GP	GRAVEL	
		GRAVELS WITH FINES (Appreciable amount of fines)	Non-plastic fines (for identification procedures see ML below)	GM	SILTY GRAVEL	
			Plastic fines (for identification procedures see CL below)	GC	CLAYEY GRAVEL	
	SANDS More than half of coarse fraction is smaller than 2.0 mm	CLEAN SANDS (Little or no fines)	Wide range in grain sizes and substantial amounts of all intermediate sizes missing	SW	SAND	
			Predominantly one size or a range of sizes with some intermediate sizes missing.	SP	SAND	
		SANDS WITH FINES (Appreciable amount of fines)	Non-plastic fines (for identification procedures see ML below).	SM	SILTY SAND	
			Plastic fines (for identification procedures see CL below).	SC	CLAYEY SAND	
FINE GRAINED SOILS More than 50% of material less than 63 mm is smaller than 0.075 mm (A 0.075 mm particle is about the smallest particle visible to the naked eye)	IDENTIFICATION PROCEDURES ON FRACTIONS <0.2 mm.					
	SILTS & CLAYS Liquid limit less than 50	DRY STRENGTH	DILATANCY	TOUGHNESS		
		None to Low	Quick to slow	None	ML	SILT
		Medium to High	None	Medium	CL	CLAY
	SILTS & CLAYS Liquid limit greater than 50	Low to medium	Slow to very slow	Low	OL	ORGANIC SILT
		Low to medium	Slow to very slow	Low to medium	MH	SILT
		High	None	High	CH	CLAY
	Medium to High	None	Low to medium	OH	ORGANIC CLAY	
HIGHLY ORGANIC SOILS	Readily identified by colour, odour, spongy feel and frequently by fibrous texture.			Pt	PEAT	
▪ Low plasticity – Liquid Limit W_L less than 35%. ▪ Medium plasticity – W_L between 35% and 50%.						

• Low plasticity – Liquid Limit W_L less than 35%. • Medium plasticity – W_L between 35% and 50%.

COMMON DEFECTS IN SOIL

TERM	DEFINITION	DIAGRAM	TERM	DEFINITION	DIAGRAM
PARTING	A surface or crack across which the soil has little or no tensile strength. Parallel or sub parallel to layering (eg bedding). May be open or closed.		SOFTENED ZONE	A zone in clayey soil, usually adjacent to a defect in which the soil has a higher moisture content than elsewhere.	
JOINT	A surface or crack across which the soil has little or no tensile strength but which is not parallel or sub parallel to layering. May be open or closed. The term 'fissure' may be used for irregular joints <0.2 m in length.		TUBE	Tubular cavity. May occur singly or as one of a large number of separate or inter-connected tubes. Walls often coated with clay or strengthened by denser packing of grains. May contain organic matter	
SHEARED ZONE	Zone in clayey soil with roughly parallel near planar, curved or undulating boundaries containing closely spaced, smooth or slickensided, curved intersecting joints which divide the mass into lenticular or wedge shaped blocks.		TUBE CAST	Roughly cylindrical elongated body of soil different from the soil mass in which it occurs. In some cases the soil which makes up the tube cast is cemented.	
SHEARED SURFACE	A near planar curved or undulating, smooth, polished or slickensided surface in clayey soil. The polished or slickensided surface indicates that movement (in many cases very little) has occurred along the defect.		INFILLED SEAM	Sheet or wall like body of soil substance or mass with roughly planar to irregular near parallel boundaries which cuts through a soil mass. Formed by infilling of open joints.	

Rock Description Explanation Sheet (1 of 2)

The descriptive terms used by Coffey are given below. They are broadly consistent with Australian Standard AS1726-1993.

DEFINITIONS: Rock substance, defect and mass are defined as follows:

Rock Substance In engineering terms rock substance is any naturally occurring aggregate of minerals and organic material which cannot be disintegrated or remoulded by hand in air or water. Other material is described using soil descriptive terms. Effectively homogenous material, may be isotropic or anisotropic.

Defect Discontinuity or break in the continuity of a substance or substances.

Mass Any body of material which is not effectively homogeneous. It can consist of two or more substances without defects, or one or more substances with one or more defects.

SUBSTANCE DESCRIPTIVE TERMS:

ROCK NAME Simple rock names are used rather than precise geological classification.

PARTICLE SIZE Grain size terms for sandstone are:
Coarse grained Mainly 0.6mm to 2mm
Medium grained Mainly 0.2mm to 0.6mm
Fine grained Mainly 0.06mm (just visible) to 0.2mm

FABRIC Terms for layering of penetrative fabric (eg. bedding, cleavage etc.) are:

Massive No layering or penetrative fabric.

Indistinct Layering or fabric just visible; little effect on properties.

Distinct Layering or fabric is easily visible. Rock breaks more easily parallel to layering of fabric.

ROCK SUBSTANCE STRENGTH TERMS

Term	Abbreviation	Point Load Index, I_{s50} (MPa)	Field Guide
Very Low	VL	Less than 0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with a knife; pieces up to 30mm thick can be broken by finger pressure.

Low	L	0.1 to 0.3	Easily scored with a knife; indentations 1mm to 3mm show with firm blows of a pick point; has a dull sound under hammer. Pieces of core 150mm long by 50mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
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CLASSIFICATION OF WEATHERING PRODUCTS

Term	Abbreviation	Definition
Residual Soil	RS	Soil derived from the weathering of rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported.
Extremely Weathered Material	XW	Material is weathered to such an extent that it has soil properties, ie. it either disintegrates or can be remoulded in water. Original rock fabric still visible.
Highly Weathered Rock	HW	Rock strength is changed by weathering. The whole of the rock substance is discoloured, usually by iron staining or bleaching to the extent that the colour of the original rock is not recognisable. Some minerals are decomposed to clay minerals. Porosity may be increased by leaching or may be decreased due to the deposition of minerals in pores.
Moderately Weathered Rock	MW	The whole of the rock substance is discoloured, usually by iron staining or bleaching, to the extent that the colour of the fresh rock is no longer recognisable.
Slightly Weathered Rock	SW	Rock substance affected by weathering to the extent that partial staining or partial discolouration of the rock substance (usually by limonite) has taken place. The colour and texture of the fresh rock is recognisable; strength properties are essentially those of the fresh rock substance.
Fresh Rock	FR	Rock substance unaffected by weathering.

Medium	M	0.3 to 1.0	Readily scored with a knife; a piece of core 150mm long by 50mm diameter can be broken by hand with difficulty.
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High	H	1 to 3	A piece of core 150mm long by 50mm can not be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
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Very High	VH	3 to 10	Hand specimen breaks after more than one blow of a pick; rock rings under hammer.
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Extremely High	EH	More than 10	Specimen requires many blows with geological pick to break; rock rings under hammer.
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Notes on Rock Substance Strength:

1. In anisotropic rocks the field guide to strength applies to the strength perpendicular to the anisotropy. High strength anisotropic rocks may break readily parallel to the planar anisotropy.
2. The term 'extremely low' is not used as a rock substance strength term. While the term is used in AS1726-1993, the field guide therein makes it clear that materials in that strength range are soils in engineering terms.
3. The unconfined compressive strength for isotropic rocks (and anisotropic rocks which fail across the planar anisotropy) is typically 10 to 25 times the point load index (I_{s50}). The ratio may vary for different rock types. Lower strength rocks often have lower ratios than higher strength rocks.

Notes on Weathering:

1. AS1726 suggests the term 'Distinctly Weathered' (DW) to cover the range of substance weathering conditions between XW and SW. For projects where it is not practical to delineate between HW and MW or it is judged that there is no advantage in making such a distinction, DW may be used with the definition given in AS1726.
2. Where physical and chemical changes were caused by hot gasses and liquids associated with igneous rocks, the term 'altered' may be substituted for 'weathering' to give the abbreviations XA, HA, MA, SA and DA.

Rock Description Explanation Sheet (2 of 2)

COMMON DEFECTS IN ROCK MASSES		Diagram	Map Symbol	Graphic Log (Note 1)	DEFECT SHAPE	TERMS		
Term	Definition				Planar	The defect does not vary in orientation		
Parting	A surface or crack across which the rock has little or no tensile strength. Parallel or sub parallel to layering (eg bedding) or a planar anisotropy in the rock substance (eg, cleavage). May be open or closed.				Curved	The defect has a gradual change in orientation		
					Undulating	The defect has a wavy surface		
					Stepped	The defect has one or more well defined steps		
					Irregular	The defect has many sharp changes of orientation		
Joint	A surface or crack across which the rock has little or no tensile strength, but which is not parallel or sub parallel to layering or planar anisotropy in the rock substance. May be open or closed.				Note: The assessment of defect shape is partly influenced by the scale of the observation.			
ROUGHNESS TERMS								
Sheared Zone (Note 3)	Zone of rock substance with roughly parallel, near planar, curved or undulating boundaries cut by closely spaced joints, sheared surfaces or other defects. Some of the defects are usually curved and intersect to divide the mass into lenticular or wedge shaped blocks.				Slickensided	Grooved or striated surface, usually polished		
					Polished	Shiny smooth surface		
					Smooth	Smooth to touch. Few or no surface irregularities		
					Rough	Many small surface irregularities (amplitude generally less than 1mm). Feels like fine to coarse sand paper.		
Sheared Surface (Note 3)	A near planar, curved or undulating surface which is usually smooth, polished or slickensided.				Very Rough	Many large surface irregularities (amplitude generally more than 1mm). Feels like, or coarser than very coarse sand paper.		
COATING TERMS								
Crushed Seam (Note 3)	Seam with roughly parallel almost planar boundaries, composed of disoriented, usually angular fragments of the host rock substance which may be more weathered than the host rock. The seam has soil properties.				Clean	No visible coating		
					Stained	No visible coating but surfaces are discoloured		
					Veneer	A visible coating of soil or mineral, too thin to measure; may be patchy		
					Coating	A visible coating up to 1mm thick. Thicker soil material is usually described using appropriate defect terms (eg, infilled seam). Thicker rock strength material is usually described as a vein.		
BLOCK SHAPE TERMS								
Infilled Seam	Seam of soil substance usually with distinct roughly parallel boundaries formed by the migration of soil into an open cavity or joint, infilled seams less than 1mm thick may be described as veneer or coating on joint surface.				Blocky	Approximately equidimensional		
					Tabular	Thickness much less than length or width		
					Columnar	Height much greater than cross section		
Extremely Weathered Seam	Seam of soil substance, often with gradational boundaries. Formed by weathering of the rock substance in place.							
Notes on Defects:								
1. Usually borehole logs show the true dip of defects and face sketches and sections the apparent dip.								
2. Partings and joints are not usually shown on the graphic log unless considered significant.								
3. Sheared zones, sheared surfaces and crushed seams are faults in geological terms.								

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 3**

Borehole No. **CBH1**

Sheet **1 of 3**

Project No: **GEOTLCOV23462AA**

Date started: **10.3.2008**

Date completed: **10.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model and mounting: **Mobile Drill 880** Easting: **323702.8** slope: **90°** R.L. Surface: **156.5**
hole diameter: **100 mm** Northing: **6266692.2** bearing: datum: **AMD**

drilling information				material substance			
method	penetration	support	notes, samples, tests, etc	depth (metres)	graphic log	classification symbol	material
ADT	1 2 3	water	E + B R + D Bs + D + E Sa SPT 2,2,5 N ₆₀ =7	156			FILL: CLAYEY SAND: Medium grained, brown and pale brown, low plasticity clay.
				1			
				155			FILL: CLAY: Medium plasticity, grey
				2			
				154			FILL: CLAY: Low to medium plasticity, brown, with some fine grained sand.
			SPT 2,3,2 N ₆₀ =5	3			
				153			
ADT				4			SANDSTONE: Fine grained, pale orange.
			E	152			
				5			Borehole CBH1 continued as core hole
				151			
				6			
				150			
				7			
				149			
				8			
method	support			notes, samples, tests		classification symbols and soil description based on unified classification system	
AS	super screwing			U ₁₀₀ undisturbed sample 100mm diameter		VS very soft	
AD	super drilling			U ₇₅ undisturbed sample 75mm diameter		S soft	
RD	rotary drilling			D disturbed sample		F firm	
W	washbore			N standard penetration test (SPT)		SI stiff	
CT	cable tool			N ₆₀ SPT - sample recovered		VSI very stiff	
HA	hand auger			N ₁₀₀ SPT with solid cone		H hard	
D	d zone			Y vane shear (kPa)		Fb friable	
R	blank bit			P pressuremeter		VL very loose	
V	V bit			Bs bulk sample		L loose	
T	TC bit			E environmental sample		MD medium dense	
4.9	ADT			R refusal		D dense	
						VD very dense	

Engineering Log - Cored Borehole

Borehole No. **CBH1**

Sheet 3 of 3

Project No: **GEOTLCOV23462AA**

Date started, 10.3.2008

Date completed: 10.3.2008

Logged by: JA

Checked by: SM

Client: *Taylor Thomson Whitting*

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA

Berchole Location: *Building 3*

drill model & mounting: Mobile Drill B&D

Easting: 323702.0

slope: -90°

R1	Surface	150 g
----	---------	-------

hole diameter: 100 mm Drilling fluid:

Northing: 5265602.2

boasting:

State	Year	Rate
Alabama	1990	10.0
Alabama	1991	10.0
Alabama	1992	10.0
Alabama	1993	10.0
Alabama	1994	10.0
Alabama	1995	10.0
Alabama	1996	10.0
Alabama	1997	10.0
Alabama	1998	10.0
Alabama	1999	10.0
Alabama	2000	10.0
Alabama	2001	10.0
Alabama	2002	10.0
Alabama	2003	10.0
Alabama	2004	10.0
Alabama	2005	10.0
Alabama	2006	10.0
Alabama	2007	10.0
Alabama	2008	10.0
Alabama	2009	10.0
Alabama	2010	10.0
Alabama	2011	10.0
Alabama	2012	10.0
Alabama	2013	10.0
Alabama	2014	10.0
Alabama	2015	10.0
Alabama	2016	10.0
Alabama	2017	10.0
Alabama	2018	10.0
Alabama	2019	10.0
Alabama	2020	10.0
Alabama	2021	10.0
Alabama	2022	10.0
Alabama	2023	10.0
Alabama	2024	10.0
Alabama	2025	10.0
Alabama	2026	10.0
Alabama	2027	10.0
Alabama	2028	10.0
Alabama	2029	10.0
Alabama	2030	10.0
Alabama	2031	10.0
Alabama	2032	10.0
Alabama	2033	10.0
Alabama	2034	10.0
Alabama	2035	10.0
Alabama	2036	10.0
Alabama	2037	10.0
Alabama	2038	10.0
Alabama	2039	10.0
Alabama	2040	10.0
Alabama	2041	10.0
Alabama	2042	10.0
Alabama	2043	10.0
Alabama	2044	10.0
Alabama	2045	10.0
Alabama	2046	10.0
Alabama	2047	10.0
Alabama	2048	10.0
Alabama	2049	10.0
Alabama	2050	10.0
Alabama	2051	10.0
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Alabama	2065	10.0
Alabama	2066	10.0
Alabama	2067	10.0
Alabama	2068	10.0
Alabama	2069	10.0
Alabama	2070	10.0
Alabama	2071	10.0
Alabama	2072	10.0
Alabama	2073	10.0
Alabama	2074	10.0
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Alabama	2077	10.0
Alabama	2078	10.0
Alabama	2079	10.0
Alabama	2080	10.0
Alabama	2081	10.0
Alabama	2082	10.0
Alabama	2083	10.0
Alabama	2084	10.0
Alabama	2085	10.0
Alabama	2086	10.0
Alabama	2087	10.0
Alabama	2088	10.0
Alabama	2089	10.0
Alabama	2090	10.0
Alabama	2091	10.0
Alabama	2092	10.0
Alabama	2093	10.0
Alabama	2094	10.0
Alabama	2095	10.0
Alabama	2096	10.0
Alabama	2097	10.0
Alabama	2098	10.0
Alabama	2099	10.0
Alabama	2100	10.0
Alabama	2101	10.0
Alabama	2102	10.0
Alabama	2103	10.0
Alabama	2104	10.0
Alabama	2105	10.0
Alabama	2106	10.0
Alabama	2107	10.0
Alabama	2108	10.0
Alabama		

drilling information					material substance				rock mass defects				
method	core-lift	water	RL	depth metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength V L M H EH	f_{cu} MPa D - diam- eter A - axial	RQD %	defect spacing mm S 100 200 300 400	defect description type, inclination, planarity, roughness, coating, thickness	
NWLC				148		Trace of pyrite mineralisation on defect surfaces. 8.9H - 10.3J - clay seams and fault. SANDSTONE: Medium grained, dark orange to pale grey, strong ferric alteration and slightly to distinctly bedded at 22°.	SW		D 0.50 A 0.52	100		PT, 22°, PL, RD, CO	
				147			MW		D 0.56 A 0.34			PT, 15°, IR, RD, CN PT, 10°, RK, RD, CN PT, 5°, IR, RD, CN PT, 20°, UN, RD, CO	
				146					D 0.94 A 0.92	88		SM, 0°, PL, SO, LAMINATED CLAY, 70MM FAULT, 0°, PL, SL, CLAY, 2MM SM, 0°, IR, SO, CLAY, 30MM SM, 0°, PL, SO, CLAY, 100MM JT, 70°, PL, SO, CLAY, 1MM JT, 40°, PL, RD, CLAY & IRON STAINING, 0.5MM	
				145					D 0.64 A 0.48			PT, 15°, PL, SO, CLAY, 0.5MM JT, 70°, PL, RD, CO (IRON), 1MM	
				144			CBH1 terminated at 12.12m						
				143									
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				0									

method

BT auger boring
AD auger drilling
RA rotary core
CS down the hole
NWLC NW Core
NQ, HQ, PQ wireline core

disturb

auger screening
sugar coating
rotary/core
clay or blade bit
NWLC Core
wireline core

core-lift

coring used

barrel withdrawn

graphic log/core recovery

core recovered
- graphic symbols indicate material
no core recovered

water

10/100 water level on date shown

water inflow
partial drill fluid loss
complete drill fluid loss

water pressure test result (megapascals) for depth interval shown

weathering

FR fresh
SW slightly weathered
MW moderately weathered
HW highly weathered
XW extremely weathered
LW extensively weathered (covers HW and XW)

strength

VL very low
L low
M medium
H high
VH very high
EH extremely high

defect type

JT joint
PT parting
SZ shear zone
SS sheared surface
CS crushed seam

planarity

PL planar
CU curved
UN undulating
ST stepped
IR irregular

roughness

VR very rough
RO rough
SO smooth
SI sawtooth

coating

CN clean
SN stained
VN varnished
CO coating



drawn	MT		client	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH - CBH1	
scale	to scale		project no:	GEOTLCOV23462AA	Photo no: CBH1 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No: **CBH2**
 Sheet: **1 of 1**
 Project No: **GEOTLCOV23462AA**
 Date started: **10.3.2008**
 Date completed: **10.3.2008**
 Logged by: **JA**
 Checked by: **SH**

