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Winten Property Group/ Australand JV Macquarie Park Commerce Centre

Stormwater Management & Water Recycling

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Report No	

Date 14 September 2010

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1 Introduction

1.1 Background

The Winten Property Group and Australand Holdings Limited joint venture proposes a 4 building commercial development at the south-western corner of Waterloo Road and Lane Cove Road, Macquarie Park.

The proposed development has been declared by the NSW Department of Planning as a project to which Part 3A of the *Environmental Planning & Assessment Act 1979* applies. Hyder Consulting Pty has been commissioned to address the Director General's Requirements (DGRs) in relation to stormwater, Water Sensitive Urban Design (WSUD), on-site detention (OSD) and water conservation/recycling. This report has been specifically prepared to identify issues and undertake assessment in relation to:

- Ryde Council's DCP 2010 regarding drainage and flooding issues associated with the development site including stormwater, drainage infrastructure, OSD and WSUD elements.
- Sydney Water's request that the proposal be connected to the recycled water scheme currently being planned for the Macquarie Park area.

1.2 Project description

Macquarie Park Commerce Centre is a new commercial and retail development located in Macquarie Park, bounded by Lane Cove Road, Waterloo Road, Coolinga Street and Giffnock Avenue. The site has an area of approximately 1.56 ha and is currently occupied by two 2storey light industrial buildings and the western entrance portal to the Macquarie Park railway station. The eastern boundary of the site partially fronts Lane Cove Road with the remainder abutting a new development occupied by Hyundai. A figure showing the development site in the context of the upstream catchment is presented in Appendix A. This shows that the site drains to two outlets at different catchments, one to Lane Cove Road and the other to Coolinga Street.

The proposed development consists of one 17-storey building and three 8-storey buildings with common basement carparks. The proposal involves significant landscaped and open space areas that include streetscapes, central courtyard to the rear of the site and courtyard links between the buildings. The buildings will be designed to provide A-Grade commercial floor space and will seek to achieve a minimum 4.5 star Green Star rating.

2 Water Sensitive Urban Design

2.1 Stormwater quality objectives & treatment targets

The City of Ryde DCP 2010 states the following management objectives in relation to stormwater quality:

- Improve water quality within the City of Ryde and to the receiving waters (Lane Cove River & Parramatta River).
- Integrate stormwater treatment with stormwater quality management where possible.
- Encourage consideration of Ecologically Sustainable Development and Catchment management while providing requirements for water management when developing a site.

Water Sensitive Urban Design (WSUD) measures are to be incorporated into the urban design of the proposed development so as to achieve the following:

- 90% reduction in the post development average annual gross pollutant load;
- 85% reduction in the post development average annual load of Total Suspended Solids load;
- 60% reduction in the post development average annual load of Total Phosphorus load;
- 45% reduction in the post development average annual load of Total Nitrogen load;

2.2 Proposed stormwater quality measures

A number of stormwater quality measures are proposed to be implemented as part of the proposed development to ensure that the set treatment targets are met. These include the following.

2.2.1 Rainwater tanks

Rainwater tanks are proposed to satisfy sustainability building requirements for the project and the water conservation principles included in the planning for the Macquarie Park Corridor. Rainwater tanks will be used to collect roof water from the site's roofs to be used for non-potable water demands for toilet flushing, cooling tower, car washing and for outdoor irrigation use. All rainwater tanks are assumed to have a first-flush device to capture gross pollutants and sediments accumulating on the roof when storms happen. Rainwater tanks also provide stormwater treatment through settling and harvesting in addition to their main purpose of providing alternative source of water for non-potable water uses.

Estimation of non-potable water demand

The Water Efficiency Guide: Office and Public Buildings (Department of Environment and Heritage 2006) provides an estimation guideline for the median water consumption in office buildings based on the net lettable floor area for the building. Based on this guideline, the median water consumption for the proposed project can be estimated as follows:

Net lettable area for the proposed development = $75,582 \text{ m}^2$

The median water consumption for office buildings in Sydney = 1.13 kL/m²/year

The irrigation water consumption in office buildings is estimated to be 1% of the total demand, thus the median water consumption for the project without irrigation = $1.11 \text{ kL/m}^2/\text{year}$

Based on the above, the estimated total water consumption for the proposed development without irrigation = $1.11 \text{ kL/m}^2/\text{year x } 75,582 \text{ m}^2 = 83,896 \text{ kL/year}$

The typical office building water consumption is shown in Table 1 below.

Table 1: Typical office Building Water Consumption (leakage factor is neutralised)

Water use	% of total
Amenities	50%
Cooling Tower	42%
Other (including retail)	6%
Irrigation	1%

Based on the above, we can assume that the non-potable water demand, which can supply the entire cooling tower demand and 50% of the amenities demand equals to 67% of the total estimated water consumption for the proposed office building project. The irrigation demand can be estimated as an average of 300 mm per year for the estimated 2500 m² landscaped area.

Thus the total non-potable water demand for the proposed project can be estimated:

 $67\% \times 83,896 \text{ kL/year} + 300/1000 \times 2500 \text{ m}^2 = 56,960 \text{ kL/year}$

2.2.2 Bio-retention systems (rain gardens)

Rain gardens are bio-retention systems that comprise a combination of vegetation and filter substrate, which provide treatment of stormwater through filtration, extended detention and some biological uptake. Rain gardens are proposed to treat runoff from the majority of the site excluding a small area as shown in the Stormwater Plan presented in Appendix B. When stormwater flow exceeds the filtration capacity of rain gardens 3, 4 & 6, a high level overflow system is provided to bypass excess runoff to the OSD system. The proposed rain garden areas for the various catchments of the site are presented in Table 2. Typical detail is presented in Appendix B.

Catchment	Rain garden area
1	25 m ²
3	30 m ²
4	30 m ²
6	300 m ²
8	10 m ²
11	10 m ²

Table 2: Proposed Stormwater Quality Treatment Measures for the Site (Refer to Stormwater Plan in Appendix B).

2.3 Methodology for assessment

Assessment of the performance of the proposed stormwater quality measures has been undertaken using the Model for Urban Stormwater Improvement Conceptualisation (MUSIC V4.0). A MUSIC model for the proposed development has been developed assuming that the site has commercial land use with imperviousness shown in Table 3. The MUSIC model layout and key modelling parameters are presented in Appendix C.