Drill model and mounting: Mobile Drill B80		Easting: 323709.4		slope: -90°		R.L. Surface: 156.7	
Hole diameter: 100 mm		Northing: 8285715.5		bearing:		datum: AHD	
drilling information				material substance			
method	penetration	support	notes, samples, tests, etc	depth metres	graphic log	classification symbol	material
ADT	1 2 3	NOT OBSERVED	E Bs C SPT N=K	156			FILL: BITUMEN and ROADBASE FILL: CLAYEY SAND: Fine grained, brown, low to medium plasticity clay, with some sandstone gravel (15mm diameter) at 1.2m.
				155			Borehole CBH2 terminated at 1.3m
				154			
				153			
				152			
				151			
				150			
				149			
				148			
method		support		notes, samples, tests		classification symbols and soil description based on unified classification system	
AS	auger screening	M mud	N nil	U ₁₀	undisturbed sample 50mm diameter	moisture U dry M moist W wet Wp plastic limit Wl liquid limit	
AD	auger drilling	C casing		U ₁₅	undisturbed sample 60mm diameter		
RP	rollerincons	penetration	1 2 3 4	D	disturbed sample	consistency/density index VS very soft S soft F firm St stiff VSI very stiff H hard Fb brittle VL very loose L loose MD medium dense D dense VD very dense	
W	washmore			N	standard penetration test (SPT)		
CT	calibre test			N ₁	SPT - sample recovered		
HA	hand auger			Nc	SPT with void cone		
BT	bitprobe			V	cone shear (kPa)		
B	blank test			P	pressuremeter		
V	Vib			Bs	bulk sample		
T	TC bit			E	environmental sample		
*oil shown by soilflow				R	refuse		
ADT							

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHRONGA**
 Borehole Location: **Building 1**

Borehole No. **CBH2A**
 Sheet **1 of 1**
 Project No. **GEOTLCOV23462AA**
 Date started: **10.3.2008**
 Date completed: **10.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting:		Mobile Cdr 880		Easting:		323707.66		slope:		-90°		R.L. Surface:		156.7	
hole diameter:		100 mm		Northing:		8265714.8		bearing:				datum:		AID	
drilling information				material substance											
method	penetration	support	water	notes samples, tests, etc.	depth meters	graphic log	classification symbol	material	moisture condition	consistency/ density index	poisson's ratio	unit weight kN/m ³	structure and additional observations		
ADT	123	NOT OBSERVED			156			FILL: BITUMEN and ROADBASE					FILL		
					1			FILL: CLAYEY SAND: Fine grained, brown, low to medium plasticity clay, with some medium gravel.					TC bit refusal on concrete at 1.08m		
Borehole CBH2A terminated at 1.08m															
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Engineering Log - Borehole

Borehole No. CBH2B

Sheet 4 of 4

Project No: **GEOTLCOV23482AA**

Date started: 10.3.2008

Date completed: **10.3.2008**

Logged by: JA

Checked by: **SH**

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA

Barcode Location: **Building 1**

drill model and mounting: Mobile Drill E-80

Easting: 323713.4

slope: -90°

RL Surface: 156.9

hole diameter: 100 mm

Nothing 526.5/13

bagging:

value AND

drilling information						material substance							
method	penetration			notes samples, tests, etc.	depth meters	graphic log	classification symbol	material soil type; plasticity or particle characteristics, texture, secondary and minor components	moisture condition	consistency/ density index	penetration kPa	cone resistance kPa	structure and additional observations
	1	2	3										
ADT					156			FILL: BITUMEN AND ROADBASE	D				FILL
					156			FILL: CLAYEY SAND: Fine grained, brown, low to medium plasticity clay, with some medium grained gravel.					
					155			Borehole CBH2B terminated at 1.6m					TC bit refusal due to concrete at 1.6m
					154								
					153								
					152								
					151								
					150								
					149								
method	auger screwing*			equipment	notes, samples, tests	classification symbols and soil description based on unified classification system			consistency/density index				
AS	auger screwing*			M mud	U _u undisturbed sample 50mm diameter	moisture D dry M moist W wet Wp plastic limit WL liquid limit			VS very soft S soft F firm St stiff VS+ very stiff H hard Fh friable VL very loose L loose MD medium dense D dense VD very dense				
AD	auger drilling*			C casing	U _u undisturbed sample 63mm diameter								
RR	rotary/reel			penetration	U _d disturbed sample	density index VS very soft S soft F firm St stiff VS+ very stiff H hard Fh friable VL very loose L loose MD medium dense D dense VD very dense							
W	washhole			1 2 3 4	U _d standard penetration test (SPT)								
CT	cable tool				U _r SPT - sample recovered								
HR	hand auger				U _c SPT with solid core								
DT	dibble				U _v vane shear (kPa)								
B	bunk drill				P pressuremeter								
V	vibr				Qa bulk sample								
T	TC bit				G geotechnical sample								
*bit shown by suffix					R refuse								
AST													

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 3**

Borehole No.	CBH3
Sheet	1 of 3
Project No:	GEOTLCOV23462AA
Date started:	10.3.2008
Date completed:	11.3.2008
Logged by:	JA
Checked by:	SH

drill model and mounting: Mobile Drill B80				Easting: 320710.4		slope: -30°		R.L. Surface: 158.0					
hole diameter: 100 mm				Northing: 6285676.35		bearing:		nature: AHD					
drilling information				material substance									
method	penetration	support	water	notes samples, tests, etc.	RL	depth metres	graphic log	classification symbol	material soil type; plasticity or particle characteristics, colour, secondary and minor components.	mixture condition	consistency/ density index	pocket penetrometer	structure and additional observations
ADV	1 2 3			E					FILL: SILTY SAND: Topsoil, fine grained, brown.	D			FILL
				R _s E					FILL: CLAY: Low to medium plasticity clay, pale gray and orange, with some sand.	<wp			
				R _s									
				SPT 2,1,5 N=6	157	1							
					156	2							
				SPT 5,5,9 N=14	155	3			FILL: SAND: Medium grained, orange, with some sandstone gravel and clay. 5mm gravel, low to medium plasticity clay, sandstone cobble.	D			
					164	4							
				SPT 2,3,4,3 N=R	153	5			FILL: SANDY CLAY: Medium plasticity, medium grained sand, with some coarse gravel	<wp			
					152	6			Tree roots at 5.5m-5.7m Stiffer clay layer 5.7m-5.9m				Organic odour from base of hole
				SPT 9,5,8 N=13	150	8			Borehole CRH3 completed as cased hole				V-pit refusal at 6.25m
					161	7							
					150	8							
method				support		N fill		notes, samples, tests		classification symbols and soil description based on unified classification system		consistency/density index	
AS auger "drinking"				M mud				U _a undisturbed sample 50mm diameter		VS very soft			
AC auger "drinking"				C casing				U _b undisturbed sample 63mm diameter		S soft			
RR rotithrone				penetration				D maximum sample		f firm			
W washbore				1 2 3 4				N standard penetration test (SPT)		SL stiff			
CT cable tool				no resistance ranging to refusal				N _r SPT - sample recovered		VRt very stiff			
HA hand auger				water				N _c SPT with cold cone		II hard			
OT outside				13/198 water level on depth chart				V vane shear (kPa)		Hb massive			
A Vark bit				water inflow				P pressuremeter		VI very loose			
V V-bit				water outflow				ss bulk sample		L loose			
F TC bit								E environmental sample		MD medium dense			
*bit driven by surface								R refusal		D dense			
ADT										VD very dense			

Engineering Log - Cored Borehole

Borehole No. CBH3

Sheet 2 of 3

Project No: **GEOTLCOV23462AA**

Date started: 10.3.2008

Date completed: 11.3.2008

Logged by: JA

Checked by: **SH**

Client: *Taylor Thomson Whittington*

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHRONGA

Borehole Location: *Building 3*

drill model & mount on: Mobile Drill B00

Eastling: 323716.4

slope: -90°

El Surface	158.0
------------	-------

hole diameter: 100 mm Drilling fluid:

Northing: 6265676.35

bearing

date: AHD

drilling information					material substance					rock mass defects				
method	core-ht	water	RL	depth metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering intensity	estimated strength	IS, MPa D diam. A axial	RQD %	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness		
				157	1									
				156	2									
				155	3									
				154	4									
				153	5									
				152	6									
						Continued from non-cored borehole								
NMLC				151	7	SANDSTONE: Medium grained orange and pale grey, indistinctly to distinctly bedded.	HW		D A 0.18 0.15	100		PT, 0°, PL, RD, SN		
									D A 0.38 0.28	95		PT, 15°, PL, SO, CO		
												SM, 0°, PL, SO, sandy clay, 50mm		
												SM, 5°, PL, SO, sandy clay, 3mm		
				150	8							SM, 16°, PL, SO, sandy clay, 3mm		

method

DI auger drilling

AS auger screwing

AD auger drilling

RK rotary core

CB core bit

NMLC NMLC core

NQ, HQ, PQ wireline core

core-ht

core recovered

graphic symbols indicate material

no core recovered

water

water level on data shows

water inflow

partial bit fluid loss

complete bit fluid loss

water pressure test result (supersat) in depth interval shown

weathering

FR fresh

SW slightly weathered

MW moderately weathered

HW highly weathered

EW extremely weathered

DW distinctly weathered (covers MW and HW)

strength

VL very low

L low

M medium

H high

VH very high

EH extremely high

defect type

JT joint

PT parting

SM shear

SZ shear zone

SS sheared surface

CS crushed seam

planarity

PL planar

CU curved

UN undulating

ST stepped

IR irregular

roughness

VA very rough

RO rough

SO smooth

SL slickensided

coating

CN clean

SN silty

VN veneer

CO coating

Engineering Log - Cored Borehole

Borehole No. **CBH3**
 Sheet **3 of 3**
 Project No. **GEOTLCOV23462AA**
 Date started. **10.3.2008**
 Date completed. **11.3.2008**
 Logged by: **JA**
 Checked by: **SH**

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 3**

drill model & mounting: Mobile Cdr 680				Easting: 323716.4		slope: -80°		R.L Surface: 155.0							
hole diameter: 100 mm Drilling fluid:				Northings: 6205076.35		bearing:		datum: AHD							
drilling information				material substance				rock mass defects							
method	core lift	water	RL	depth, metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	IS _{sp} MPa D diam drill A: anal	ROD %	defect spacing mm	defect description			
												particular	general		
NMLO				149	9	SANDSTONE: Medium grained orange and pale gray, indistinctly to distinctly bedded. (continued)	HW		0.76 0.68						
				148	10		MW		0.57 0.5			JT, 70°, UN, CN			
				148	10				0.34 0.4			PT, 20°, PL, RO, SN			
				147	11						PT, 20°, PL, SO, CO				
				147	11						SM, 20°, PL, SO, clay, 3mm				
				146	12						JT, 65° PL, SO, clay, 3mm,				
				146	12						SM, 10°, UN, SO, clayey sand, 10mm				
				146	12						SM, 10°, UN, SO, clayey sand, 10mm				
				146	12						PT, 5°, IR, RO, CN				
				146	12						SM, 0°, PL, SO, clay, 40mm				
			145	13		NO CORE: 0.09m Clay seams, 260mm thick, from 12.07m - 12.33m	MW		0.31 0.24				SM, 0°, PL, SO, clay, 260mm		
			145	13		NO CORE: 0.00m CBH3 terminated at 12.36m	MW								
			144	14											
			143	15											
			142	16											

method	DT AS AD RH CB NMLO NO, HQ, PQ	diatube auger screwing auger drilling rotary core down the blow bit RTMLO core wireline core	core lift casing used borehole withdrawn graphic log/core recovery core recovered graphic symbols indicator extended no core recovered	water 10/10% water level on date shown water inflow partial drill fluid loss complete drill fluid loss water pressure test result (log means) for depth interval shown	weathering FR SW MW NW XW OW brach slightly weathered moderately weathered highly weathered extremely weathered disintegrated (termers MW and NW) strength VL L M H VH BH very low low medium high very high extremely high	defect type JT PT SM SZ SS CS joint parting seam sheared cont sheared surface crushed seam planarity PL CU UN ST IR planar curved undulating stepped irregular roughness VR RO SO SL very rough rough smooth slickensided couling CN RN VN CO clean stained weather coating
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drawn	MT	 <p>coffey geotechnics SPECIALISTS MANAGING THE EARTH</p>	client	Taylor Thomson Whitting	
approved	ST		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2006		title	ROCK CORE PHOTOGRAPH - CBH3	
scale	to scale		project no:	GEOTLCOV23462AA	Photo no: CBH3 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH4**
 Sheet **1 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **11.3.2008**
 Date completed: **11.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting: Mobile Drill B30				Easting: 323870.7		slope: -80°		R.L. Surface: 162.9					
hole diameter: 100 mm				Northing: 6265657.3		bearing:		datum: AMP					
drilling information				material substance									
method	penetration	support	notes samples, tests, etc	RL	depth metres	graph log	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency/ density index	soil penetration test kPa	structure and additional observations	
ADV			E E + B ₁ B ₂ E	162	1		CL	FILL: BITUMEN and ROADBASE SANDY CLAY: Low plasticity, orange, fine grained sand. CLAY: Low plasticity, orange, friable, with some fine grained sand. SANDSTONE: Fine to medium grained, pale orange.	S	SI		FILL RESIDUAL SOIL	
ADT												SANDSTONE V-bit refusal at 0.7m	
NOT MONITORED								Borehole CBH4 continued as cored hole					
					18.1	2							
					160	3							
					159	4							
					158	5							
					157	6							
					156	7							
					155	8							
method	support			notes, samples, tests			classification symbols and soil description based on unified classification system			consistency/density index			
AS	auger screwing*			U ₁	undisturbed sample 50mm diameter			moisture	D dry	VS	very soft		
AD	auger drilling*			U ₂	undisturbed sample 63mm diameter					S	soft		
RR	rotary/stone			D	disturbed sample			moisture	M moist	F	firm		
W	washstone			N	standard penetration test (SPT)					SI	stiff		
CT	cable tool			N*	SPT - sample recovered			moisture	V wet	VS ₁	very stiff		
HA	hand auger			Nc	SPT with surface cone					H	hard		
DT	dialube			V	vane shear (kPa)			moisture	VL very loose	VS ₂	very stiff		
B	blank bit			V	pressuremeter					H	hard		
V	V bit			Rs	risk sample			moisture	VL very loose	VS ₃	very stiff		
T	TC bit			C	environmental sample					VS ₄	very stiff		
*bit shown by suffix e.g. ADT				R	refused			moisture	VL very loose	VS ₅	very stiff		
										VS ₆	very stiff		

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH4**
 Sheet **2 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **11.3.2008**
 Date completed: **11.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drilling information				material substance				rock mass defects				
method	core lift	water	RL	depth meters	graphic log core recovery	rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	Is, pa MPa D - diam- etral A - axial	ROQ %	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness
						particular						
						general						
			162	1		Continued from non-cored borehole						
			161	2		SANDSTONE: Fine grained, dark orange and pale grey, distinctly bedded with irregular weathering patterns.	NW					SM, 0°, PL, SO, clay, 30mm SM, 0°, PL, SO, clay, 30mm
			160	3								PT, 0°, PL, SO, clay, 0.5mm JT, 82°, UN, RQ, CO, 1mm, fine tree root
			159	4								PT, 5°, PL, SO, clay, 1mm SM, 0°, PL, SO, clay, 30mm SM, 25°, PL, SP, clay, 10mm
			158	5		SANDSTONE: Medium grained, pale grey with bands of iron stained orange, distinctly bedded.	SH					SM, 32°, PL, SO, sandy clay, 20mm PT, 0°, PL, SO, CN, fine roots PT, 0°, PL, SO, clay, 1mm JT, 25°, PL, SO, VN PT, 0°, PL, SO, clay, 2mm PT, 15°, PL, SO, CO PT, 5°, PL, SO, CO SM, 45°, IR, SO, clay, 2mm JT, 45°, PL, SO, CO, 1mm PT, 2°, PL, RO, CN PT, 0°, PL, SO, CO PT, 0°, PL, RO, SN PT, 0°, PL, RO, CN
			157	6								PT, 5°, PL, SO, CO PT, 2°, PL, RO, CN
			156	7		CBH terminated at 6.18m						
			155	8								

method
NT
AS
AD
RR
CB
NWC
NQ, NQ, PQ

disturb
auger sampling
auger drilling
rotary core
claw or grab on
NWC core
winding core

core lift
casing used
barrel withdrawn

graphic log core recovery
core recovered
graphic symbols
mobile material
on core recovered

water
10/1/98 water level
on date shown
water inflow
partial drill fluid loss
complete drill fluid loss

water pressure last recall
(if gauge) for depth
interval shown

weathering
FR fresh
GW slightly weathered
NW moderately weathered
HW highly weathered
XW extremely weathered
LW distinctly weathered
(cover NW and HW)

strength
VL very low
L low
M medium
H high
VH very high
EH extremely high

defect type
JT part
PT parting
SM beam
S7 shear zone
SS sheared surface
CS crushed beam

planarity
Pv plane
CU curved
UN undulating
ST stepped
IR irregular

roughness
VR very rough
RO rough
SO smooth
SL slickensided

coating
CN clean
SN stained
VN veneer
CO coating



drawn	MT	 <p>coffey geotechnics SPECIALISTS MANAGING THE EARTH</p>	client	Taylor Thomson Whitting	
approved	SI		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 200E		title	ROCK CORE PHOTOGRAPH – CBH4	
scale	Not to scale		project no.	GEOTLCOV23462AA	Photo no: CBH4 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH5**
 Sheet **1 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **11.3.2008**
 Date completed: **12.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting: Mobile Drill Rig		Easting: 323839.1		slope: 90°		R.L. Surface: 162.9	
hole diameter: 100 mm		Northing: 6265846.9		bearing: 		datum: AHD	
drilling information				material substance			
method	penetration	support	notes samples, tests, etc	RL	depth metres	graphic log	classification symbol
1	2	3					
ADV			E	162	1		FILL: BITUMEN and ROADBASE
			F + R _s				CLAY: Low plasticity, brown, with some sand fine grained sand.
			R _s				
			SPT x10 N=R				SANDSTONE: Fine to medium grained, orangeish brown, highly weathered.
							Borehole CBH5 continues as cored hole
				161	2		
				160	3		
				159	4		
				158	5		
				157	6		
				156	7		
				155	8		
method				support		notes, samples, tests	
AD: auger drilling				M: mud		U _s : undisturbed sample 50mm diameter	
AR: roller/hammer				C: casing		U _d : disturbed sample 50mm diameter	
W: washstone				penetration 1 2 3 4		D: disturbed sample	
CT: cable tool				no resistance ranging to refusal		N: standard penetration test (SPT)	
HM: hand auger				water		N': SPT - sample recovered	
DT: distube				100/100 water level on date shown		N _c : SPT with solid cone	
B: blank bit				water inflow		V: vane shear (kPa)	
Y: Y bit				water outflow		P: pressuremeter	
T: TC bit						Bs: bulk sample	
"on" down by falls						E: environmental sample	
e.g. ADT						R: refusal	
						classification symbols and soil description	
						based on Unified Classification System	
						moisture	
						D: dry	
						M: moist	
						W: wet	
						Wp: plastic limit	
						W _L : liquid limit	
						consistency/density index	
						VS: very soft	
						S: soft	
						F: firm	
						St: stiff	
						VS1: very stiff	
						H: hard	
						FH: friable	
						VL: very loose	
						L: loose	
						MD: medium dense	
						D: dense	
						VD: very dense	

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH5**
 Sheet **2 of 2**
 Project No: **GEOTLCOV23462AA**
 Date started: **11.3.2008**
 Date completed: **12.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model & mounting: **Mobile Dnr 880** Easting: **323830.1** slope: **-00°** R.L. Surface: **162.9**
 hole diameter: **100 mm** Drilling fluid: Northing: **6265846.9** bearing: datum: **AHD**

drilling information					material substance			rock mass defects										
method	core-lit	water	RL	depth metres	graphic log core recovery	rock type; grain characteristics, colour, structures, minor components	weathering alteration	estimated strength	$I_{s,un}$ MPa R _u diam- eter A axial	defect spacing mm	defect description							
								$\sigma_1 > \sigma_2 > \sigma_3$			particular	general						
			162	1		Continued from non-cored borehole												
NMLC			161	2		SANDSTONE: Fine grained, pale grey and orange, distinctly bedded	HW		D A 0.01 0.2									
			160	3		SANDSTONE: Medium grained, orange and pale brown, bands of iron stained rock.	MW		D A 0.00 3.02									
			159	4					D A 0.62 0.97									
			158	5					D A 0.73 0.87									
			157	6		SANDSTONE: Medium grained, orange and pale grey, distinctly bedded.	SW FR		D A 0.63 0.69									
			156	7		CBH5 terminated at 6m												
			155	8														
method					core-lit		water		weathering		defect type							
DT AS ARS RR CB NMLC NQ, HQ, PQ					delube super screening water drilling isolation natural bleed off NMLC core wireline core		casing used barrel withdrawn graphic log/core recovery none recovered graphic symbols indicate material no core recovered		10/12/93 water level on data shown water inflow partial drill fluid loss complete drill fluid loss water pressure test result (Augeons) for depth interval shown		FR SW MW HW ASV DW strength VI L M H VH EH		fresh slightly weathered moderately weathered highly weathered extremely weathered distinctly weathered (covers MW and HW) very low low medium high very high extremely high		JT JT PM SM SZ SS CS planarity PL CU UN ST R		roughness VR RO SO SL cleaning CN SN VN CO	
											very rough rough smooth stepped		clean stained various cracking					

method
 DT dilute
 AS auger screwing
 AR auger drilling
 RR rotary/circum
 CB core or blast bit
 NMLC NMLC core
 HQ, HQ, PO wireline core

core-lit
 casing used
 barrel withdrawn
 graphic log/core recovery
 core recovered
 - graphic symbols indicate material
 no core recovered

water
 10/125 water level on data shown
 water inflow
 partial drill fluid loss
 complete drill fluid loss
 water pressure test result (lugons) for depth interval shown

weathering
 FR fresh
 SW slightly weathered
 MW moderately weathered
 HW highly weathered
 AV extremely weathered
 DW extremely weathered (below MW and HW)
 strength
 VI very low
 L low
 M medium
 H high
 VH very high
 EH extremely high

defect type
 JT joint
 PT part 2
 SM seam
 SZ sheared zone
 SS sheared surface
 CS crushed seam
 planarity
 PL planar
 CU curved
 UN undulating
 ST stepped
 R irregular
 roughness
 VR very rough
 RO rough
 SO smooth
 SL slickensided
 coating
 CN clean
 SN stained
 VN veneer
 CO coating



drawn	MT	 coffey geotechnics SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting	
approved	St		project:	185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH - CBHE	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBHE 1 of 1
original size	A4				

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Warehouse Location: **Building 1**

Borehole No.	CBH6
Sheet	1 of 2
Project No.	GEOTLCOV23462AA
Date started	12.3.2008
Date completed	12.3.2008
Logged by	JA
Checked by:	SH

drilling information				material substance							
method	penetration	support	water	notes, samples, tests, etc.	depth (meters)	classification symbol	material	moisture condition	consistency/density index	pocket penetrometer (MPa)	structure and additional observations
AS	1	2	3				FILL: BRICKS and ROADBASE				FILL
AD				E F + Gs	1.56	SP	SAND: Medium graded, brown, with some clay, trace of gravel.		AMD		RESIDUAL SOIL
				Bs	1						Insufficient SPT sample for PID test
AD				SPT N=1 N ₆₀ =R	1.55		SANDSTONE: Medium graded, pale yellow and pale gray. Borehole DBH6 continued as cased hole				V-BK refusal at 1.02m SANDSTONE
					2						
					3						
					4						
					5						
					6						
					7						
					8						

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 1**

Borehole No.	CBH6
Sheet	2 of 2
Project No.	GEOTLCOV23462AA
Date started:	12.3.2008
Date completed:	12.3.2008
Logged by:	JA
Checked by:	SH

[illegible]



drawn	MT	 coffey geotechnics SPECIALISTS MANAGING THE EARTH	client	Taylor Thomson Whiting	
approved	ST		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 200E		title	ROCK CORE PHOTOGRAPH – CBHE	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBHE 1 of 1
original size	A4				

Engineering Log - Borehole

Borehole No: **CBH7**
 Sheet: 1 of 3
 Project No: **GEOTLCOV23462AA**
 Date started: **12.3.2008**
 Date completed: **13.3.2008**
 Logged by: **JA**
 Checked by: **SH**

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 3**

drill model and mounting: **Mobile Drill 880** Easting: **323734** slope: **-90°** R.L. Surface: **157.7**
 hole diameter: **100 mm** Northing: **6265890** bearing: datum: **AMD**

drilling information					material substance						
method	penetration	support	notes samples tests, etc	RL	depth metres	grain size log	classification symbol	material	moisture condition	consistency/density index	structure and additional observations
ADV			E(x2) E(x3) + Bs Bs SPT 2,9,9 N=12 SPT <10 N=8 E	157 156 155	1 2 3			FILL: CLAYEY SAND: Topsoil, medium grained sand, organics FILL: SANDY CLAY: Low to medium plasticity, orange and pale gray, fine sand, with some sandstone fragments. FILL: CLAYEY SAND: Medium grained, dark brown, medium plasticity clay. Sandstone cobble (weathered): 1.3-1.45m SANDY CLAY: Low plasticity orange, fine grained sand. Borehole CBH7 continued as cored hole	D <Wp W >Wp		FILL No odour from GW Insufficient SPT sample for PID Test SPT sample disturbed RESIDUAL SOIL V-bl refuse at 2.86m
				154 153 152 151 150	4 5 6 7 8						

Borehole GEOTLCOV23462AA CPJ COFFEY OCT 4 '08

Form GEOT-2.3 Date 2 Rev 2

method AS auger screening AD auger drilling RR reference W washbore CT cable tool HA hand auger OT diaphane B blank bit V vb T TG bit *bl shown by suffix B.g. ADT	support M mud C casing penetration 1 2 3 4 no resistance ranging to refusal water 100/150 water level on site shown water inflow water outflow	notes, samples, tests U _u undisturbed sample 50mm diameter U _b undisturbed sample 63mm diameter D disturbed sample N standard penetration test (SPT) N _r SPT - sample recovered N _r SPT with split cone V vane shear (c/s) P pressuremeter R _c bulk sample C environmental sample R refusal	classification symbols and soil description based on unified classification system moisture f clay M moist W wet Wp plastic limit W _L liquid limit	consistency/density index VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense
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Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 3**

Borehole No. **CBH7**
 Sheet **2 of 3**
 Project No: **GEOTLCOV23462AA**
 Date started: **12.3.2008**
 Date completed: **13.3.2008**
 Logged by: **JA**
 Checked by: **SH**

core model & mounting: **Mobile Crt 880** Easting: **323784** slope: **-00°** R.L. Surface: **157.7**
 hole diameter: **100 mm** Drilling fluid: Northing: **6266690** bearing: datum: **AHD**

drilling information				material substance				rock mass defects			
method	core-lift	water	HL	depth metres	graphic log core recovery	material rock type, grain characteristics, colour, structure, minor components	weathering classification	estimated strength	IS ₁₀₀ MPa C - diam. stat A - anal	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness
				157	1						
				156	2						
				155	3	Continued from non-cored borehole					
NMLO				154	4	SANDSTONE: Medium grained sand pale grey with leached weathered seams and bands of ironstone.	XW		D A 0.44 0.67		SM, 20°, PL, SO, CLAY, 250mm BM, 10°, PL, SO, CLAY, 10mm RM, 10°, PL, SO, CLAY, 3mm JT, 60°, PL, SO, CO JT, 60°, PL, SO, CLAY, 10mm
						NO CORE: 0.05m	HW		D A 0.02 1.21		SM, 0°, PL, SO, CLAY, 150mm
				153	5	NO CORE: 0.04m SANDSTONE: Medium grained, pale grey with occasional bands of red ironstone, sugary, bedded at 25°	MW		D A 0.31 0.54		PT, 25° PL, RO, CN PT, 5° PL, SO, CO PT, 5° PL, SO, CO PT, 10° PL, SO, CO PT, 80° UN, RO, CO
				152	6				D A 0.48 0.37		
				151	7	Subvertical iron/clay filled seam extends from 6.78m to 11.4m					PT, 20°, PL, SO, CO PT, 20°, PL, SO, CO PT, 20°, PL, SO, CO
				150	8				D A 0.15 0.38		PT, 10°, PL, SO, CO SM, 10°, PL, SO, CLAY 8mm

CORED BOREHOLE GEOTLCOV23462AA CPU COFFEY.ECT 4/8/08

Form GEO 5.5 ISS. 0 3 Rev. 3

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 3**

Borehole No: **CBH7**

Sheet: **3 of 3**

Project No: **GEOTLCOV23462AA**

Date started: **12.3.2008**

Date completed: **13.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model & mounting: **Mobile Drill 880**

Easting: **320734**

slope: **-90°**

R.L. Surface: **157.7**

hole diameter: **100 mm** Drilling fluid:

Northing: **6265490**

bearing:

datum: **AHD**

drilling information					material substance					rock mass defects				
method	core lift	water	RL	depth metres	graphic log core recovery	material rock type: grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	is _{sp} MPa Q ₁₀ diam. and A ₁₀ axial	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness			
											particular	general		
MM.C			149	9		SANDSTONE: Medium grained, pale grey with occasional bands of red ironstone. sugary, bedded at 25°. (continued)	MW				PT, 8°, PL, SO, CN			
					SM, 20°, PL, SO, SANDY CLAY, 5mm									
					PT, 20°, PL, SO, CO									
					PT, 20°, PL, SO, CO									
					PT, 20°, PL, SO, CO									
					PT, 20°, PL, SO, CO									
			148	10							PT, 10°, PL, SO, CO			
					PT, 10°, PL, SO, CO									
					SM, 15°, PL, SO, CLAY, 50mm									
					PL, 5°, PL, SO, CO									
			147	11							PT, 10°, PL, SO, CO			
					PT, 45°, PL, SO, CLAYEY SAND, 3mm									
				PM, 0° PL, SO, CLAYEY SAND, 5mm										
				PM, 0° PL, SO, CLAYEY SAND, 5mm										
				PT, 30°, PL, SO, CO										
				PT, 10°, PL, SO, CO										
				SM, 25° PL, SO, CLAY (HP, DARK BROWN), 100mm										
				SM, 10° PL, SO, CLAY LAMINATED, 170mm										
			146	12	Seam at 11.7m contains finely laminated clay and very fine sand.			D ₁₀ 0.21 D ₅₀ 0.10 D ₉₀ 0.7			PT, 10°, PL, SO, CO			
					CBH7 terminated at 12m	FR								
			145	13										
			144	14										
			143	15										
			142	16										

method	core lift	water	weathering	defect type	roughness
UT	T	101.08 water level on date shown	FR	JT	VR
AS	—		SW	PM	HO
AD	—		UN	SI	SO
RR	—		HW	SE	SL
CB	—		KW	CS	
MM.C	—		CW		
ND, HCL, PO	—				
core lift	water	weathering	defect type	roughness	planarity
T	101.08 water level on date shown	FR	JT	VR	PL
—		SW	PM	HO	CU
—		UN	SI	SO	UN
—		HW	SE	SL	ST
—		KW	CS		IR
—		CW			
graphic log/core recovery	water	weathering	defect type	roughness	planarity
—	101.08 water level on date shown	FR	JT	VR	PL
—		SW	PM	HO	CU
—		UN	SI	SO	UN
—		HW	SE	SL	ST
—		KW	CS		IR
—		CW			
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CORED BOREHOLE GEOTLCOV23462AA GPJ CD5667 EDT 4 13 08

FORM GEOT 4.2 ISSUE 2 REV. 2



drawn	MT	 SPECIALISTS MANAGING THE EARTH	client	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL	
date	26 / 3 / 2008			WAHROONGA	
scale	Not to scale		title	ROCK CORE PHOTOGRAPH - CBH7	
original size	A4		project no:	GEOTLCOV23462AA	Photo no: CBH7

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No: **CBH8**
 Sheet: **1 of 2**
 Project No: **GEOTLCOV23462AA**
 Date started: **13.3.2008**
 Date completed: **13.3.2008**
 Logged by: **JA**
 Checked by: **SH**