Catchment	Surface type	Area (m²)	Imperviousness
1	Ground level	787	92%
2	Roof	2179	100%
3	Ground level	1214	78%
4	Ground level	1099	66%
5	Roof	2192	100%
6	Ground level	2374	25%
7	Ground level	450	100%
8	Ground level	467	57%
9	Roof	2220	100%
10	Roof	2190	100%
11	Ground level	452	98%

Table 3: MUSIC Model Catchment Details

2.4 Results

Based on the proposed stormwater quality measures the treatment performance for the whole site is presented in Table 4. Treatment performance for each catchment is presented in Appendix C.

Table 4: Treatment Performance Summary for the Site

Catchment	Pollutant reduction				
	Gross pollutants	TSS	ТР	TN	
	(%)	(%)	(%)	(%)	
Total site	97	86	83	78	
Treatment targets	90	85	60	45	

3 Flooding & On-site Stormwater Detention

3.1 Flooding

Flood level information affecting the site was provided by the City of Ryde and is presented in Appendix D. This information provides flood levels for the 20 year and 100 year ARI flood events as well as the Probable Maximum Flood (PMF) event.

This information was considered in determining the finished floor levels for the proposed development buildings. The finished floor levels for the site buildings, which are presented in Appendix B, are all set at least 300 mm above the predicted design flood level (100 year ARI) to ensure that they are not subject to stormwater inundation. This is in line with the requirements of the City of Ryde DCP 2010.

3.2 On-site detention

On-site detention (OSD) of stormwater involves storing stormwater on the site then slowly releasing it to counteract the effects of urban development within a catchment by reducing the peak discharge during storms to a specified level.

3.2.1 Design standard

The design criteria for the OSD system is to provide sufficient storage to ensure peak flow rates at any point within the downstream drainage system do not increase as a result of the development during storms from the 5-year to the 100-year ARI storm events of all durations. The City of Ryde DCP 2010 notes that where the site contains existing buildings or hard surfaces which are to be removed or substantially modified for a proposed development (similar to the case of this development), the site will be considered vacant and site runoff determined for "state of nature" conditions.

3.2.2 Existing conditions

DRAINS software has been used to develop a rainfall runoff model to assess the performance of the existing site drainage.

The site is split into two existing catchments based on the catchment plan provided by the City of Ryde, which is presented in Appendix A of this report. Catchment A has an area of 0.507 ha and drains to Lane Cove Road, while Catchment B has an area of 1.054 ha and drains to Cooliga Street. A 100% pervious ground was assumed for the existing conditions to reflect the guidelines in the City of Ryde DCP 2010. No external catchments were assumed to enter the site as the Hyundai building in 394 Lane Cove Road drains to Lane Cove Road and Giffnock Avenue.

The calculated maximum peak flow from the site in pre-development (natural) conditions is 0.199 m^3 /s discharging to Lane Cove Road and 0.395 m^3 /s discharging to Coolinga Street.

3.2.3 Post development conditions

The DRAINS software has been used to develop a rainfall runoff model to assess the performance of the proposed site OSD stormwater system with respect to mitigating potential flow impacts on neighbouring downstream areas.

All roof catchments (Catchments 2, 5, 9 & 10), which drain initially to the rainwater tank, overflow to the OSD tank, which drains to the existing Council's pit at the low point in Coolinga Street. Additionally, Catchments 3, 4 and 6, which drain initially to rain garden systems, would discharge to the OSD tank via underdrains and overflow pipes. Catchments 1, 7, 8 & 11 would bypass the OSD system. The OSD outlet is set at a level higher than the 100 year level of the connection point with Council's drainage system to ensure that the controlled flow from the OSD system is free flowing. This is illustrated in the Stormwater Plan for the site presented in Appendix B.

Detention volume of 750 m³ was required to reduce peak flows from the site to pre-development (natural) levels. Details of the DRAINS model and results for pre and post development conditions are presented in Appendix E.

The City of Ryde DCP 2010 provides for rainwater tank offset for OSD systems. This can be estimated as equal to the internal reuse demand within the proposed project. As discussed in Section 2 earlier, the internal non-potable water demand for the project can be estimated as follows:

67% x 67,488 kL/year / 365 = 124 m³

Thus, the minimum OSD volume required to be provided is $750 - 124 = 626 \text{ m}^3$. It is recommended at this stage of the project to provide 700 m³ OSD volume to cater for any design changes and allowance for headroom and overflow from the OSD tank.

4 Water Conservation & Recycling

Water conservation measures are essential as part of the sustainability building requirements for the project and the water conservation principles included in the planning for the Macquarie Park Corridor. Additionally, Sydney Water requested in their letter of 6 April 2010 that the proposed development be connected to the recycled water scheme currently being planned for the Macquarie Park area.

In their letter of 6 April 2010, Sydney Water requested that an integrated water management plan be prepared for the proposed development that would include any proposed alternative water supply, proposed end uses of potable and non-potable water, demonstration of WSUD and any water conservation measures. They have indicated that they are near the completion of a feasibility study for the provision of a recycled water scheme for the Macquarie Park area and if the cost was affordable, that the next step would be seeking approval for allocation of funding for the scheme.

4.1 Estimation of non-potable water demand & wastewater discharges

As presented earlier in Section 2, the non-potable demands for the proposed development comprise the majority of the estimated water demand (about 68%) and is estimated to be 56,960 kL/year.

Typically, commercial buildings are assumed to have wastewater discharge factor of 0.9 (i.e 90% of their estimated water use would be discharged to the sewer). Thus, the estimated average wastewater discharge for the proposed development = $0.9 \times 56,960 = 51,264 \text{ kL/year}$.

4.2 Water conservation measures

4.2.1 Efficient water appliances

The proposed buildings on the site will have to achieve a minimum 4.5 star Green Star rating, and as such water efficient fixtures and water saving measures will have to be allowed for in the design of the buildings and implemented before being occupied.

4.2.2 Rainwater reuse

As discussed earlier in Section 2, a rainwater reuse strategy is proposed for the project, which involves collecting rainwater from the building roofs into a 700 m³ rainwater tank. This tank will be used to supply reuse water for all the non-potable demands such as toilet flushing, cooling tower, irrigation of the landscaped areas within the development and for car washing facilities.