DRI model and mounting:		Mobile DRI 1580		Easting:		323693.6		slope:		-80°		R.L. Surface:		156.4	
hole diameter:		100 mm		Northing:		626577.4		bearing:				datum:		AHD	
drilling information						material substance									
method	penetration	support	water	notes samples, tests, etc.	depth meters	graphic log	classification symbol	material	moisture and flow	consistency density index	penetration kPa	structure and additional observations			
ADU	1 2 3			E E(x3) + Bs + D Bs Bs + E	156		Sp	FILL: BITUMEN and ROADBASE SAND: Fine to medium grained, orange and pale grey, trace of clay.	D	MD		FILL RESIDUAL SOIL V-bl refusal at 0.87m			
Borehole CBH8 continued as core hole															
<div style="display: flex; justify-content: space-between;"> <div style="writing-mode: vertical-rl; transform: rotate(180deg);">NCT MON TORED</div> <div> <div style="text-align: center;">155</div> <div style="text-align: center;">2</div> <div style="text-align: center;">154</div> <div style="text-align: center;">3</div> <div style="text-align: center;">153</div> <div style="text-align: center;">4</div> <div style="text-align: center;">152</div> <div style="text-align: center;">5</div> <div style="text-align: center;">151</div> <div style="text-align: center;">6</div> <div style="text-align: center;">150</div> <div style="text-align: center;">7</div> <div style="text-align: center;">149</div> <div style="text-align: center;">8</div> </div> </div>															
method	support			notes, samples, tests		classification symbols and soil description based on unified classification system				consistency/density index					
AS	auger screening			U _u undisturbed sample 50mm diameter		moisture Q dry M moist W wet Wp plastic limit W _L liquid limit				VS very soft S soft F firm SI stiff VSI very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense					
AD	auger drilling			U _d undisturbed sample 83mm diameter											
RR	roller/cone			D disturbed sample											
W	washcore			N standard penetration test (SPT)											
CT	cable tool			N _r SPT sample recovered											
HA	hand auger			Nc SPT with soil cone											
DI	diamond			V vane shear (kPa)											
R	blank bit			P pressuremeter											
V	V bit			Bs bulk sample											
T	TC bit			E environmental sample											
*not shown by suffix e.g. AU1															

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 1**

Borehole No: **CBH8**

Sheet: **2 of 2**

Project No: **GEOTLCOV23462AA**

Date started: **13.3.2008**











Date completed: **13.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model & mounting: **Mobile Drill B80** Easting: **323603.9** slope: **-90°** R.L. Surface: **166.4**
hole diameter: **100 mm** Drilling fluid: Northing: **6266771.1** bearing: datum: **AMU**

drilling information					material substance		rock mass defects										
method	core lift	water	RL	depth metres	graphic log core recovery	rock type; grain characteristics, colour, siliceous, minor components	weathering a notation	estimated strength					is _u MPa U - down A - axial	RQD %	defect spacing mm	defect description	
								V	L	M	H	EH				type, inclination, planarity, roughness, coating, thickness	particulate
			156														
NMLC	NOT MONITORED		155	1		Continued from non-cored borehole SANDSTONE: Medium grained, dark red to pale yellow, indistinctly bedded.	MW								PT, 5°, PL, RO, CO		
															PT, 5°, PL, SO, CLAY, 4MM		
															PT, 10°, PL, SO, CLAY, 4MM		
															PT, 2°, PL, RO, CO		
			154	2		SANDSTONE: Medium grained, orange to pale yellow, indistinctly bedded.									SV, 0°, PL, SO, SANDY CLAY, 80MM		
			153	3												PT, 10°, PL, RO, SN	
			152	4		SANDSTONE: Medium grained, dark red due to strong iron staining, indistinctly bedded. Trace of fine pyrite mineralisation.										SM, 10°, PL, SO, CLAYEY SAND 3MM	
			151	5												PT, 16°, PL, RO, SN	
																PT, 15°, PL, RO, CN	
																SO, 16°, PL, SO, CLAYEY SAND, 10MM	
				6												PT, 16°, PL, RO, CO	
						CBL terminated at 6.12m											
			150	7													
			140	8													

method	core lift	water	weathering	defect type	roughness
DT	 casing used	 10/1/99 water level on date shown	FR	JT	VR
AS	 barrel withdrawn	 water meter	SW	PT	RR
AD		 partial dry and wet	MW	SM	SO
MX		 complete dry fluid loss	MW	SZ	SL
CB			XW	GC	
NMLC			OW	CS	
NQ, HQ, PQ					
	 core recovered	 water pressure test result (fig mm) for depth interval shown			
	 graphic symbols indicate material		strength		
	 no core recovered		VL	planarity	coating
			L	PL	CN
			M	CU	SN
			H	UN	VN
			VH	SI	CO
			EH	R	

CORED BOREHOLE GEO-LOG COV23462AA GP, COFFEY BOT 4-19-08

form GEO 3.1.1 issue 3 Rev 3



drawn	MT	 SPECIALISTS MANAGING THE EARTH-	client	Taylor Thomson Whitting	
approved	SH		project:	185 FOX VALLEY ROAD, SAN HOSPITAL- WAHROONGA	
date	4/4/2002		title	ROCK CORE PHOTOGRAPH - CBH8	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH8 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH9**
 Sheet **1 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **13.3.2008**
 Date completed: **13.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting: Mobile Drill D60		Easting 323825.6		slope: -90°		R.L. Surface: 100.0	
hole diameter: 100 mm		Northing 626556.9		bearing:		datum: AID	
drilling information				material substance			
method	penetration	support	notes samples, tests, etc.	depth metres	classification symbol	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	structure and additional observations
ADV			E(x2)			FILL: BITUMEN and ROADBASE	FILL
			E(x3) + B5		CL	SANDY CLAY: Medium plasticity, orange brown, medium grained sand becoming more sandy with depth.	RESIDUAL SOIL Whit refusal at 0.6m
ADT			B5			SANDSTONE: Medium grained, pale grey and orange.	SANDSTONE
				1		Borehole CBH9 continued as cored hole	
				2			
				3			
				4			
				5			
				6			
				7			
				8			
method				support		notes, samples, tests	
AS AD RR W CT HA UI P V I				M - mud C - casing penetration 1 2 3 4 no refusal or refusal water 100% water level GR data shown water inflow water outflow		U _u - undisturbed sample 50mm diameter U _u - undisturbed sample 80mm diameter O - disturbed sample N - standard penetration test (SPT) N* - SPT - sample recovered N ₆₀ - SPT with 60kN cone V - vane shear (kPa) P - pressure meter B - bulk sample E - environmental sample R - refusal	
classification symbols and soil description based on unified classification system				consistency/density index			
moisture D - dry M - moist W - wet Wp - plastic limit WL - liquid limit				VS - very soft S - soft F - firm St - stiff VS _h - very soft H - hard Fb - brittle VL - very loose L - loose MC - medium dense D - dense VD - very dense			

Engineering Log - Cored Borehole

Borehole No **CBH9**
 Sheet **2 of 2**
 Project No **GEOTLCOV23462AA**
 Date started **13.3.2008**
 Date completed **13.3.2008**
 Logged by **JA**
 Checked by **SH**

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

drill model & mounting: Mobile Drift 890				Easting: 523825.6		skew: -80°		R.L. Surface: 160.0					
hole diameter: 100 mm Drilling fluid:				Northing: 6265888.9		bearing:		datum: AHD					
drilling information				material substance				rock mass defects					
method	core bit	water	RL	depth (m)	graphic log	core recovery	material	weathering	estimated strength	1500 MPa	1500 MPa	defect spacing mm	defect description
							rock type; grain characteristics, colour, structure, minor components	weathering alteration	VL	L	M	H	type, inclination, planarity, roughness, coating, thickness
									VL	L	M	H	particular
									VL	L	M	H	general
Continued from next-cored borehole													
NMLC			159	1			SANDSTONE: Medium grained, pale grey-orange and dark red, indistinctly to distinctly bedded at 5°, occasional bands of iron stained sandstone.	MW	0.33 0.33	0.33 0.33	0.33 0.33		PT, 5°, PL, SO, CO
			158	2					0.25 0.2	0.25 0.2	0.25 0.2		SM, 5°, IR, RO, CLAY/SAND, 20mm SM, 5°, IR, SO, CLAY/SAND, 20mm SM, 5°, IR, SO, CLAY/SAND, 20mm SM, 5°, IR, SO, CLAY/SAND, 50mm PT, 5°, PL, SO, CO
			157	3					0.18 0.2	0.18 0.2	0.18 0.2		JT 74°, IR, RO, SN PT, 5°, PL, SO, CO SM, 5°, PL, SO, CLAY, 180mm SM, 5°, PL, SO, CLAY, 40mm SM, 5°, PL, SO, CLAY, 25mm
			156	4			NO CORE	SW	0.21 0.24	0.21 0.24	0.21 0.24		PT, 5°, PL, SO, CLAY, 1mm SM, 5°, PL, SO, CLAY, 10mm PT, 5°, PL, SO, CO
			155	5					1.05 0.07	1.05 0.07	1.05 0.07		PT, 5°, PL, SO, CO PT, 5°, PL, SO, CO
			154	6					0.62 0.3	0.62 0.3	0.62 0.3		
			153	7			CBH9 terminated at 6.12m		0.66 1.25	0.66 1.25	0.66 1.25		
			152	8									

method	core bit	water	weathering	defect type	roughness
UP	diatase	10/1/98 water level on date shown	FR	joint	VR
AS	auger screwing	water inflow	SV	parting	MO
AD	auger drilling	partial and fluid loss	MW	seam	SO
RR	rotary zone	complete drill fluid loss	HW	sheared zone	SL
CB	claw or blade bit		NW	sheared surface	
NMLC	NMLC core		NW	crushed seam	
NO, NO, RO	whistle core		CH		

core bit	weathering	defect type	roughness
reaching used	FR	joint	VR
core recovered	SV	parting	MO
graphic symbols	MW	seam	SO
indicate material	HW	sheared zone	SL
no core recovered	NW	sheared surface	
	CH	crushed seam	

strength	planarity	coating
VL	planar	CN
L	curved	SN
M	undulating	VN
H	stepped	CO
VH	irregular	
CH		



drawn	MT	 SPECIALISTS MANAGING THE EARTH-	client	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH - CBHE	
scale	Not to scale		project no.	GEOTLCOV23462AA	Photo no: CBH9 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHRONGA**

Borehole Location: **Building 2**

Borehole No. **CBH10**

Sheet **1 of 2**

Project No: **GEOTLCOV23462AA**



Date started: **14.3.2008**

Date completed: **14.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model and mounting: **Mobile Dm 890** Easting: **323865** slope: **90°** R.L. Surface: **159.3**
hole diameter: **100 mm** Northing: **6265001.1** bearing: datum: **AID**

drilling information				material substance								
method	penetration	support	notes samples, tests, etc	RI	depth metres	grasp or log	classification symbol	material soil type, plasticity or particle characteristics, colour, secondary and minor components	moisture condition	consistency/ density index	depth meters	structure and additional observations
ADV			E Bg + E + D Bs E		159		CL	FILL: BITUMEN and ROADBASE CLAY: Medium plasticity, dark orange and brown, with some sand, medium grained sand.	<Wp	VSt		FILL RESIDUAL SOIL
					1			SANDSTONE. Medium grained, orange. Borehole CBH10 continued as cored hole				SANDSTONE V-bit ref. 18 at 0.5m
					158							
					2							
					157							
					3							
					156							
					4							
					155							
					5							
					154							
					6							
					153							
					7							
					152							
					8							
method	support			notes, samples, tests				classification symbols and soil description based on unified classification system		consistency/density index		
AS	auger screwing			M mud	N 14	U ₆₀	undisturbed sample 60mm diameter				VS	very soft
AD	auger drilling			C casing		U ₁₀₀	undisturbed sample 100mm diameter				S	soft
RR	roller/corer			penetration		O	disturbed sample				F	firm
YW	wand bore			1 2 3 4		N	standard penetration test (SPT)				St	stiff
QT	eggle log				no resistance refusal	N ₆₀	SPT - sample corrected				VS ₁	very stiff
HA	hand auger			water		N _c	SPT with solid cone				H	hard
OT	disturb				10/1/90 water level no data shown	V	vane shear (kPa)				Fa	mass
D	plank bit					P	pressuremeter				VI	very loose
V	V bit					Bs	bulk sample				L	loose
T	TC bit					E	environmental sample				MD	medium dense
*bit shown by suffix e.g.	ADT					R	refusal				D	dense
											VD	very dense

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 2**

Borehole No. **CBH10**

Sheet **2 of 2**

Project No: **GEOTLCOV23462AA**

Date started: **14.3.2008**

Date completed: **14.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model & mounting: Mobile Drill B30 Easting: 323885 slope: 90° R.L. Surface: 159.3
hole diameter: 100 mm Drilling fluid: Nothing Northing: 5265901.1 bearing: datum: AHD

drilling information					material substance			rock mass defects				
method	core-lift	water	RL	depth metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	Is _{pc} MPa D _{ukem} seal A: 2000	RCD %	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness
			159									
			158			Continued from non-cored borehole						
NMLC			158			SANDSTONE: Medium grained, orange and pale grey with some dark red iron staining bands.	MW	0.22 0.32				SM, 5°, IR, SO, CLAY, 10MM SM, 10°, IR, SO, CLAY, 2MM SM, 10°, PL, SO, CLAY, 2MM PT, 15°, PL, SO, CO SM, 10°, PL, SO, CLAY, 30MM PT, 15°, PL, RO, CN
			157									
			156			Trace pyrite mineralisation from seam at 3.81m.						SM, 5°, FL, SO, CLAY, 30MM JT, 60°, PL, SO, CLAY, 30MM PT, 5°, UN, SO, CO
			155				SW	1.37 1.67				PT, 5°, PL, SO, VN SM, 0°, PL, SO, CLAY, 80MM SM, 0°, PL, SO, CLAY, 55MM
			154									PT, 21°, PL, RO, SN
			153			CBH10 terminated at 6.10m						SM, 20°, PL, SO, CLAY, 10MM SM, 20°, PL, SO, CLAY, 10MM SM, 5°, PL, SO, CLAY, 2MM PT, 21°, PL, SO, CO
			152									

method DI AS AD FR CB NMLC NU, HQ, PC	dense auger screwing auger drilling cable tooling cable or blade bit NMLC core wireline core	core-lift casing used barrel withdrawn graphic log/core recovery core recovered graphic symbols indicate material no core recovered	water 10/1500 water level on depth shown water inflow partial drill fluid loss complete drill fluid loss water pressure test result (Ugeona) for depth interval shown	weathering FR SW MW HW XW DW strength VL L M H VH PH	high slightly weathered moderately weathered highly weathered extremely weathered distinctly weathered (covers MW and HW) very low low medium high very high extremely high	defect type JT PT SM SZ SS CS planarity PL CU UN ST R	roughness VR RO SO SL coating CN SN VN CO
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Job No. GEOTLCOV23462AA
CBH10
DEPTH: 0.96m - 6.19m



drawn:	MT	 SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	26 / 3 / 2008		title	ROCK CORE PHOTOGRAPH - CBH1C	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH10 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No: **CBH11**
 Sheet: **1 of 2**
 Project No: **GEOTLCOV23462AA**
 Date started: **14.3.2008**
 Date completed: **14.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting:		Mobile Drill B3C		Casting:		323671		slope:		-90°		R.L. Surface:		156.6	
hole diameter:		100 mm		Northing:		6265773		bearing:				datum:		AHD	
drilling information				material substance											
method	penetration	support	notes samples, tests, etc	depth metres	graphic log	classification symbol	material soil type; plasticity or particle characteristics, colour, secondary hard mineral components	moisture condition	consistency density index	100 kPa	200 kPa	300 kPa	water	structure and additional observations	
ADV			E E(x3) + Bs Bs E + Bs	156			FILL: SILTY SAND: Taproot, medium-grained sand, brown, grass roots, organics. FILL: SANDY CLAY: Medium plasticity, orange and pale grey, medium grained sand.	<wp						FILL Y-bit refusal on sandstone boulder at 7m	
		VC MONITORED		155			Borehole CBH11 continued as cored hole								
				154											
				153											
				152											
				151											
				150											
				149											
				148											
method				support		notes, samples, tests		classification symbols and soil description based on unified classification system				complete density index			
AS auger screwing AD super drilling RR rollercone W wireline CT cable tool EA hand auger DI dilator B blank bit V V bit T TC bit m shown by suffix 04				M mud C casing penetration 1 2 3 4 no resistance ranging to 100 mm water 10/150 water level on date shown water inflow water outflow		U _{un} undisturbed sample 50mm diameter U ₆₀ undisturbed sample 63mm diameter R disturbed sample H standard penetration test (SPT) H' SPT - sample recovered HRC SPT with solid cone V vane shear (kPa) P pressuremeter BS bulk sample E environmental sample R refusal		moisture D dry M moist W wet Wp plastic limit W _L liquid limit				VS very soft S soft F firm St stiff VS: very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense			

Job No. GEOTLCOV23462AA

CBH11

DEPTH: 1m – 6m



drawn	MT		client:	Taylor Thomson Whitting	
approved	SH		project:	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	26 / 3 / 2008		title	ROCK CORE PHOTOGRAPH – CBH11	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH11 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA

Boothole Location: **Building 2**Borehole No. **CBH12**

Sheet 1 of 2

Project No: **GEO TL COV23462AA**

Date started: 17.9.2008

Date completed: 17.9.2008

Logged by: **JA**

Checked by: **SH**

drill model and mounting:		Mobile Drill B&B		bearing: 323931.7		slope: 0°		R.L. Surface: 157.8				
hole diameter:		100 mm		Nonrig		6205920.5		bearing:				
datum:		AHD										
drilling information				material substance								
method	penetration	support	notes, samples, tests etc.	R.L.	depth metres	graphic log	classification symbols	material	moisture condition	consistency/density index	section penetration meter	structure and additional observations
ACV	1 2 3							soil type: plast clay or particle characteristics, colour, secondary and minor components				
			$E_{(x2)}$					FILL: BITUMEN and ROADBASE	D			FILL
			$D_s + E_{(x2)}$					FILL: CLAY: Medium plasticity, brown and orange, with some fine sand and fine gravel.	<Wp			
			D_s	157	1			FILL: CLAYEY SAND: Fine to medium grained, pale reddish brown, medium plasticity clay.	D			
			SPI 3, 5, 6 N=11					FILL: CLAY: Medium plasticity, pale orange and pale brown, with some fine grained sand.	<Wp			
				156	2			Becoming dark brown, red and pale grey, trace of rootlets, heterogeneous colouring.				
			SPT 2, 3, 7 N=10	155	3		CL	SANDY CLAY: Medium plasticity, pale yellow, fine grained sand. Evenly coloured with occasional root fragments.	S			RESIDUAL SOIL
												Inefficient SPT sample for PID test
												V-bit refusal at 3.64m
				154	4			Borehole CBH12 continued as bored hole				
				153	5							
				162	6							
				151	7							
				150	8							

method

AS auger screwing

AD auger drilling

RR rollerbit core

W washbore

CT cable tool

HA hand auger

OT other

S mark on

V V-bit

T TC bar

not shown by date

P.D. ADT

support

M mud

C casing

penetration 2 3 4

no resistance

water

100/100 water level on date shown

water inflow

water outflow

notes, samples, tests

U_u undisturbed sample 50mm dia meter

U_u undisturbed sample 45mm diameter

D disturbed sample

N standard penetration test (SPT)

SP1 - sample recovered

SP2 - SPT with solid cone

SP3 - cone shear (kPa)

P piezometer

BS bulk sample

E environmental sample

R refusal

classification symbols and soil description based on unified classification system

moisture

D dry

M moist

W wet

Wp plastic limit

WL liquid limit

VS very stiff

S stiff

F firm

St soft

VS1 very stiff

H hard

Fh fracture

VL very loose

L loose

MD medium dense

D dense

VD very dense

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH12**
 Sheet **2 of 2**
 Project No **GEOTLCOV23462AA**
 Date started: **17.3.2008**
 Date completed: **17.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model & mounting: Mobile Drill 880 Easting: 323831.7 slope: -80° R.L. Surface: 157.8
 hole diameter: 100 mm Drilling fluid: Northing: 6265920.5 bearing: datum: AHD

drilling information					material substance					rock mass defects										
method	core-lift	water	R1	depth metres	Core recovery	material	weathering alteration	estimated strength				Is _{sp} MPa	defect spacing mm				defect description			
						rock type, grain characteristics, colour, structure, minor components		VL	L	M	H	VH	EH		D - diam- etral	A - axial		type, inclination, planarity, roughness, coating, thickness		
														RQC %	IR	PL	SO	particular	general	
				157	1															
				158	2															
				155	3															
						Continued from non-cored borehole														
NM/LC				154	4	SANDSTONE: Medium grained, red, pale grey and yellow, indistinctly to distinctly bedded at 10°-20°. Significant 210mm thick seam from 3.74 - 3.95m	MW													
							SW													
				153	5															
				152	6															
						CBH12 terminated at 6.2m														
				151	7															
				150	8															

method DT AS RH RR CB NM/LC HQ, HQ, PO	distube auger sampling auger drilling rotary core down or live drill NM/LC core wireline core	core lift casing used barrel, wireline graphic log/core recovery core recovered graphic symbols indicate material on core recovered	water 10Y198 water level on data shown water inflow partial drill fluid loss complete drill fluid loss water pressure test result (if graphed) for depth interval shown	weathering FR fresh SN slightly weathered MN moderately weathered HW highly weathered MV extremely weathered RW extremely weathered (covers MN and HW) strength VL very low L low M medium H high VH very high EH extremely high	defect type JT joint PT parting SM seam SZ sheared zone SR sheared surface CS crushed seam planarity PL planar CR curved UN undulating ST stepped IR irregular roughness VR very rough RO rough SO smooth SL slickensided coating CN clean SN stained VN varnished CO coating
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drawn	M1	 coffey geotechnics SPECIALISTS MANAGING THE EARTH	client	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH – CBH12	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH12 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No. **CBH13**
 Sheet **1 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **18.3.2008**
 Date completed: **18.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting:		Mobile Drill 000		Easting		523905.94		slope:		90°		R.L. Surface:		161.0	
hole diameter:		100 mm		Northing		6265882.3		bearing:				datum:		AHD	
drilling information				material substance											
method	penetration	support	notes samples, tests, etc	depth	depth	graphic log	classification	material	moisture	consistency	density	penetration	structure and additional observations		
1	2	3		RL	method		symbol	soil type, plasticity or particle characteristics, colour, secondary and minor components.	condition	index	index	index			
ADP			E Bs + C	160	1			FILL: BITUMEN and ROADBASE	D				PR L		
			Bs + C + D					FILL: CLAY: Medium plasticity, brown and yellow, with some fine grained sand.	<wsp						
			SPT f, 11, 2, 1 W = R				CL	SANDY CLAY: Medium plasticity, yellowish brown trace of roots	VSR				Insufficient SPT sample for PID test		
								SANDSTONE: Medium grained, yellow and orange.					RESIDUAL SOIL		
								Borehole CBH13 continued as cored hole					V-br refusal at 1.48m		
				159	2								SANDSTONE		
				158	3										
				157	4										
				156	5										
				155	6										
				154	7										
				153	8										
method				support		notes, samples, tests		classification symbols and soil description based on unified classification system				consistency/density index			
AS	auger screwing		M	man	N	nd	U ₆	undisturbed sample 50mm diameter				VS	very soft		
AD	auger drilling		C	casing			U ₆₃	undisturbed sample 63mm diameter				S	soft		
RP	rotary percussion		penetration		1 2 3 4		D	disturbed sample				F	firm		
W	wireline						N	standard penetration test (SPT)				SI	stiff		
CT	cable tool						N'	SPT - sample recovered				VSI	very stiff		
HA	hand auger						N ₂	SPT with split cone				H	hard		
OT	drill						V	vibrating cone (VC)				PH	plastic		
B	block bit						P	pressuremeter				VL	very loose		
V	V bit						Bs	bulk sample				L	loose		
I	TC bit						F	environmental sample				MD	medium dense		
bit driven by air							R	refusal				D	dense		
e.g. ADT												VD	very dense		

Engineering Log - Cored Borehole

Borehole No. **CBH13**

Sheet 2 of 2

Project No: **GEO TL COV23462AA**

Date started: 18.3.2008

Date completed: 18.3.2008

Logged by: JA

Checked by: **SH**

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA

Borehole Location: **Building 2**

Part model & mounting: Mobile Unit BR0

Ending	323915.94
--------	-----------

_____ slope _____

8.1 Surface*	161.0
--------------	-------







hole diameter	700 mm	Drilling fluid:
---------------	--------	-----------------

Nothing: 6265982.3

head:00:

490 AHD

drilling information					material substance								rock mass defects									
method	core ID	water	RL	depth metres	graphic log core recovery	rock type; grain characteristics, colour, structure, size & proportions	weathering alteration	estimated strength					IS ₁₀₀ MPa	D diam. mm	A - axial	RO ₂ %	defect spacing mm	defect description				
								VC	L	M	H	SH	EH				type, location, planarity, roughness, coating, thickness					
																	particular	general				
			160	1																		
						Continued from non-cored borehole																
MACC			159	2		SANDSTONE: Medium grained, dark red to orange, laminated and pale grey leached rock. Indistinctly bedded at 20".	HW							U	A	27		SM, 0", IR, SO, sandy clay, 10mm				
						NO CORE:								U	A	0.17		SM, 0", IR, SO, clay, clay and wood/rool fragments, 100mm				
							HW											SM, 0", PL, SO, clay				
																		SM, 0", IR, SO, sandy clay + wood/rool fragments, 40mm				
			158	3														SM, 20", PL, SO, clay, 10mm				
																		SM, 20", PL, SO, clay, 10mm				
																		SM, 20", PL, SO, clay, 10mm				
																		PT, 20", PL, SO, CO				
							MW											PT, 20", IR, RO, CO				
																		SM, 0", PL, SO, clay, 30mm				
			167	4														SM, 0", PL, SO, clay, 130mm				
						SANDSTONE: Medium grained, pale grey, indistinctly to distinctly bedded. Trace of pyrite mineralisation	FR							U	A	0.94 1.36		PT, 4", PL, RO, CO, bent stained, 1mm				
			156	5																		
			155	6		NO CORE: 0.09m CBH13 terminated at 6m																
			154	7																		
			153	8																		

method	core ID	water	weathering	defect type	roughness
DT	normal	 100% water level on data shown	FR fresh	AT joint	VR very rough
AS	sugar screwing		SVV slightly weathered	PI pitting	RO rough
AO	sugar drilling		MW moderately weathered	SM seam	SO smooth
RR	rullen/corona	 water flow	HW highly weathered	G2 sheared zone	SL stockpiled
CS	claw or blade bit	 partial drill hole lines	XW extremely weathered	GS sheared surface	
AMLC	AMLC core	 complete rock thickness	QW distinctly weathered (common MW and HW)	CS crushed seam	
NO, HQ, PQ	wireline core				
			strength	planarity	coating
		 water pressure test result (legends) for depth interval shown	VL very low	PL planar	CN clean
			L low	CU curved	SN stained
			M medium	UN undulating	VN variegated
			H high	SI stepped	CO coating
			UH very high	IR irregular	
			EH extremely high		



drawn	MT	 SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH - CBH13	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH13 1 of 1
original size	A4				

Engineering Log - Borehole

Borehole No. **CBH14**
 Sheet 1 of 2
 Project No. **GEOTLCOV23462AA**
 Date started: **18.3.2008**
 Date completed: **18.3.2008**
 Logged by: **JA**
 Checked by: **SH**

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

drill model and mounting: Mobile Drill 880		Easting: 323945.6		slope: -90°		R.L. Surface: 159.7	
hole diameter: 100 mm		Northing: 6265882.3		bearing:		datum: AHD	
drilling information				material substance			
method	penetration	support	notes samples, tests, etc	depth metres	graphic log	classification symbol	material
ADV	123						soil type: plasticity or particle characteristics, colour, secondary and minor components.
			E				FILL: BITUMEN and ROADBASE
			E(x2) + Bs				FILL: CLAY: Medium plasticity, brown, yellow and pale grey, with some fine grained sand.
			Bs	159			
			SPT 5,7,10 N=17	1			
				158			
				2			
			SPT 7,12,13 N=25	157			CLAY: Medium plasticity, pale orange and brown, with some fine grained sand.
				3			SANDY CLAY: Medium plasticity, pale grey, becoming more sandy with depth.
							SANDSTONE: Medium grained, orange.
							Borehole CBH14 continued as cored hole
				156			
				4			
				155			
				5			
				154			
				6			
				153			
				7			
				152			
				8			
method				support		notes, samples, tests	
AS auger screwing				M mud N nil		U _x undisturbed sample 50mm diameter	
AD auger drilling				C casing		U ₅ undisturbed sample 63mm diameter	
RR roller/cone				penetration 1 2 3 4		D disturbed sample	
W washbore				no resistance ranging to refusal		N standard penetration test (SPT)	
CT cable tool						N [*] SPT - sample recovered	
HA hand auger						Nc SPT with solid cone	
DT diatube						V vane shear (kPa)	
B blank bit						P pressuremeter	
V V bit						Bs bulk sample	
T TC bit						E environmental sample	
*bit shown by suffix						R refusal	
e.g. ADT							
						classification symbols and soil description based on unified classification system	
						moisture	
						D dry	
						M moist	
						W wet	
						Wp plastic limit	
						W _L liquid limit	
						consistency/density index	
						VS very soft	
						S soft	
						F firm	
						St stiff	
						VSt very stiff	
						H hard	
						Fb friable	
						VL very loose	
						L loose	
						MD medium dense	
						D dense	
						VD very dense	

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 2**

Borehole No.	CBH14
Sheet	2 of 2
Project No.	GEOTLCOV23462AA
Date started:	18.3.2005
Date completed:	18.3.2008
Logged by:	JA
Checked by:	SH

drilling information				material substance				rock mass defects			
method	core-lift	water	RL	depth metres	rock type; grain characteristics, colour, structure, minor components	weathering	estimated strength	15 cm MPa D - diametral A - axial	RCD % D A 10 20 30 100 300	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness
				158							
				158							
				157							
				156							
				155							
				154							
				153							
				152							



drawn	MT	 SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting	
approved	SH		project:	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 200E		title:	ROCK CORE PHOTOGRAPH – CBH14	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH14 1 of 1
original size	A4				

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 1**

Borehole No.	CBH15
Sheet	1 of 2
Project No:	GEOTLCOV23462AA
Date started:	18.3.2008
Date completed:	18.3.2008
Logged by:	JA
Checked by:	SH

[illegible]

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No: **CBH15**
 Sheet: **2 of 2**
 Project No: **GEOTLCOV23462AA**
 Date started: **18.3.2008**
 Date completed: **18.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model & mounting: Mobile Drill R80		Fasting: 373697		slope: -90°		R.L. Surface: 159.5														
hole diameter: 100 mm Drilling fluid:		Mething: 8785706 3		bearing:		datum: AHD														
drilling information				material substance				rock mass defects												
method	core lift	water	RL	depth metres	graphic log core recovery	material rock type, grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	log MPa Q-diameter A-axial	RQC %	defect spacing mm	defect description								
												particular	general							
			156	1																
			155	2																
NMLC	NOT MONITORED		154	3		Continued from non-cored borehole SANDSTONE: Medium grained, orange, pale yellow and pale grey with leached clay seams. Indistinctly to distinctly bedded at 25°.	MW		D A 0.20 0.32			SM, 0° PL, SO, clay, 70mm PT, 25° PL, RO, CN PI, 25° PL, SO, clay, 3mm SM, 0° PL, SO, clay, 50mm PI, 3° PL, SO, CO PT, 20° PL, SO, clay, 5mm								
			153	4					D A 0.42 0.47			PT, 0° IR, RO, CN PT, 25° PL, RO, CN PT, 25° PL, RO, CN PT, 25° PL, RO, CO PT, 25° PL, RO, CO								
			152	5		SANDSTONE: Medium grained, dark red and orange with pale grey leached seams. Trace of pyrite mineralisation.			D A 1.69 2.4			PT, 25° PL, RO, clayey sand, 10mm PT, 25° PL, RO, SN								
			151	6					D A 0.76 1.05											
			150	7		SANDSTONE: Medium grained, pale grey with minor pale orange CBH15 terminated at 6.2m	FR		D A 0.55 0.43											
			149	8																
method				core lift				water				weathering		defect type		roughness				
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD
DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD	DT	AS	AD	RR	CB	NMLC	NO, HQ, PD



drawn	MT	 coffey geotechnics <small>SPECIALISTS MANAGING THE EARTH</small>	client:	Taylor Thomson Whitting	
approved	ST		project:	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2008		title	ROCK CORE PHOTOGRAPH - CBH15	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH15 1 of 1
original size	A4				

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 3**

Borehole No. **CBH16**

Sheet **1 of 3**

Project No: **GEOTLCOV23462AA**

Date started: **19.3.2008**

Date completed: **19.3.2008**

Logged by: **JA**

Checked by: **SH**

drill model and mounting: Mobile Drill B80 Easting: 323761.9 slope: -90° R.L. Surface: 181.1
hole diameter: 100 mm Northing: 8265860.7 bearing: datum: AHD

drilling information				material substance					
method	penetration	support	notes, samples, tests, etc.	depth metres	graphic log	classification symbol	material	moisture condition	structure and additional observations
ADV	2.3			11			FILL: SILTY SAND: Topsoil, medium grained sand, brown, grass roots and organics. FILL: SAND: Sand fine to medium grained, trace of clay, concrete rubble and organic fragments.	D	FILL
ADT				160			FILL: CLAYEY SAND: Medium grained, reddish brown, with some concrete rubble. FILL: SANDY CLAY: Medium plasticity, brown and pale grey, with some sandstone cobbles.	AWp	Void refusal on fir cobbles at 1m.
				159					
				158					
				157			FILL: CLAY: Medium plasticity, orange and green. FILL: CLAY: Medium plasticity, black and pale brown, with some fine grained sand. FILL: GRAVELLY CLAY: Medium plasticity, greenish yellow, cobbles of monstone.		Unknown black substance, odourless. Insufficient SPT sample for PID (4.05-4.25m)
				156			Borehole CBH16 continued as cored hole		
				165					
				164					
				163					
				162					
				161					
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				12					
				11					
				10					
				9					
				8					
				7					
				6					
				5					
				4					
				3					
				2					
				1					

method	support	notes, samples, tests	classification symbols and soil description based on unified classification system	consistency/density index
AS AD HX VW CT HA DT B V T "oil shown by surface e.g. ADT"	M - mud C - casing penetration 2, 3, 4 no increase penetration refusal water 10/1/08 water level on date shown water inflow water outflow	U _u - undisturbed sample 50mm diameter U _u - undisturbed sample 63mm diameter D - disturbed sample T - standard penetration test (SPT) N ₁ - SPT - sample recovered N ₂ - SPT with solid core V - vane shear (kPa) P - pressuremeter B _s - bulk sample E - environmental sample R - refusal	Moisture condition D - dry M - moist W - wet W _p - plastic limit W _L - liquid limit	VS - very soft S - soft F - firm St - stiff VSt - very stiff H - hard Ht - medium VL - very loose L - loose ML - medium dense D - dense VD - very dense