The first flush (first 2 mm of rain) should be diverted away from the storage tank. Stored water should be filtered and disinfected before using it in the reticulated non-potable water supply system within the building. It is also recommended that a site-specific risk assessment be undertaken before finalising the detailed design for the rainwater reuse system according to The Australian Guidelines for Water Recycling: Managing Health and Environmental Risks: Stormwater Harvesting and Reuse (NRMMC 2009) and/or Managing Urban Stormwater: Harvesting and Reuse (DEC 2006).

Based on the water balance results for the proposed development using the MUSIC model, the proposed 700 m³ rainwater tank will be sufficient to reuse about 90% of the collected rainwater from the site's roofs, satisfying about 15% of the estimated non-potable water demand of the

proposed development. This rainwater reuse strategy also works as part of the broader WSUD strategy for the site, which aims to improve stormwater quality and reduce stormwater volume discharged from the site as discussed earlier in this report.

4.3 Recycled water supply scheme

Hyder have spoken to Sarah Cannon from Sydney Water regarding the Macquarie Park recycled water scheme and the following is noted:

- Over the last 18 months Sydney Water has been doing a feasibility study for a potential reticulated recycled water scheme in Macquarie Park area.
- This has included technical and feasibility analysis and stakeholder consultation with major land owners and other interested parties.
- A report is now being prepared with a refined business case for detailed assessment.
- The option considered is a localised sewer mining system with a reticulated recycled water supply.
- The main risk associated with the proposed recycled water scheme is uncertainty of connection of customers. Sydney Water is now looking into mandating the connection of future developers to this scheme.
- The scheme will be funded by developers in a similar way to the usual Sydney Water's developer's services charges that they levy from developers of Greenfield developments with an approximate estimate of \$6000/Equivalent Tenement (ET). The operational fees for the scheme will be covered by charging connection and usage fees for recycled water supply in a similar fashion to potable water supply.
- The expected recycled water uses would be for non-potable demands such as toilet flushing, cooling tower, irrigation and washdown.

Based on the above and the earlier analysis of the proposed water conservation measures for the proposed development, it can be concluded that the proposed water saving measures and rainwater reuse system can only meet a fraction (15-20%) of the estimated non-potable water demands for the development. These proposed measures are important for the proposed development to meet its WSUD objectives and its sustainability building requirements (a minimum 4.5 star Green Star rating) Thus, should Sydney Water progress their feasibility analysis of the proposed recycled water scheme for Macquarie Park further and start planning for this scheme, there is still an opportunity to supply the proposed development with recycled water from this scheme.

5 Conclusion

The following conclusion can be drawn from this assessment:

- i. A suite of WSUD measures are proposed to sustainably manage stormwater on the site and meet the treatment standard required by Ryde City Council. These include rainwater tank and rain garden systems.
- ii. The proposed OSD system would be capable of mitigating potential peak runoff flows from the site to no greater than pre-development (natural) levels as required by Ryde City Council DCP 2010.
- iii. Rainwater reuse system and water conservation measures will be utilised to meet the building sustainability requirements for the proposed development.
- iv. There is potential for recycled water supply for the site from a centralised Sydney Water recycled water scheme for the Macquarie Park area should this scheme goes ahead.

Appendix A

Development Site & Catchment Map



City of Ryde

4

TREATTY RO

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15 Million

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FOLKARD ST

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ile Name:			
Date:	06/07/2010		
Scale:	1:3000		

BA

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Appendix B

Site's Stormwater Plan & Typical Section





Appendix C

MUSIC Model Parameters and Results

Rainfall

6 minute interval pluviograph data were used from the nearest BoM stations to the site. Pluviograph record from Wahroonga Reservoir (Station no. 66063) from 1st January 1963 through until 31 December 1972 was selected for the MUSIC modelling because this period had an average annual rainfall of 1034mm, which is closest to the average annual rainfall for the Wahroonga Estate.

Input parameters

The following input parameters for commercial developments were used (Music Modelling Guidelines for South East Queensland- Draft Dec 2009):

	Storm Flow					Base Flow						
	Tot Suspe Soli	tal ended ids	To Phosp	tal horus	Total Ni	trogen	Tot Suspe Soli	tal ended ids	Tot Phosp	tal horus	Tota Nitrog	al gen
Land Use	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD	Mean	SD
(all values expressed as log10mg/l												
Ground level	2.16	0.38	-0.39	0.34	0.37	0.34	0.78	0.39	-0.60	0.50	0.32	0.30
Roofs	1.30	0.38	-0.89	0.34	0.37	0.34	N/A	N/A	N/A	N/A	N/A	N/A

Note: SD = Standard Deviation

	Units	Ground level/ Roof
Rainfall Threshold	mm/day	1.0
Soil Storage Capacity	mm	200
Initial Storage	% of capacity	30
Field Capacity	mm	170
Infiltration Capacity Coefficient - a		200
Infiltration Capacity Coefficient – b		1.0
Initial Depth	mm	10
Daily Recharge Rate	%	25
Daily Baseflow Rate	%	5.0
Daily Deep Seepage Rate		0.0

MUSIC model layout



Results

	Pre-treatment load (kg/year)	Post-treatment load (kg/year)	% reduction
Catchment 1			
Flow (ML/yr)	0.70	0.65	7.40
Total Suspended Solids (kg/yr)	148.00	8.67	94.10
Total Phosphorus (kg/yr)	0.37	0.06	84.20
Total Nitrogen (kg/yr)	2.23	0.91	59.20
Gross Pollutants (kg/yr)	17.50	0.00	100.00
Catchment 3			
Flow (ML/yr)	0.95	0.89	6.70
Total Suspended Solids (kg/yr)	212.00	13.40	93.70
Total Phosphorus (kg/yr)	0.52	0.08	84.50
Total Nitrogen (kg/yr)	3.16	1.26	60.20
Gross Pollutants (kg/yr)	24.90	0.00	100.00
Catchment 4			
Flow (ML/yr)	0.69	0.63	9.10
Total Suspended Solids (kg/yr)	142.00	5.90	95.80
Total Phosphorus (kg/yr)	0.38	0.05	87.30
Total Nitrogen (kg/yr)	2.25	0.83	63.20