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 3**

Borehole No. **CBH16**
 Sheet **2 of 3**
 Project No. **GEOTLCOV23462AA**
 Date started **19.3.2008**
 Date completed **19.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model & mounting: Mobile DRI 880				Easting: 323761.8		slope: -90°		R.L. Surface: 161.1			
hole diameter: 100 mm Drilling fluid:				Northing: 6265660.7		bearing:		datum: AHD			
drilling information				material substance				rock mass defects			
method	core-lift	water	RL	depth metres	graphic log core recovery	material rock type, grain characteristics, colour, structure, minor components	weathering classification	estimated strength	IS _{sp} MPa D ₅₀ (mm) F ₈₀ (mm) A _v (mm)	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness
				163							
				160	1						
				159	2						
				158	3						
				157	4						
				156	5						
				155	6						
				164	7						
					8						
NOT MONITORED											
NMLC											
Continued from non-cored borehole											
SANDSTONE: Medium grained, dark red but stained and pale grey leached zones. Indistinctly bedded at 23°.											
SANDSTONE: Medium grained, pale grey and pale orange.											
water											
10/100mm water level on d 210 shown											
water inflow											
partial fluid loss											
complete fluid loss											
water pressure test result (fluquons) for depth interval shown											
weathering											
FR fresh											
SW slightly weathered											
MW moderately weathered											
HW highly weathered											
XW extremely weathered											
DW defectively weathered (covers MW and HW)											
strength											
VL very low											
L low											
M medium											
H high											
VH very high											
EH extremely high											
defect type											
JT joint											
PT parting											
SM seam											
SZ sheared zone											
SS sheared surface											
CS rough seam											
planarity											
PL planar											
CU curved											
UN undulating											
ST stepped											
IR irregular											
roughness											
VR very rough											
RH rough											
SO smooth											
SI slickensided											
coating											
CN clean											
SN stained											
VM varnish											
CO coating											

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 3**

Borehole No. **CBH16**
 Sheet **3 of 3**
 Project No. **GEOTLCOV23462AA**
 Date started: **19.3.2008**
 Date completed: **19.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drilling information				material substances				rock mass defects				
method	core-lit	water	RL	depth metres	graphic log core recovery	rock type; grain characteristics, colour, structure, size & components	weathering alteration	estimated strength	$I_{s, \text{avg}}$ MPa	$I_{s, \text{max}}$ MPa	defect spacing mm	defect description
NMLC			153			SANDSTONE: Medium grained, pale grey and pale orange. (continued)	MW		0.24	0.4		PT, 20°, PL, RO, CO SM, 15°, PL, RO, sand with some clay, 10mm PT, 15°, PL, SO, CO PT, 15°, PL, SO, CO PT, 10°, PL, SO, CO
			150	9		CLAY SEAM: Low plasticity, pale grey with brown laminations.						
			151	10		SANDSTONE: Medium grained, pale orange and grey. NO CORE: 0.08m	MW		0.52	0.63		SM, PL Sandy clay 80mm
			150	11		SANDSTONE: Fine grained, pale grey with brown laminations. Distinctly bedded at 0°-5°.	MW		0.85	0.88		PT, 5°, PL, RO, SN PT, 0°, ST, RO, SN
			148	12		SANDSTONE: Medium grained, dark red, orange and pale yellow, mottled strong iron staining. Indistinctly to distinctly bedded at 10°-15°.			1.18	1.02		JT, 30°, PL, RO, SW PT, 15°, PL, RO, SN
			148	13		CBH16 terminated at 12.05m						
			147	14								
			146	15								
			146	16								

method	core-lit	water	weathering	defect type	roughness
DT	DT	10/198 water level on date shown	FW	JT	VR
AS	AS	water inflow	SW	PT	RO
AD	AD	partial drill fluid loss	MW	SM	SD
RR	RR	complete drill fluid loss	HW	SZ	SI
CB	CB		XW	SS	
NMLC	NMLC		UW	CS	
NQ, HQ, PQ	NQ, HQ, PQ				

core-lit	water	weathering	defect type	roughness
causing used	10/198 water level on date shown	FW	JT	VR
barrel withdrawn	water inflow	SW	PT	RO
graphic log/core recovery	partial drill fluid loss	MW	SM	SD
core recovered	complete drill fluid loss	HW	SZ	SI
- graphic symbols indicate material		XW	SS	
no core recovered		UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	


water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO
partial drill fluid loss	MW	SM	SD
complete drill fluid loss	HW	SZ	SI
	XW	SS	
	UW	CS	

water	weathering	defect type	roughness
10/198 water level on date shown	FW	JT	VR
water inflow	SW	PT	RO



Job No. GEOTLCOV23462AA
CBH16
DEPTH: 5.05m – 12.05m



drawn	MT	 SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	4 / 4 / 2006		title	ROCK CORE PHOTOGRAPH – CBH1E	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH16 1 of 1
original size	A4				

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 2**

Borehole No.	CBH17
Sheet	1 of 2
Project No:	GEOTLCOV23462AA
Date started:	19.3.2008
Date completed:	19.3.2008
Logged by:	JA/MT
Checked by:	SH

[illegible]

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole Location: **Building 2**

Borehole No:	CBH17
Sheet:	2 of 2
Project No:	GEOTLCOV23462AA
Date Started:	19.3.2008
Date completed:	19.3.2008
Logged by:	JA/MT
Checked by:	SH

drilling information				material substance				rock mass defects			
method	core-lift	water	Rt	depth metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	Is _{pn} MPa D-dam- aged A-axial	defect spacing mm	defect description type: inclination, planarity, roughness, coating, thickness
				157	1						
				158	2						
				155	3						
				154	4						
				153	5						
				152	6						
				151	7						
				150	8						



drawn	MTI	 coffey geotechnics SPECIALISTS MANAGING THE EARTH	client:	Taylor Thomson Whitting		
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA		
date	4 / 4 / 2006		title	ROCK CORE PHOTOGRAPH - CBH17		
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no:	CBH17 1 of 1
original size	A4					

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole location: **Building 3**

Borehole No. **CBH18**
 Sheet **1 of 3**
 Project No. **GEOTLCOV23462AA**
 Date started: **19.3.2008**
 Date completed: **20.3.2008**
 Logged by: **MT**
 Checked by: **SH**

drilling information				material substance			
method	penetration	notes, samples, tests, etc.	depth (metres)	graphic log	classification symbol	material	structure and additional observations
ADV	12.3		159			FILL: SILTY CLAY: Low plasticity, dark brown, with some fine grained sand, shale gravel and igneous gravel.	
		E + Bs					
		Bs					
		SPT 2.3.3 N=6	158			FILL: SAND: Fine to medium grained, pale brown.	
						FILL: SILTY CLAY: High plasticity, red and dark brown with some root fibres, some fine grained sand and trace of gravel.	
			157				
		SPT 3.5.3 N=8					
			156				
		SPT 1.1.2 N=3					
			155				
		SPT 2.1.1 N=2					
			154				
			153				
			152			SANDY CLAY: High plasticity, orange-brown, pale grey mottled red. Sand is fine to medium grained.	
						Borehole CBH18 continues as cored hole	
							RESIDUAL SOIL

Borehole Section 23462AA GPJ Coffey GBT 4.18.08

Form GEO 3.3 Issue 3 Rev 2

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
Principal: **Coffey Projects**
Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
Borehole location: **Building 3**

Borehole No:	CBH18
Sheet:	2 of 3
Project No:	GEOTLCOV23462AA
Date started:	19.3.2008
Date completed:	20.3.2008
Logged by:	MT
Checked by:	SH

drill model & mounting: Mobil Dril B&D										Easting: 323738.9		shape: -90°		R.L. Surface: 169.7	
hole diameter: 100 mm. Drilling fluid:										Northings: 6255648.5		bearing:		datum: AHD	
drilling information					material substance					rock mass defects					
method	core-lift	water	R.L.	depth: metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength V _u J _u S _u T _u U _u	log ₁₀ KPa sk. diam. - sk. - axis	RQD % 20 100 200 300 400 500	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness			
												particular	general		
			160												
				158	1										
				157	2										
				156	3										
				155	4										
				154	5										
				153	6										
					7	Continued from non-cored borehole									
NMJC			152			SANDSTONE: Fine to med. gr. (pinkish, orange-brown and pale grey, indistinctly bedded at 0°-20°).	MW		D _u A _u 1.47 1.13	98					
				151	8										

method

DT dual tube
AS auger-screwing
AD auger drilling
RR rollerbit/crusher
CB crew or made by
NAC NAC core
NQ, HQ, PQ

core-lift

casing used
 band with draw

graphic log/core recovery

core recovered
 graphic symbols
 indicate material
 no core recovered

water

10/198 water level on data shown
 water inflow
 partial drill fluid loss
 complete drill fluid loss

water pressure test result (lugons) for depth interval shown

water pressure test result (lugons) for depth interval shown

weathering

FR fresh
SW slightly weathered
MW moderately weathered
HW highly weathered
XW extremely weathered
CW distinctly weathered (covers MW and HW)

strength

VL very low
L low
M medium
H high
VH very high
CH extremely high

defect type

JT joint
PS parting
SM seam
SZ sheared zone
SS sheared surface
CS crushed seam

planarity

FL planar
CU curved
UN undulating
ST stepped
IR irregular

roughness

VR very rough
RO rough
SO smooth
SI slickensided

coating

CH clean
SH silty
VN varnish
CO coating

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: **Building 3**

Borehole No. **CBH18**

Sheet **3 of 3**

Project No. **GEOTLCOV23462AA**

Date started: **19.3.2008**

Date completed: **20.3.2008**

Logged by: **MT**

Checked by: **SH**

drill model & mounting: Noble Drill 880				Easting: 328738.3		Slope: -90°		R.L. Surface: 169.1			
hole diameter: 100 mm Drilling fluid:				Northing: 6285648.5		bearing:		datum: AHD			
drilling information				material substance				rock mass defects			
Method	Cone-IM	Water	RI	depth metres	graphic log core recovery	material rock type; grain characteristics, colour, structure, minor components	weathering alteration	estimated strength A B C T S R	IS _{sp} MPa C ₀ unconf. axial A axial	defect spacing mm 2 100 300 1000 3000	defect description type, inclination, planarity, roughness, coating, thickness particular general
MMLC			151			SANDSTONE: fine to medium grained, orange-brown and pale grey. Indistinctly bedded at 0°-20° (continued)	AW		D A 1.1 1.35		
			160	9		Becoming distinctly bedded at 0°-20°.	SW		D A 0.73 0.82		PT, 15°, PL, SO, CN PI, 0°, PL, SO, SN SM, 0°, PL, SO, clay, 5mm
			149	10					D A 0.98 1.22		PT, 10°, UN, RO, SN
			148	11					D A 1.11 1.08		SM, 0°, PL, SO, clay, 5mm PT, 0° UN, RO, CN
			147	12					D A 1.67 1.03		
						CBH18 terminated at 12.18m					
			148	13							
			145	14							
			144	15							
			144	16							

Method DT auger drilling AS auger drilling AU auger drilling RR rotary CB core NMLC NMLC core NQ, HQ, PQ wireline core	cone-IM casing used barrel withdrawn graphic log/core recovery core recovered - graphic symbols indicate material no core recovered	water 10/198 water level on date shown water inflow partial drill fluid loss complete and free loss water pressure test result (key cone) for depth interval shown	weathering FR fresh SW slightly weathered MW moderately weathered HW highly weathered XW extremely weathered OW distinctly weathered (covers HW and XW) strength VL very low L low M medium H high VH very high E+ extremely high	defect type JT joint PT parting SM seam SZ sheared zone SS shattered surface CS crushed seam planarity PL planar CU curved UN undulating SI stepped IR irregular roughness VR very rough RC rough SO smooth SL slickensided coating CN clean SN stained VN varnished CO coating
--	--	--	--	---



drawn	MT	 <p>coffey geotechnics SPECIALISTS MANAGING THE EARTH</p>	client:	Taylor Thomson Whitting	
approved	SH		project:	185 FOX VALLEY ROAD, SAN HOSPITAL WAHROONGA	
date	26 / 3 / 2008		title	ROCK CORE PHOTOGRAPH - CBH1E	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH1E 1 of 1
original size	A4				

Engineering Log - Borehole

Flonhole No. CBH19

Sheet 1 of 2

Project No: **GEOTLCOV23462AA**

Date started: 20.3.2008

Date completed: 20.3.2008

Logged by: **MT**

Checked by: **SH**

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: 185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA

Borehole Location: **Building 1**

[illegible]

Engineering Log - Cored Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No. **CBH19**
 Sheet **2 of 2**
 Project No. **GEOTLCOV23462AA**
 Date started: **20.3.2008**
 Date completed: **20.3.2008**
 Logged by: **MT**
 Checked by: **SH**

drill model & mounting: Mobile Drill B80				Easting: 323882.5		slope: -90°		R.L. Surface: 150.5											
hole diameter: 100 mm Drilling fluid:				Northing: 6285738.9		bearing:		datum: AHD											
drilling information				material substance				rock mass defects											
method	core-lift	water	depth metres	graphic log core recovery	material rock type: grain characteristics, colour, structure, minor components	weathering alteration	estimated strength	IS _{avg} MPa D diam- eter A axial	RQD %	defect spacing mm	defect description								
											type, inclination, planarity, roughness, coating, thickness	particular	general						
			156																
			155																
			154		Continued from non-cored borehole														
NWLC			2		SANDSTONE: fine to medium grained, orange-brown and pale grey. Indistinctly to distinctly bedded at 0°-15°.	SW		D A 0.43 0.37	100		SM, 10°, PL, 5mm SM, 0°, PL, 15mm								
	NOT MONITORED		3		Becoming red and orange-brown	HW		D A 0.12 0.1			SM, 0°, PL, 5mm								
			153					D A 0.53 0.46			SM, 0°, PL, 20mm								
			4		Becoming pale grey stained orange-brown and red.	RW/MW		D A 0.5 0.48			PT, 10°, PL, SO, VN								
			5		Becoming pale grey.	FR		D A 0.22 0.77	100		JT, 65°, PL, SO, clay, 10mm JT, 65°, PL, RO, CN								
			151		Becoming red and orange-brown stained pale grey.	HW													
			6		CBH19 terminated at Bm														
			150																
			149																
			8																
method DT auger AS auger screwing AD auger drilling RR roller reamer CR claw or blade bit NWLC NWLC core RW, HQ, PQ wireline core				core-lift casing used barrel withdrawn graphic log/core recovery core recovered graphic symbols indicate material no core recovered				water 1/21/08 water level on data shown water inflow partial drill fluid loss complete drill fluid loss water pressure test result (megapascals) for depth interval shown				weathering FR fresh SW slightly weathered MW moderately weathered HW highly weathered XW extremely weathered FSW distinctly weathered (covers MW and HW) strength VL very low L low M medium H high VH very high EH extremely high				defect type JT joint PT parting SM seam SZ sheared zone SS shear surface CS crushed seam planarity PL planar CU curved UN undulating ST stepped IR irregular roughness VR very rough RO rough SO smooth SL slickensided coating CN clean SN stained VN variegated CO crusting			



drawn	MT		client	Taylor Thomson Whitting	
approved	SH		project	185 FOX VALLEY ROAD, SAN HOSPITAL. WAHROONGA	
date	26 / 3 / 2008		title	ROCK CORE PHOTOGRAPH – CBH15	
scale	Not to scale		project no:	GEOTLCOV23462AA	Photo no: CBH15 1 of 1
original size	A4				

Client: **Taylor Thomson Whitting**

Principal: **Coffey Projects**

Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**

Borehole Location: *Building 3*

Borehole No. CBH20

Steel 1 of 1

Project No. **GEOTLCOV23462AA**

Date started: 20.3.2008

Date completed: 20.3.2008

Logged by: **MT**

Checked by: **SH**

[illegible]

Engineering Log - Borehole

Client:	Taylor Thomson Whitting
Principal:	Coffey Projects
Project:	185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA
Borehole Location:	Building 3