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Gross Pollutants (kg/yr)	19.00	0.00	100.00
Flow (ML/yr)	0.07	0.996	90.4
Total Suspended Solids (kg/yr)	0.37	0.000	00.0
Total Phosphorus (kg/yr)	254.00	25.4	90.0
Total Nitrogen (kg/yr)	1.38	0.136	90.2
Gross Pollutants (kg/yr)	25.10	2.68	89.3
	202.00	0.00	100.00
Catchment 6			
Flow (ML/yr)	0.86	0.45	47.20
Total Suspended Solids (kg/yr)	146.00	1.38	99.10
Total Phosphorus (kg/yr)	0.47	0.03	94.50
Total Nitrogen (kg/yr)	2.48	0.52	78.90
Gross Pollutants (kg/yr)	24.90	0.00	100.00
Catchment 7			
Flow (ML/yr)	0.43	0.43	0.0
Total Suspended Solids (kg/yr)	87.90	87.90	0.0
Total Phosphorus (kg/yr)	0.23	0.23	0.0
Total Nitrogen (kg/yr)	1.34	1.34	0.0
Gross Pollutants (kg/yr)	10.30	10.30	0.0
Catchment 8			
Flow (ML/yr)	0.29	0.27	7 50
Total Suspended Solids (kg/yr)	57.80	3.38	94 20
Total Phosphorus (kg/yr)	0 17	0.02	85.70
Total Nitrogen (kg/yr)	0.92	0.36	61 10
Gross Pollutants (kg/yr)	8 20	0.00	100.00
	0.20	0.00	100.00
Catchment 11			
Flow (ML/yr)	0.42	0.40	4.80
Total Suspended Solids (kg/yr)	94.70	9.67	89.80
Total Phosphorus (kg/yr)	0.24	0.04	81.50
I otal Nitrogen (kg/yr)	1.35	0.63	53.50
Gross Pollutants (kg/yr)	10.20	0.00	100.00
WHOLE SITE			
Flow (ML/vr)	12 70	1 61	63.8
Total Suspended Solids (kg/vr)	1160.00	16/ 0	85.0
Total Phosphorus (kg/yr)	3 70	0 6/	82.7
Total Nitrogen (kg/vr)	30.10	2.0 1 8.51	78.3
Gross Pollutants (kg/yr)	317	10.3	96.7
	317	10.3	96. <i>1</i>

Appendix D

Flood Information for the Site from the City of Ryde

FILE Hyder Consulting HECEYED	f Ryde
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	Civic Centre
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	Locked Bag 2069
	North Ryde NSW 1670
	DX 8403 Ryde
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	www.ryde.nsw.gov.au
	TTY (02) 9952 8470
Fac	simile (02) 9952 8070
Tele	phone (02) 9952 8222

Mr Firas Naji L5, 141 Walker Street NORTH SYDNEY NSW 2060

22 July 2010

Our ref: D10/52576

Dear Mr. Naji,

RE: Request for Flood Information – No. 396 Lane Cove Road, Macquarie Park

Reference is made to your application dated 19 July 2010 seeking flood level information pertaining to the above-mentioned address.

Please find attached flood level data sheet providing flood levels for the 20 year and 100 year ARI (Average Recurrence Interval) flood events as well as the PMF (Probable Maximum Flood) event.

Please be advised that flood models only approximate flood behaviour. Care and expertise is required in the interpretation of these flood levels. In addition, this flood information does not take into account any local overland flow issues.

Any person or organisation who acts on the information provided does so at his / her / its own risk. To the extent permitted by law, the City of Ryde accepts no responsibility and excludes all liability whatsoever in respect of any use of or reliance upon this information.

Should you require any further information, please feel free to contact me on (02) 9952 8222.

Yours sincerely,

d. Gunn-

Guna Veerasingham Acting Manager – Stormwater and Park Assets

City of Ryde FLOOD INFORMATION REQUEST



Property Address: Issue Date: Flood Study Reference: Flood Model Reference: No. 396 Lane Cove Road, Macquarie Park 22 July 2010 Draft Macquarie Park Flood Study Report (Dec 2009) TUFLOW Model (July 2010)

Flood Level Location Map



Flood Level Data Table

Location	20 Year ARI Flood (m AHD)	100 Year ARI Flood (m AHD)	Probable Maximum Flood (m AHD)
A	61.5	61.6	61.6
В	Nil	Nil	Nil
С	Nil	Nil	60.5
D	Nil	58.5	58.6
E	56.8	56.8	57.0
F	Nil	56.1	56.3
G	55.8	55.8	56.2
Н	56.6	56.6	56.6
I	Nil	Nil	Nil

Notes:

- All levels are based on Australian Height Datum (AHD).
- This flood level information is for existing site conditions only.
- A site specific flood study / risk assessment may be required for any future development. Engage a suitably qualified engineer to assist you in this matter. Any study or assessment shall be in accordance with the NSW Government's Floodplain Development Manual 2005 and the City of Ryde Development Control Plan 2006.
- Site specific ground and building survey levels should be used to relate flood levels and to assess the impact of flooding.

Appendix E

Drains Model & Results

Existing Catchments

- Total Area of site is approximately 1.56ha
- The site was split into two existing catchments based on the catchment diagram from City of Ryde Council.
- Catchment A has an area of 0.507ha (Cnr of Waterloo Rd and Lane Cove Rd)
- Catchment B has an area of 1.054ha (Cnr of Cooling St and Waterloo Rd)
- There are currently two outlets draining the site, these connect to the street drainage.
- While the site currently has a building, the council requires new developments to design stormwater discharge to 'natural state' conditions. 100% pervious ground for 'natural state' conditions was assumed.
- 100 year ARI Peak flow from site 0.199 m³/s and 0.394 m³/s, a total of 0.593 m³/s
- No external catchments enter the site

Modelling existing conditions

- The time of concentration (t_c) is important in determining the peak discharge from each storm event.
- The tc for Catchment A included 20m of sheet flow and then a remaining 140m of channelised flow. The grade for this catchment was 3%. This resulted in a time of concentration (t_c) of 15min
- The tc for Catchment B include 20m of sheet flow and then a remaining 120m of channelised flow. The grade for this catchment was 1%. This resulted in a time of concentration (t_c) of 17min.