Borehole No.	CBH21
Sheet	1 of 1
Project No.	GEOTLCOV23462AA
Date started	25.3.2008
Date completed	25.3.2008
Logged by:	JA
Checked by:	SH

drill model and mounting

Mobile Data Base

Easting: 323757.8

slope: -90°

R.L. Surface: 160.7

hole diameter: 100 mm

Northing: 6265655.53

bearing:

datum: AHD

drilling information

material substance

method	penetration	support	notes samples tests etc	Rt	depth metres	graphic log	classification symbol	material	moisture condition	consistency/density index	socket penetrometer	structure and additional observations
1	2	3						soil type: plasticity or particle characteristics, colour, secondary and trace components.			100 200 300 400 mm	
ADT			E		160			FILL: SILTY SAND: Fine grained, dark brown, Topsoil and grass FILL: SAND: Fine grained brown, with some silt, clay and gravel	D			FILL
			E									
			E									
			SPT 2.3.3 N=8		161			FILL: SANDY CLAY: Medium plasticity, red, pale grey, orange and brown, medium grained sand, with some gravel and cobbles	<WP			Insufficient SPT sample for PID test
					162							
			SPT 4.3.4 N=7		163			FILL: SANDY CLAY: Medium plasticity, brown, medium grained sand. FILL: CLAY: Medium plasticity orange and red, with some sand and cobbles.				
					164							
			SPT 2.2.4 N=8		165							
					166		SM	SILTY SAND: Fine grained, brownish grey.	D	MD		Insufficient SPT sample for PID test RESIDUAL SOIL
					167							
					168			SANDSTONE. Fine grained, orange and pale grey.				V-bit refusal at 4.7m SANDSTONE
			E		169							
					170			Borehole GBH21 terminated at 5.1m				
					171							
					172							
					173							
					174							
					175							
					176							
					177							
					178							
					179							
					180							
					181							
					182							
					183							
					184							
					185							
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					188							
					189							
					190							
					191							
					192							
					193							
					194							
					195							
					196							
					197							
					198							
					199							
					200							

method

AS auger screwing

AD auger drilling

RR core/drill core

W washbore

CT cable tool

HA hand auger

DT diaphane

B blank bit

V vial

I TC on

not known by suffix

ADT

support

M mud

C casing

penetration

1 2 3 4

no resistance ranging to refusal

water

0.1/99 water (air) or data shown

water down

water runoff

notes, samples, tests

U_{un} undisturbed sample 50mm diameter

U_{un} undisturbed sample 40mm diameter

D disturbed sample

N standard penetration test (SPT)

N₁ SPT - sample measured

N₂ SPT with solid cone

V vane shear (kPa)

P pressuremeter

BU bulk sample

E environmental sample

R refusal

classification symbols and soil description

based on unified classification system

Moisture

D dry

M moist

W wet

Wp plastic limit

WL liquid limit

consistency/density index

VS very soft

S soft

F firm

St stiff

YB very stiff

H hard

Fa friable

VL very loose

L loose

MD medium dense

D dense

VD very dense

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 1**

Borehole No: **CBH22**
 Sheet: **1 of 1**
 Project No: **GEOTLCOV23462AA**
 Date started: **25.3.2008**
 Date completed: **25.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting:		Mobile Unit 8811		Easting:		323689.5		slope:		-80°		R.L. Surface:		156.5	
hole diameter:		100 mm		Northing:		6285750.2		bearing:				datum:		AND	
drilling information						material substance									
method	penetration		support	water	notes samples, tests, etc.	R.L.	depth metres	graphic log	classification symbol	material	moisture condition	consistency/density index	penetration kPa	structure and additional observations	
ADT	1	2								soil type: plasticity or particle characteristics, colour, secondary and minor components.					
										FILL: BITUMEN and ROADBASE	D			FILL	
										FILL: CLAYEY SAND: Medium grained, orange, pale grey and red, medium plasticity clay, with some sandstone cobbles.					

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No: **CBH23**
 Sheet: **1 of 1**
 Project No: **GEOTLCOV23462AA**
 Date started: **25.3.2008**
 Date completed: **25.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting: Mobile DRI 880		Easting: 323850		slope: -30°		R.L. Surface: 159.0	
hole diameter: 100 mm		Northing: 6265905.6		bearing: 		datum: AHD	
drilling information				material substance			
method	penetration	support	notes samples, tests, etc.	depth metres	graphic log	classification symbols	material soil type: plasticity or particle characteristics, colour, secondary and minor components.
ADT	1 2 3	NOT OBSERVED					
				159			FILL: BITUMEN and ROADBASE
				158			FILL: CLAYEY SAND: Fine grained, orange-brown, medium plasticity clay, with some gravel.
				157			SANDSTONE: Fine to medium grained, orange and pale grey.
				156			
				155			
				154			
				153			
				152			
Borehole CBH23 terminated at 1.1m							
method		support	notes, samples, tests	classification symbols and soil description based on unified classification system		consistency/density index	
AS	auger screening	M: mud	undisturbed sample 70mm diameter	moisture		VS very soft	
AD	auger drilling	C: casing	undisturbed sample 62mm diameter	M: moist		S soft	
RR	rotary rig	penetration	disturbed sample	W: wet		F firm	
W	washbore	no resistance ranging to refusal	standard penetration test (SPT)	wp: plastic limit		SI stiff	
CT	cable tool		SPT - sample recovered	VL: liquid limit		VST very stiff	
HA	hand auger		SPT with solid cone			H hard	
DI	disturb		water slurry (N/A)			Fb flexible	
K	U-test bit		pressuremeter			VL very loose	
V	V bit		bulk sample			L loose	
I	TC rig		environmental sample			MD medium dense	
W	water shown by surface		refusal			D dense	
eg	ADT					VD very dense	

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHROONGA**
 Borehole Location: **Building 2**

Borehole No: **CBH24**
 Sheet: **1 of 1**
 Project No: **GEOTLCOV23462AA**
 Date started: **25.3.2008**
 Date completed: **25.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill method and recording:		Mobile Drill BHD		Facing		323832.3		slope:		-90°		R.L. Surface:		161.2	
hole diameter:		100 mm		Nothing		8785870.7		bearing				datum:		AHD	
drilling information						material substance									
method	1	2	3	notes samples, tests, etc	RL	depth metres	graphic log	classification symbols	material soil type: plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency density index	packet penetration kPa	meter	structure and additional observations	
ADT				NOT OBSERVED	161				FILL: BITUMEN and ROADBASE					FILL	
					159				FILL: SAND: Fine to medium grained, grayish brown, with some silt, gravel and cobbles						
					158				SANDSTONE: Medium grained, orange and pale grey					SANDSTONE	
					160				Borehole CBH24 terminated at 1m						
					159										
					158										
					157										
					156										
					155										
					154										
method		auger driving*		M: mud		N: fill		notes, samples, tests		classification symbols and soil description based on unified classification system		consistency/density index			
AD		auger drilling*		C: casing		penetration 1 2 3 4		U _u : undisturbed sample 50mm diameter				VS: very soft			
KH		interferometer						U _u : undisturbed sample 63mm diameter				S: soft			
W		washbore						G: disturbed sample				F: firm			
OT		cable tool						N: standard penetration test (SPT)				SI: stiff			
HA		hand auger						N ⁺ : SPT - sample recovered				VS1: very soft			
DT		dialube						Nc: SPT with solid cone				H: hard			
B		blank bit						V: vane shear (kPa)				F: brittle			
V		Vane						P: pressuremeter				VL: very loose			
T		TC bit						Ds: bulk sample				I: loose			
*As shown by suffix e.g. AD3								T: environmental sample				MD: medium dense			
								R: refusal				D: dense			
												VD: very dense			

Engineering Log - Borehole

Client: **Taylor Thomson Whitting**
 Principal: **Coffey Projects**
 Project: **185 FOX VALLEY ROAD, SAN HOSPITAL, WAHRDONGA**
 Borehole Location: **Building 2**

Borehole No.: **CBH25**
 Sheet: **1 of 1**
 Project No.: **GEOTLCOV23462AA**
 Date started: **25.3.2008**
 Date completed: **25.3.2008**
 Logged by: **JA**
 Checked by: **SH**

drill model and mounting:		Mobile D87B80		Easing		323857.0		slope:		00°		R1 Surface		161.4					
hole diameter:		100 mm		Nothing		6255574.4		bearing:				datum:		AHD					
drilling information				material substance															
method	penetration	support	water	notes samples, tests, etc	RL	Depth metres	graphic log	classification symbol	material soil type, plasticity or particle characteristics, colour, secondary and minor components.	moisture condition	consistency density index	poCKET penetro- meter mm	structure and additional observations						
ADT	123	NOT OBSERVED			161	1			FILL: BITUMEN and ROADBASE				FILL						
					161	1			FILL: GRAVELLY SAND: Medium grained, greyish brown, medium to coarse sandstone gravel										
					161	1			SANDSTONE: Medium grained, pale yellow.				SANDSTONE						
					160	2			Borehole CBH25 terminated at 1m										
					159	3													
					158	4													
					157	5													
					156	6													
					155	7													
					154	8													
methods AS auger 'scrapping' AD auger drilling RR wireline W washbore LT cable tool HA hand auger DT delube B block bit V V bit T TC bit *bit shown by suffix e.g. ADT				support M mud C casing penetration 1 2 3 4 no resistance suspension refusal water 10/150 water level run data shown water inflow water outflow				notes, samples, tests U ₁₀ undisturbed sample 50mm diameter U ₅₀ undisturbed sample 50mm diameter D disturbed sample N standard penetration test (SPT) R ₁ SPT - sample recovered H ₁ SPT with solid core V vane shear (kPa) P pres-suremeter B ₁ bulk sample E environmental sample R refusal				classification symbols and soil description based on unified classification system moisture D dry M moist W wet W _p plastic limit W _L liquid limit				consistency/density index VS very soft S soft F firm SL stiff VSI very stiff H hard VH very hard VI very tough L loose MD medium dense D dense VD very dense			

Appendix B

Laboratory Test Reports

Report No: CBR:LCOV089-01180

Issue No: 1

This report replaces all previous issues of report no: CBR:LCOV089-01180.

California Bearing Ratio

Client: Coffey Geotechnics Pty Ltd
8/12 Mars Road
Lane Cove NSW 2066

Principal:

Job No: LABTLCOV00268AA

Project: GEOTLCOV23462AA

Lot No:

TRN:



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Approved Signatory: Marshall Webster
(Laboratory Manager)
NATA Accredited Laboratory Number: 431
Date of Issue: 22/04/2008

Sample Details

Product:

Date Sampled: 7/04/2008

Source:

Sampling Method:

Location: SAN Hospital, Wahroonga

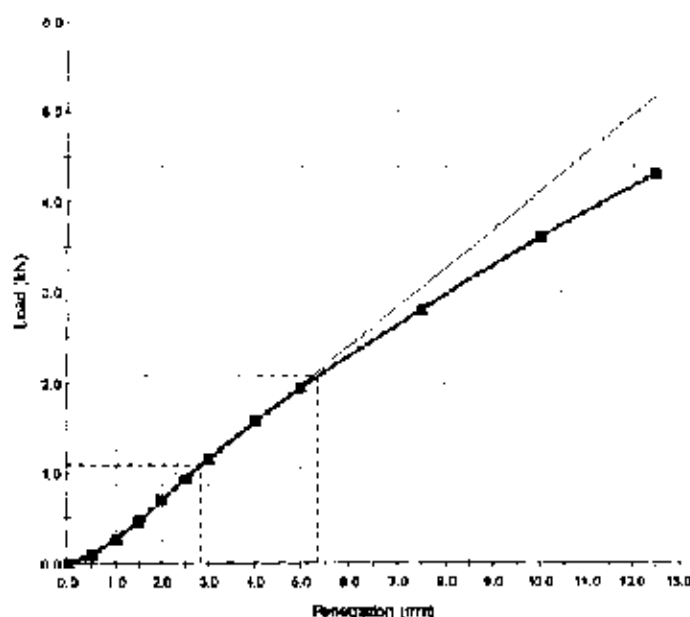
Sample ID: LCOV089-01180

Client Ref: CBH 15

Test Results

Chart

Description	Result
Test Method	AS 1289.6.1.1
Maximum Dry Density (t/m^3)	1.970
Optimum Moisture Content (%)	11.2
CBR 2.5mm (%)	8.0
CBR 5.0mm (%)	10.0
Preparation	Soaked
Initial Moisture Content (%)	11.8
Achieved Dry Density (t/m^3)	1.956
Achieved Moisture Content (%)	11.8
Swell (%)	0.0
Moisture After Penetration (%)	11.8
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	13.1
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	105
Laboratory Density Ratio After Compaction (%)	99
Oversize Material Excluded	YES
Percent Oversize Excluded	7.9



CBR (%): 10.0

Rate of Penetration

Comments

Depth of sample = 0.25 - 1.0m

California Bearing Ratio

Report No: CBR:LCOV08S-01181

Issue No: 1

This report replaces all previous issues of report no. CBR:LCOV08S-01181.

Client: Coffey Geotechnics Pty Ltd
8/12 Mars Road
Lane Cove NSW 2066

Principal:
Job No: LABTLCOV00268AA
Project: GEOTLCOV23462AA
Lot No: TRN:



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Approved Signature: Marshall Webster
(Laboratory Manager)
NATA Accredited Laboratory Number: 431
Date of Issue: 22/04/2008

Sample Details

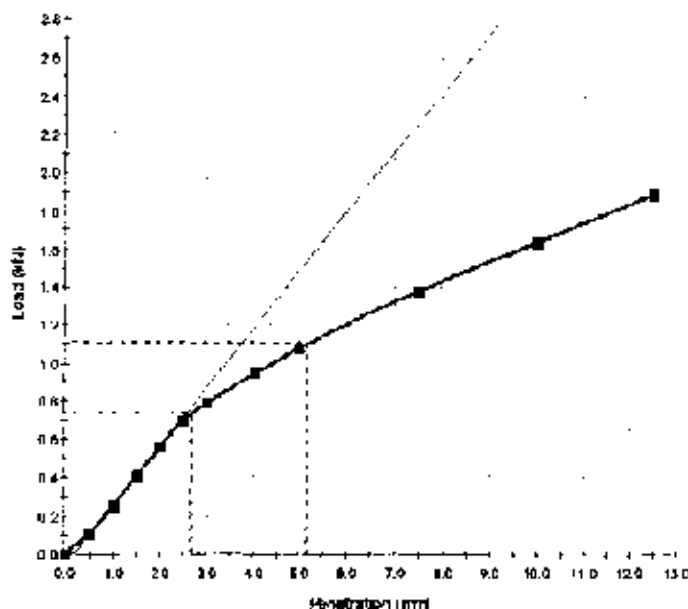
Product:
Source:
Location: SAN Hospital, Wahronga
Client Ref: CBH 11

Date Sampled: 1/04/2008
Sampling Method:
Sample ID: LCOV08S-01181

Test Results

Description	Result
Test Method	AS 1289 6.1.1
Maximum Dry Density (t/m^3)	1.890
Optimum Moisture Content (%)	12.8
CBR 2.5mm (%)	6.0
CBR 5.0mm (%)	6.0
Preparation	Soaked
Initial Moisture Content (%)	12.9
Achieved Dry Density (t/m^3)	1.882
Achieved Moisture Content (%)	12.9
Swell (%)	3.0
Moisture After Penetration (%)	13.8
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	16.0
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	101
Laboratory Density Ratio After Compaction (%)	100
Oversize Material Excluded	YES
Percent Oversize Excluded	0.0

Chart



CBR (%): 6.0

Rate of Penetration

Comments

Depth of sample = 0.25 - 1.0m

California Bearing Ratio

Report No: CBR:LCOV08S-01182

Issue No: 1

This report replaces all previous issues of report no 'CBR:LCOV08S-01182'.

Client: Coffey Geotechnics Pty Ltd
 8/12 Mars Road
 Lane Cove NSW 2066

Principal:

Job No: LABTLCOV00268AA

Project: GEOTLCOV23462AA

Lot No: TRN:



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Approved Signatory: Marshall Webster
 (Laboratory Manager)
 NATA Accredited Laboratory Number: 431
 Date of Issue: 22/04/2008

Sample Details

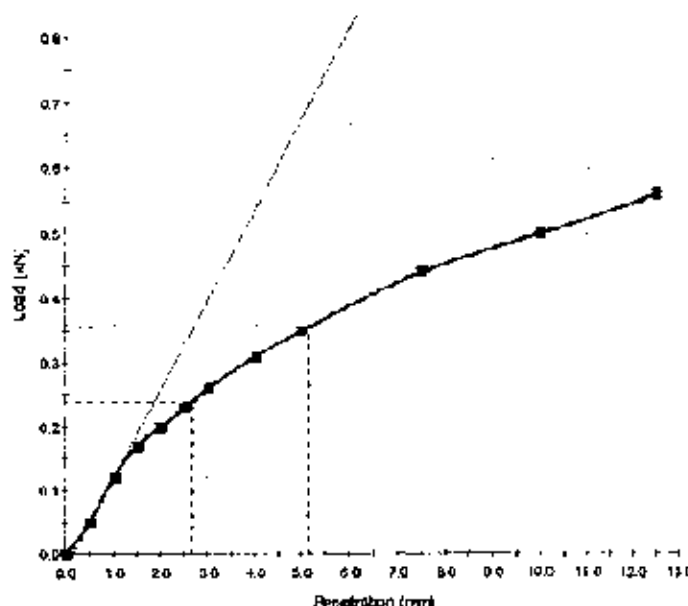
Product:
Source:
Location: SAN Hospital, Wahroonga
Client Ref: CBH 14

Date Sampled: 7/04/2008
Sampling Method:
Sample ID: LCOV08S-01182

Test Results

Description	Result
Test Method	AS 1289.6.1.1
Maximum Dry Density (t/m^3)	1.690
Optimum Moisture Content (%)	20.0
CBR 2.5mm (%)	2.0
CBR 5.0mm (%)	2.0
Preparation	Soaked
Initial Moisture Content (%)	22.3
Achieved Dry Density (t/m^3)	1.656
Achieved Moisture Content (%)	22.3
Swoll (%)	0.0
Moisture After Penetration (%)	22.3
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	23.2
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	117
Laboratory Density Ratio After Compaction (%)	98
Oversize Material Excluded	YES
Percent Oversize Excluded	

Chart



CBR (%): 2.0

Rate of Penetration

Comments

Depth of sample = 0.25 - 1.0m

California Bearing Ratio

Report No: CBR:LCOV08S-01183

Issue No: 1

This report replaces all previous issues of report no CBR:LCOV08S-01183.