Post Development Conditions

- One OSD tank located in Catchment B with outflows connecting to existing street drainage. The OSD system has two-stage outlet.
 - 200mm Low-Flow
 - 150mm High-Flow
 - Weir height of 58m

Modelling post-development conditions

- DRAINS software used to model the site.
- The OSD had to be sufficient to ensure peak flow rates from the 5 year to the 100 year ARI storm events over all durations. (6min to 180min from council DCP)
- The IFD data was taken from the City of Ryde Council DCP for Stormwater Management.
- The volume of storage required was 750m³
- An ARI 100Yr tail water level of 55.80m AHD was used in the analysis.

OSD Required

- Detention volume of 750m³ is sufficient to reduce peak flows for the entire site.
- These volumes do not take into account headroom which may be required at the top of the tank.

DRAINS Model



DRAINS Model Name and File Path:	F:\AA003465\D-Calculations\Stormwater\OSD_Final.drn	
DRAINS Version:	2010.01 - 5 August 2010	
Modeller's Name:	Chris McClelland	DAIA
Description:	Macquistic Park Commerce Contro OSD DRAINS Model	

PIT / NODE DETAI	ILS		Version 9											
Name	Туре	Family	Size	Ponding	Pressure	Surface	Max Pond	Base	Blocking	х	у	Bolt-down	id	Part Full
				Volume	Change	Elev (m)	Depth (m)	Inflow	Factor			lid		Shock Loss
				(cu.m)	Coeff. Ku			(cu.m/s)						
1	Node							C)	200.316	220.13		69	
2	Node							C)	197.824	244.626	i	70	
3	Node							C)	171.668	280.333		71	
4	Node							C)	156.721	329.325		72	
5	Node							C)	147.587	298.186	; 	73	
6	Node							C)	104.407	296.94		74	
7	Node							C)	69.531	258.743		75	
8	Node							C)	82.402	316.454		76	
9	Node							C)	62.058	291.543		77	
10	Node							0)	101.085	340.535		78	
11	Node							C)	121.43	358.803		79	
ANS	Node							C)	247.232	285.349		80	
BNS	Node							0)	3.597	394.625		81	
N27	Node							0)	255.209	250.606		82	
N28	Node							0)	45.173	242.966	; 	83	
N29	Node							0)	75.275	385.514		84	
N36	Node					55		0)	66.636	344.913		119	
N46	Node							0)	27.816	376.749		75490	
N47	Node							0)	-13.414	379.632		75498	
DETENTION BASI				0.4.5				D'' E ''	D: - T				0	0
INAME	LIEV	volume	init vol. (cu.m)	Outlet Type	ĸ	Dia(mm)		Pit Family	Pit Type	X	y 000.07-	HED	Crest RL	Crest Length
USD	56.75	0	0	None						137.254	338.388	NO		
	58.75	750							<u> </u>					
		+							<u> </u>					
SUB-CATCHMENT		T-4-1	Devie d	0	0	Daviad	0	0	Devend	0	0	Deveed	0	0
Name	Pit or	lotal	Paved	Grass	Supp	Paved	Grass	Supp	Paved	Grass	Supp	Paved	Grass	Supp
	Node	Area	Area	Area	Area	lime	lime	lime	Length	Length	Length	Slope(%)	Slope	Slope
0.11		(ha)	%	%	%	(min)	(min)	(min)	(m)	(m)	(m)	%	%	%
Cat1	1	0.0787	91.6	8.4	0	5	6	0)					
Cat2	2	0.2179	100	0	0	3	0	0)					
Cat3	3	0.1214	/8.5	21.5	0	6	3	0)					
Cat4	4	0.1099	65.7	34.3	0	3	6	0	2					
Cat5	5	0.2192	100	0	0	3	0)					
Cato	6	0.2374	25.1	74.9	0	6	/	0)					
Cat/	/	0.045	100	0	0	6	0							
Cate	8	0.0467	56.8	43.3	0	6	/	C)					
Caty	9	0.222	100	0	0	3	0)					
Catil	10	0.219	100	0	0	3	0)					
	11	0.0452	97.8	2.2	0	4	5)					
A_NAT_STATE	ANS	0.507	0	100	0	0	15							
B_NAT_STATE	BN2	1.054	. 0	100	0	0	17	L C)					
											1			
	From	To	Langth			Clana	Turne	Die		Daugh	Dine le		Cha From	At Cha
Name	FIOM	10	Length	0/5 IL	D/S IL	Slope	Туре	Dia	1.D.	Rougn	Pipe is	No. Pipes	Chg From	ALCING
			(m)	(m)	(11)	(%)		(mm)	(mm)					
DE TAILO UI SERV	Cha	Rottom	Hoight of Sonvice	Cha	Bottom	Hoight of C	Cha	Bottom	Hoight of C	oto				
Pipe	Chg	Bollom Flass (m)		Cng	Bollom	Height of S		Bollom	Height of S	elc				
	(11)		(11)	(11)		(m)	(11)	Liev (m)	(m)	elu				
	<u>ا</u>													
	-0	То	Turne	Longth			Clana	Deee Widt	L R Slope	D.D. Slope	Monning	Dopth	Poofod	
INAILIE		10	туре	(m)	(m)	(m)		(m)	(1·2)	(1·2)	n	(m)	NUDIEU	
		+		(11)	(11)	(11)	(70)	(11)	(1.1)	(1.1)	11	(11)		
									1					
Nomo	Erom	То	Travol	Spill	Croct	Woir	Cross	Sofo Dorth	SofoDonth	Safa	Rod	D/S Aroc		id
INGINE		10	Time		Length		Section	Major Stor	Minor Stor		Slope	Contributio	a	iu
			(min)		Lengtii (m)	CUEII. C		(m)	(m)		(%)		y	
OF CAT1	4	N27	(11111)	(11)	(11)		Dummy used to model flow corese to			(sq.m/sec)	(/0)	/0		05
	1		0.1				Dummy used to model flow across r		0.05	0.6	1	0		04
	2		0.1				Dummy used to model flow across re	0.2	0.05	0.6		0		94
OF_CAI3	3		0.1	<u> </u>			Dummy used to model flow across fo	y 0.2	0.05	0.6	1	0		95
OF CATE	4		0.1				Dummy used to model flow across re	0.2	0.05	0.6	۱ ۸	0		90
OF_CATE	5		0.1				Dummy used to model flow across for	y 0.2	0.05	0.6	1	0		97
OF_CATO	6	1030	0.1				Dummy used to model flow across for	y 0.2	0.05	0.6	1	0		98
	1	N20	0.1				Dummy used to model flow across fo	y 0.2	0.05	0.6	1	0		36
	8		0.1				Dummy used to model flow across fo	y 0.2	0.05	0.6	1	0		8/
OF_CATE	9		0.1				Dummy used to model flow across fo	y 0.2	0.05	0.6	1	0		400
	10	N20	0.1				Dummy used to model flow across re	0.2	0.05	0.6		0		100
	11	N/29	0.1				Dummy used to model flow across fo	y 0.2	0.05	0.6	1	0		75407
OF26	N20	N/40	0.1				Dummy used to model flow across re	0.2	0.05	0.6	۱ ۸	0		10491
OSD TWO STAC	090	N26	0.1	EC 75			Dummy used to model flow across re	0.2	0.05	0.6	1	0		1 3469
OF29	N36	N46	0.1	50.75			Dummy used to model flow across re		0.05	0.0	4	0		75/02
	N46	N47	0.1				Dummy used to model flow across re	0.2	0.05	0.0	1	0		75/00
	11-10	1.1.1.1	0.1	1	1	1	Learning used to model now across to	ч U.2	. 0.05	0.0		. 0		10499

	DRAINS Mode	I Name and F	ile Path:	F:\AA003465\	D-Calculations\	Stormwater\O	SD_Final.drn						
	DRAINS Version:		2010.01 - 5 A	ugust 2010									
Barbonic June JP Alego Description Description <thdescription<< td=""><td>Modeller's Name: Description:</td><td></td><td>Chris McClella Macquarie Pa</td><td>and irk Commerce (</td><td>Centre OSD DR</td><td>AINS Model</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thdescription<<>	Modeller's Name: Description:		Chris McClella Macquarie Pa	and irk Commerce (Centre OSD DR	AINS Model							
SUM B match 2000 Database per two bracks 2011-00 Provide 1011-00 Provide 10	Description.												
Differential Description Description <thdescription< th=""> <thdescription< th=""></thdescription<></thdescription<>	DRAINS results prep	bared 30 Augu	st, 2010 from	Version 2010.0	9						D		тς
District Dis result Dis result Dis result Dis result District District <thdistrict< th=""> District District</thdistrict<>					Manalan O							LOUL	10
	PIT / NODE DETAIL	S Max HGI	Max Pond	Max Surface	Version 8 Max Pond	Min	Overflow	Constraint			5 `	YEAR	ARI
Norme Norme <t< td=""><td>Thumbo .</td><td>MaxTICE</td><td>HGL</td><td>Flow Arriving</td><td>Volume</td><td>Freeboard</td><td>(cu.m/s)</td><td>Conotraint</td><td></td><td></td><td>1</td><td></td><td></td></t<>	Thumbo .	MaxTICE	HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)	Conotraint			1		
SUBCECONDUCT IS 1925 Parted Parted Parted Parted				(cu.m/s)	(cu.m)	(m)							
Direct Direct <thdirec< th=""> <thdirec< th=""> Direc</thdirec<></thdirec<>													
No. No. <td>Name</td> <td>DETAILS Max</td> <td>Paved</td> <td>Grassed</td> <td>Paved</td> <td>Grassed</td> <td>Supp</td> <td>Due to Storm</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Name	DETAILS Max	Paved	Grassed	Paved	Grassed	Supp	Due to Storm					
No. No. <td>Name</td> <td>Flow Q</td> <td>Max Q</td> <td>Max Q</td> <td>Tc</td> <td>Tc</td> <td>Tc</td> <td>Due to otomi</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Name	Flow Q	Max Q	Max Q	Tc	Tc	Tc	Due to otomi					
One Origin (1) Contract of the second were of a function of the second were		(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)						
Solu Color Color <thc< td=""><td>Cat1</td><td>0.033</td><td>0.031</td><td>0.002</td><td>5</td><td>6</td><td>0</td><td>AR&R 5 year</td><td>, 25 minutes st</td><td>orm, average 7</td><td>'9.1 mm/h, Zoi '4.5 mm/h, Zoi</td><td>ne 1</td><td></td></thc<>	Cat1	0.033	0.031	0.002	5	6	0	AR&R 5 year	, 25 minutes st	orm, average 7	'9.1 mm/h, Zoi '4.5 mm/h, Zoi	ne 1	
Base Disk Disk <thdisk< th=""> Disk Disk <thd< td=""><td>Cat2 Cat3</td><td>0.094</td><td>0.094</td><td>0.009</td><td>6</td><td>3</td><td>0</td><td>AR&R 5 year</td><td>. 25 minutes sto</td><td>orm, average 15</td><td>9.1 mm/h. Zoi</td><td>ne 1</td><td></td></thd<></thdisk<>	Cat2 Cat3	0.094	0.094	0.009	6	3	0	AR&R 5 year	. 25 minutes sto	orm, average 15	9.1 mm/h. Zoi	ne 1	
Carbon Oute <	Cat4	0.044	0.031	0.013	3	6	0	AR&R 5 year	, 25 minutes st	orm, average 7	'9.1 mm/h, Zoi	ne 1	
Lat. Comp Comp< Comp Comp< Comp<<	Cat5	0.094	0.094	0	3	0	0	AR&R 5 year	, 5 minutes sto	rm, average 15	i4.5 mm/h, Zoi	ne 1	
Diff Control C	Cat6	0.082	0.024	0.058	6	7	0	AR&R 5 year	, 25 minutes st	orm, average 7	'9.1 mm/h, Zoi	ne 1	
See 1288 0.038 0.	Cat8	0.018	0.018	0.007	6	7	0	AR&R 5 year	25 minutes st	orm, average 7	9.1 mm/h, Zoi '9.1 mm/h, Zoi	ne 1	
Carbo Carbo <th< td=""><td>Cat9</td><td>0.095</td><td>0.095</td><td>0</td><td>3</td><td>0</td><td>0</td><td>AR&R 5 year</td><td>, 5 minutes sto</td><td>rm, average 15</td><td>64.5 mm/h, Zoi</td><td>ne 1</td><td></td></th<>	Cat9	0.095	0.095	0	3	0	0	AR&R 5 year	, 5 minutes sto	rm, average 15	64.5 mm/h, Zoi	ne 1	
Bit Wart O118 0278 0 4 S 0 0.00000000000000000000000000000000000	Cat10	0.094	0.094	0	3	0	0	AR&R 5 year	, 5 minutes sto	rm, average 15	i4.5 mm/h, Zoi	ne 1	
At All Storm O.02 O.02 <tho.02< th=""> O.02 O.02</tho.02<>	Cat11	0.019	0.019	0	4	5	0	AR&R 5 year	, 25 minutes st	orm, average 7	'9.1 mm/h, Zoi	ne 1	
Sector Description Description Description Description Description Define Values to Table of the Construction of the Const	B NAT STATE	0.113	0	0.113	0	15	0	AR&R 5 year	, 2 hours storm	, average 33 m	nm/h, Zone 1		