Client: Coffey Geotechnics Pty Ltd
8/12 Mars Road
Lane Cove NSW 2066

Principal:
Job No: LABTI COV00268AA
Project: GEOTLCOV23462AA
Lot No:

TRN:



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Approved Signatory: Marshall Webster
(Laboratory Manager)
NATA Accredited Laboratory Number: 431
Date of issue: 22/04/2008

Sample Details

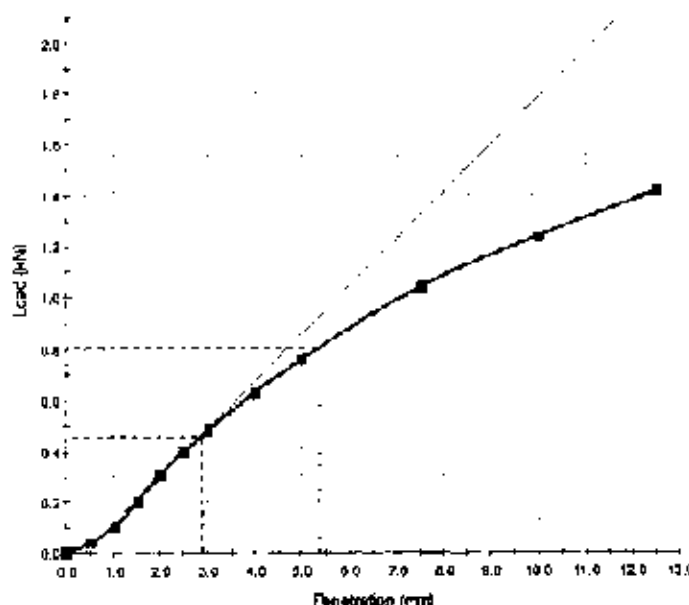
Product:
Source:
Location: SAN Hospital, Wahroonga
Client Ref: CBH 10

Date Sampled: 7/04/2008
Sampling Method:
Sample ID: LCOV08S-01183

Test Results

Description	Result
Test Method	AS 1289.6.1.1
Maximum Dry Density (t/m^3)	1.900
Optimum Moisture Content (%)	11.4
CBR 2.5mm (%)	3.6
CBR 5.0mm (%)	4.0
Preparation	Soaked
Initial Moisture Content (%)	15.2
Achieved Dry Density (t/m^3)	1.846
Achieved Moisture Content (%)	15.2
Swell (%)	0.0
Moisture After Penetration (%)	15.7
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	16.2
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	133
Laboratory Density Ratio After Compaction (%)	97
Oversize Material Excluded	YES
Percent Oversize Excluded	3.6

Chart



CBR (%): 4.0

Rate of Penetration

Comments

Depth of sample = 0.3 - 0.6m

California Bearing Ratio

Report No: CBR:LCOV08S-01184

Issue No: 1

This report replaces all previous issues of report no 'CBR:LCOV08S-01104'.

Client: Coffey Geotechnics Pty Ltd
8/12 Mars Road
Lane Cove NSW 2066

Principal:

Job No: LABTLCOV00268AA

Project: GEOTLCOV23462AA

Lot No:

TRN:



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Approved Signatory: Marshall Webster
(Laboratory Manager)
NATA Accredited Laboratory Number 491
Date of Issue: 22/01/2008

Sample Details

Product:

Date Sampled: 7/04/2008

Source:

Sampling Method:

Location: SAN Hospital, Wahroonga

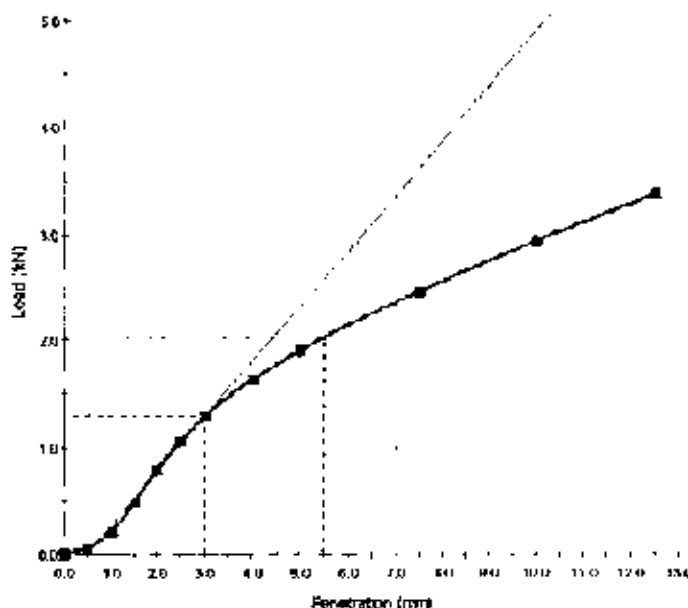
Sample ID: 1 COV08S-01184

Client Ref: CBH 7

Test Results

Description	Result
Test Method	AS 1289.6.1.1
Maximum Dry Density (t/m^3)	1.930
Optimum Moisture Content (%)	11.9
CBR 2.5mm (%)	10.0
CBR 5.0mm (%)	10.0
Preparation	Soaked
Initial Moisture Content (%)	11.5
Achieved Dry Density (t/m^3)	1.935
Achieved Moisture Content (%)	11.5
Swell (%)	0.0
Moisture After Penetration (%)	11.9
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	14.1
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	97
Laboratory Density Ratio After Compaction (%)	100
Oversize Material Excluded	YES
Percent Oversize Excluded	0.0

Chart



CBR (%): 10.0

Rate of Penetration

Comments

Depth of sample = 0.25 - 1.0m

California Bearing Ratio

Report No: CBR:LCOV08S-01185

Issue No: 1

This report replaces all previous issues of report no CBR:LCOV08S-01185.

Client: Coffey Geotechnics Pty Ltd
8/12 Mars Road
Lane Cove NSW 2066

Principal:

Job No: LABTLCOV00268AA

Project: GEOTLCOV23162AA

Lot No:

TRN:



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Approved Signatory: Marshall Webster
(Laboratory Manager)
NATA Accredited Laboratory Number: 431
Date of Issue: 22/04/2008

Sample Details

Product:

Date Sampled: 7/04/2008

Source:

Sampling Method:

Location: SAN Hospital, Wahroonga

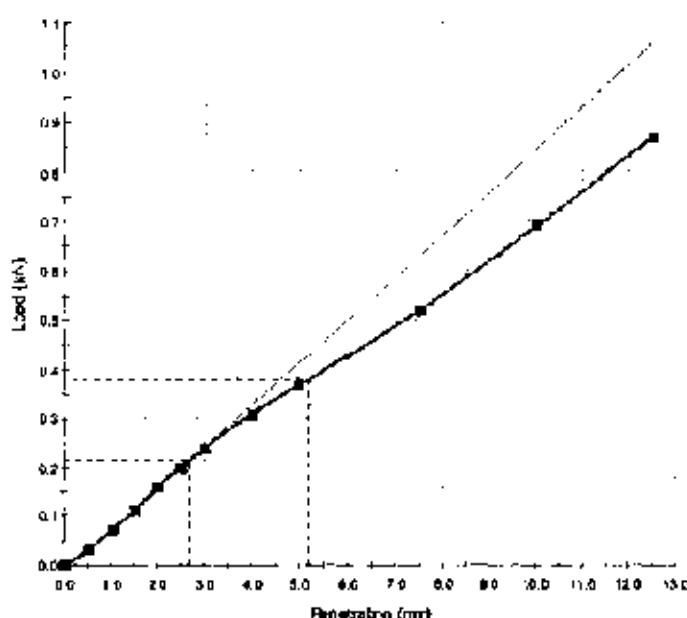
Sample ID: LCOV08S-01185

Client Ref: CBH 18

Test Results

Description	Result
Test Method	AS 1289.6.1.1
Maximum Dry Density (t/m^3)	1.810
Optimum Moisture Content (%)	15.8
CBR 2.5mm (%)	1.5
CBR 5.0mm (%)	2.0
Preparation	Soaked
Initial Moisture Content (%)	16.7
Achieved Dry Density (t/m^3)	1.794
Achieved Moisture Content (%)	16.7
Swell (%)	0.0
Moisture After Penetration (%)	16.7
Period of Soaking (days)	4
Moisture Content of Top 30mm (%)	19.6
Moisture of Penetrated End (%)	
Compaction Type	
Surcharge Mass (kg)	4.50
Laboratory Moisture Ratio After Compaction (%)	106
Laboratory Density Ratio After Compaction (%)	99
Oversize Material Excluded	YES
Percent Oversize Excluded	0.0

Chart



CBR (%): 2.0

Rate of Penetration

Comments

Depth of sample = 0.2 - 1.0m

2 April 2008

TEST REPORT

Coffey Environments Pty Ltd
8/12 Mars Road
LANE COVE WEST
NSW 2066

Your Reference: GL23462AA
Report Number: 59760

Attention: Richard Moyle

Dear Richard

The following samples were received from you on the date indicated.

Samples:	Qty.	7 Soils
Date of Receipt of Samples:		26/03/08
Date of Receipt of Instructions:		26/03/08
Date Preliminary Report Emailed:		Not Issued

These samples were analysed in accordance with your written instructions.
A copy of the instructions is attached with the analytical report.

The results and associated quality control are contained in the following pages of this report.
Unless otherwise stated, solid samples are expressed on a dry weight basis (moisture has been supplied for your information only), air and liquid samples as received.

Should you have any queries regarding this report please contact the undersigned.

Yours faithfully
SGS ENVIRONMENTAL SERVICES


Ly Kim Ha
Senior Organic Chemist


Edward Ibrahim
Laboratory Services Manager



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Page 1 of 7

Inorganics						
Our Reference:	UNITS	59760-1	59760-2	59760-3	59760-4	59760-6
Your Reference:	-----	CBH16	CBH13	CBH15	CBH12	CBH8
Sample Type:	-----	Soil	Soil	Soil	Soil	Soil
Depth:		0.3-0.5	0.7-1.0	0.25-1.0	0.2-0.3	0.3-0.4
Date Sampled:		19/03/2008	18/03/2008	18/03/2008	17/03/2008	13/03/2008
Date Extracted (pH)		27/03/2008	27/03/2008	27/03/2008	27/03/2008	27/03/2008
Date Analysed (pH)		27/03/2008	27/03/2008	27/03/2008	27/03/2008	27/03/2008
pH 1:5 soil:water 1:5 soil:water	pH Units	7.7	4.7	8.1	5.5	7.6

Inorganics		
Our Reference:	UNITS	59760-7
Your Reference:	-----	CBH1
Sample Type:	-----	Soil
Depth:		0.1-0.6
Date Sampled:		10/03/2008
Date Extracted (pH)		27/03/2008
Date Analysed (pH)		27/03/2008
pH 1:5 soil:water 1:5 soil:water	pH Units	8.0



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Anions in soil						
Our Reference:	UNITS	59760-1	59760-2	59760-3	59760-4	59760-5
Your Reference:	-----	CBH16	CBH13	CBH15	CBH12	CBH8
Sample Type:	-----	Soil	Soil	Soil	Soil	Soil
Depth:		0.3-0.5	0.7-1.0	0.25-1.0	0.2-0.3	0.3-0.4
Date Sampled:		19/03/2008	18/03/2008	18/03/2008	17/03/2008	13/03/2008
Date Extracted:		31/03/08	31/03/2008	31/03/2008	31/03/2008	31/03/2008
Date Analysed:		02/04/08	31/03/2008	31/03/2008	31/03/2008	31/03/2008
Chloride, Cl 1:5 soil:water	mg/kg	6.2	290	6.7	17	2.0
Sulphate, SO4 1:5 soil:water	mg/kg	33	46	33	78	39

Anions in soil		
Our Reference:	UNITS	59760-7
Your Reference:	-----	CBH1
Sample Type:	-----	Soil
Depth:		0.7-1.0
Date Sampled:		10/03/2008
Date Extracted:		31/03/2008
Date Analysed:		31/03/2008
Chloride, Cl 1:5 soil:water	mg/kg	6.4
Sulphate, SO4 1:5 soil:water	mg/kg	38

Moisture						
Our Reference:	UNITS	59760-1	59760-2	59760-3	59760-4	59760-6
Your Reference	-----	CBH16	CBH13	CBH15	CBH12	CBH8
Sample Type	-----	Soil	Soil	Soil	Soil	Soil
Depth		0.3-0.5	0.7-1.0	0.25-1.0	0.2-0.3	0.3-0.4
Date Sampled		19/03/2008	18/03/2008	18/03/2008	17/03/2008	13/03/2008
Date Analysed (moisture)		27/03/2008	27/03/2008	27/03/2008	27/03/2008	27/03/2008
Moisture	%	10	10	10	11	7

Moisture		
Our Reference:	UNITS	59760-7
Your Reference	-----	CBH1
Sample Type	-----	Soil
Depth		0.1-0.8
Date Sampled		10/03/2008
Date Analysed (moisture)		27/03/2008
Moisture	%	17

Method ID	Methodology Summary
AN101	pH - Measured using pH meter and electrode in accordance with APHA 20th ED, 4500-H+.
SEI-038	Anions - a range of Anions are determined by Ion Chromatography, in accordance with APHA 20th ED, 4110-B.
AN002	Preparation of soils, sediments and sludges undergo analysis by either air drying, compositing, subsampling and 1:5 soil water extraction where required. Moisture content is determined by drying the sample at 105 ± 5°C.

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QUALITY CONTROL	UNITS	LOR	METHOD	Blank	Duplicate Sm#	Duplicate		
Inorganics						Base + Duplicate + %RPD		
Date Extracted (pH)				(NT)	59760-1	27/03/2008 27/03/2008		
Date Analysed (pH)				(NT)	59760-1	27/03/2008 27/03/2008		
pH 1:5 soil:water	pH Units	0	AN101	(NT)	59760-1	7.7 7.7 RPD: 0		
QUALITY CONTROL	UNITS	LOR	METHOD	Blank	Duplicate Sm#	Duplicate	Spike Sm#	Matrix Spike % Recovery
Anions in soil						Base + Duplicate + %RPD		Duplicate + %RPD
Date Extracted				31/03/08	59760-1	31.03.08 31.03.08	LCS	31/03/08%
Date Analysed				31/03/08	59760-1	02.04.08 02.04.08	LCS	31/03/08%
Chloride, Cl 1:5 soil:water	mg/kg	0.5	SEI-038	<0.5	59760-1	6.2 6.0 RPD: 3	LCS	103%
Sulphate, SO4 1:5 soil:water	mg/kg	2	SEI-038	<2	59760-1	33 28 RPD: 16	LCS	101%
QUALITY CONTROL	UNITS	LOR	METHOD	Blank				
Hold sample NO test required								
Sample on HOLD				(NT)				
QUALITY CONTROL	UNITS	LOR	METHOD	Blank				
Moisture								
Date Analysed (moisture)				(NT)				
Moisture	%	1	AN002	(NT)				



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Result Codes

[INS]	: Insufficient Sample for this test	(RPD)	: Relative Percentage Difference
[NR]	: Not Requested		: Not part of NATA Accreditation
[NT]	: Not tested	(N/A)	: Not Applicable

Report Comments

Date Organics extraction commenced: N/A

NATA Corporate Accreditation No. 2562, Site No 4354

Note: Test results are not corrected for recovery (excluding Dioxins/Furans* and PAH in XAO and PLF).

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Quality Control Protocol

Method Blank: An analyte free matrix to which all reagents are added in the same volume or proportions as used in sample processing. The method blank should be carried through the complete sample preparation and analytical procedure. A method blank is prepared every 20 samples.

Duplicate: A separate portion of a sample being analysed that is treated the same as the other samples in the batch. One duplicate is processed at least every 10 samples.

Surrogate Spike: An organic compound which is similar to the target analyte(s) in chemical composition and behavior in the analytical process, but which is not normally found in environmental samples. Surrogates are added to samples before extraction to monitor extraction efficiency and percent recovery in each sample.

Internal Standard: Added to all samples requiring analysis for organics (where relevant) or metals by ICP after the extraction/digestion process; the compounds/elements serve to give a standard of retention time and/or response, which is invariant from run-to-run with the instruments.

Laboratory Control Sample: A known matrix spiked with compound(s) representative of the target analytes. It is used to document laboratory performance. When the results of the matrix spike analysis indicates a potential problem due to the sample matrix itself, the LCS results are used to verify that the laboratory can perform the analysis in a clean matrix.

Matrix Spike: An aliquot of sample spiked with a known concentration of target analyte(s). The spiking occurs prior to sample preparation and analysis. A matrix spike is used to document the bias of a method in a given sample matrix.

Quality Acceptance Criteria

Unless otherwise specified in the test method, the following general acceptance criteria apply:

Method Blanks:	<LOR
Duplicates:	<5 x LOR: No RPD criteria applied. >5 x LOR: 0-30% RPD is accepted.
LCS's:	Determined by Control Charts. Where control charts have not been developed, the Matrix Spikes criteria apply.
Matrix Spikes:	70-130% recovery is accepted for metals / inorganics. 60-140% is accepted for organics
Surrogates:	60-130% recovery is accepted for BTEX. 70-130% recovery is accepted for other organics.