Control Control <t< td=""><td></td><td></td><td></td><td>5.22</td><td></td><td></td><td></td><td></td><td></td><td></td><td>,</td><td></td><td></td></t<>				5.22							,		
Dufferen Line of Lot different 1 Dat reportion 1.5 Data bite 1 Line 1 <thlin 1<="" th=""> <thlin 1<="" th=""> <thline 1<="" <="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thline></thlin></thlin>													
Name Name <th< td=""><td>Outflow Volumes for</td><td>Total Catchm</td><td>ent (1.29 impe</td><td>rvious + 1.83 p</td><td>ervious = 3.12 1</td><td>otal ha)</td><td> </td><td> </td><td></td><td></td><td></td><td></td><td></td></th<>	Outflow Volumes for	Total Catchm	ent (1.29 impe	rvious + 1.83 p	ervious = 3.12 1	otal ha)							
ABAR D year, D me	30000	rutar Kainfall cu.m	cu.m (Runoff	cu.m (Runoff)	CU.m (Runoff %	6)							
ARAR 9 vor. 10 m E11.9 Biol. 129.2 M0 71 40 71 80 89 00 Mol 200 40 72 80 71 71 71 71 80 72 80 71 70 71 70 71 70 70 70 70 70 70 70 70 70 70 70 70 70	AR&R 5 year, 5 min	402.14	200.43 (49.8%	153.52 (92.2%	46.91 (19.9%)	-,							
ABAB 5 yer, 15 m 726.5 (327) (66.79) 122.2 (66.79) 122.3 (52.71) (22.3 (52	AR&R 5 year, 10 mi	621.56	386.12 (62.1%	244.35 (95.0%	141.78 (38.9%)							
Stand Park Diff Disk Dev C (bit 1 M) (11 (bit 0 M) (0 0 (bit 0 M) (1 M)) Disk Dev C (bit 1 M) (11 (bit 0 M) (0 0 (bit 0 M)) Disk Dev C (bit 1 M) (11 (bit 0 M) (0 0 (bit 0 M))) Disk Dev C (bit 1 M) (11 (bit 0 M) (0 0 (bit 0 M))) Disk Dev C (bit 1 M) (11 (bit 0 M) (0 0 (bit 0 M))) Disk Dev C (bit 0 M) (11 (bit 0 M) (0 0 (bit 0 M))) Disk Dev C (bit 0 M) (11 (bit 0 M) (0 0 (bit 0 M))) Disk Dev C (bit 0 M) (11 (bit 0 M) (0 M) (0 M) (11 (bit 0 M) (0 M) (11 (bit 0 M) (0 M) (11 (bit 0 M) (1	AR&R 5 year, 15 min	785.54	524.70 (66.8%	312.22 (96.0%	212.48 (46.2%)							
Add E. Sow 20 ml 1122 (E. V.2.1 / C. D. HéSZ, V. V. 24 352, S.	AR&R 5 year, 20 mil	918.28 1029 12	034.72 (69.19 721 19 (70 10	307.17 (96.6% 413 17 (97.0%	∠07.56 (49.7% 308 02 (51 1%)							
ARSR 9 yet, 1 For 1 (36.3 (0) 31 / 17 / 4 (95.4 (0) 7 / 34 / 17 (2.8 / 36) I	AR&R 5 year, 30 mil	1127.55	792.31 (70.3%	453.79 (97.2%	338.52 (51.2%)							
AR8R 5 year, 1 how 1996 21 1113 30 172 1622 320.82 0(4) 480 81 30 30 1 Image 1 402 77 17 402 78 405 30 (10 10 10 10 10 10 10 10 10 10 10 10 10 1	AR&R 5 year, 45 mi	1363.36	973.17 (71.4%	551.40 (97.7%	421.77 (52.8%)							
ARMAK SPR Total Total SPR SPR Total SPR	AR&R 5 year, 1 hou	1549.21	1115.30 (72.0	628.32 (98.0%	486.98 (53.6%)							
AREAR 9 year, 3 hoo 2417.91 1748.22 (72.367) (80.77.80.77) Non- Non- <th< td=""><td>AR&R 5 year, 1.5 ho</td><td>1836.56</td><td>1326.02 (72.2</td><td>747.27 (98.3% 840 35 (98.5%</td><td>578.75 (53.8% 647 38 (53.6%</td><td>)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	AR&R 5 year, 1.5 ho	1836.56	1326.02 (72.2	747.27 (98.3% 840 35 (98.5%	578.75 (53.8% 647 38 (53.6%)							
PRE DETALS Name	AR&R 5 year, 2 hour	2417.51	1748.22 (72.3	987.75 (98.7%)	760.47 (53.7%)							
PIPE DETAILS Nume Num Nume Nume Nume<			、 、	, , , , , , , , , , , , , , , , , , ,	, , , , , , , , , , , , , , , , , , ,								
Name Mar U Mar US Mar US <td>PIPE DETAILS</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	PIPE DETAILS					_							
Control Onto Order Line Control Control <t< td=""><td>Name</td><td>Max Q</td><td>Max V</td><td>Max U/S</td><td>Max D/S</td><td>Due to Storm</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm							
CHANNELDETAILS Max Max Max Max <		(cu.m/s)	(11/5)	ngl (m)	HGL (III)								
Name Max (m) Mainage Max (m) Unit (m) Mainage Max (m) Max (m) <th< td=""><td>CHANNEL DETAILS</td><td>5</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	CHANNEL DETAILS	5											
County (Inv.) (Inv.) HEL Inv.	Name	Max Q	Max V	Chainage	Max	Due to Storm							
OVERFLOW ROUT Der Norme New O		(cu.m/s)	(m/s)	(m)	HGL (m)								
Name Nax O US Nax O D Sale O Nax D Nax Wetter Max V Due to Sum Image Image OF CAT1 0.033 0.036 0.022 0.01 7.63 0.38 AR8 5 yar, 25 minutes storm, werage 71 mm/h, Zone 1 OF_CAT2 0.044 0.046 0.256 0.026 0.01 8.83 0.04 AR85 yar, 25 minutes storm, werage 71 mm/h, Zone 1 OF_CAT4 0.044 0.044 0.026 0.033 0.02 10.61 0.4 AR85 yar, 25 minutes storm, werage 71 mm/h, Zone 1 OF_CAT6 0.068 0.068 0.026 0.033 0.02 10.61 0.4 AR85 yar, 25 minutes storm, werage 75 mm/h, Zone 1 OF_CAT6 0.068 0.068 0.026 0.033 0.02 10.61 0.31 AR85 yar, 25 minutes storm, werage 75 mm/h, Zone 1 OF_CAT7 0.017 0.026 0.038 0.02 10.61 0.31 AR85 yar, 25 minutes storm, werage 75 mm/h, Zone 1 OF_CAT8 0.017 0.026 0.039 0.021 10.31 AR88 yar, 25 minutes storm, werage 75 mm/h, Zone 1 OF_CAT8 0.009 0.027 <td>OVERELOW ROUT</td> <td>E DETAILS</td> <td></td>	OVERELOW ROUT	E DETAILS											
OF_CAT1 0.033 0.023 0.024 0.024 0.01 7.63 0.38 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT3 0.044 0.026 0.020 0.01 8.83 0.41 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT4 0.044 0.048 0.026 0.01 8.53 0.41 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT4 0.044 0.048 0.026 0.033 0.02 0.011 0.44 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT6 0.064 0.016 0.026 0.013 0.011 0.44 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT7 0.018 0.016 0.026 0.010 0.016 0.44 0.33 AR84 Syar, 25 minutes storm, average 73.1 mmh, Zone 1 OF_CAT1 0.006 0.026 0.026 0.02 0.021 0.024 AR84 Syar, 2 minutes storm, average 73.1 mmh, Zone 1 OF_CAT1 0.006 0.026 0.026 0.02 0.021 AR84 Syar, 3 munutes storm, average 73.1 mmh, Zone 1	Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm				
OF_CAT2 0.094 0.264 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.028 minutes storm, average 701 mm/L Zens OF_CAT3 0.044 0.044 0.256 0.026 0.01 8.83 0.04 RARR 5 year. 2 minutes storm, average 701 mm/L Zens OF_CAT3 0.042 0.062 0.026 0.033 0.02 10.51 0.48 RARR 5 year. 2 minutes storm, average 701 mm/L Zens OF_CAT3 0.017 0.026 0.026 0.018 0.01 6.14 0.31 RARR 5 year. 2 minutes storm, average 711 mm/L Zens 1 OF_CAT3 0.017 0.026 0.026 0.021 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.024 0.034 RARR 5 year. 5 minutes storm, average 714 mm/L Zens 1 0.025 0.024 0.02 0.024 0.024 0.024 0.024 0.024 0.034 RARR 5 year. 5 minutes storm, average	OF_CAT1	0.033	0.033	0.256	0.023	0.01	7.63	0.38	AR&R 5 year,	25 minutes sto	orm, average 7	79.1 mm/h, Zo	ne 1
UP_DA13 UD48 UD48 UD48 UD48 <	OF_CAT2	0.094	0.094	0.256	0.034	0.02	10.74	0.5	AR&R 5 year,	5 minutes stor	m, average 15	54.5 mm/h, Zo	ne 1
OP: CATE 0.094 0.296 0.033 0.02 1.019 0.46 AR85 Syster. Simulation.average 7.1 mm/h. Zone 1 OF: CATE 0.018 0.296 0.033 0.02 10.56 0.46 AR85 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATE 0.018 0.018 0.019 0.011 6.14 0.33 AR85 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATE 0.019 0.026 0.026 0.021 10.91 0.46 AR85 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATO 0.096 0.256 0.003 0.02 10.91 0.48 AR85 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATO 0.094 0.026 0.010 6.44 0.31 AR88 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATO 0.094 0.026 0.011 6.44 0.31 AR88 Syster. Simulations average 7.1 mm/h. Zone 1 OF: CATO 0.019 0.256 0.029 0.02 11.81 0.54 AR88 Syster. Simulations average 7.81 mm/h. Zone 1 OF: DEVISITIONE AND PARE 0.134 0.256 0.039 0.02 11.81 0.54 AR88 Syster. Simulations average 7.81 mm/h. Zone 1	OF_CAT3	0.048	0.048	0.256	0.026	0.01	8.83	0.41	AR&R 5 year, AR&R 5 year	25 minutes sto	orm, average <i>i</i> orm, average 7	'9.1 mm/n, 20 79.1 mm/h Zo	ne 1
OF_CATT 0.082 0.082 0.032 0.033 0.02 1.056 0.048 ABR 5 year, 25 minutes stom, average 7.3 mmh, Zone 1 OF_CAT3 0.017 0.018 0.01 6.14 0.33 ABR 5 year, 25 minutes stom, average 7.3 mmh, Zone 1 OF_CAT3 0.009 0.026 0.035 0.02 10.01 0.48 ABR 5 year, 25 minutes stom, average 7.3 mmh, Zone 1 OF_CAT1 0.094 0.026 0.035 0.02 10.01 0.48 ABR 5 year, 5 minutes stom, average 7.1 mmh, Zone 1 OF_CAT1 0.019 0.016 0.44 0.31 ABRR 5 year, 5 minutes stom, average 7.1 mmh, Zone 1 OF2AT1 0.019 0.026 0.001 0.44 0.31 ABRR 5 year, 5 minutes stom, average 7.3 mmh, Zone 1 OF2A 0.013 0.026 0.029 0.02 11.81 0.54 ABRR 5 year, 3 hours stom, average 2.5 mmh, Zone 1 OSD_TVO_STACE 0.134 0.147 0.266 0.002 11.81 0.54 ABRR 5 year, 3 hours stom, average 2.5 mmh, Zone 1 OSD_TVO_STACE 0.147 0.147 0.266 0.002 11.81 0.54 ABRR 5 year, 3 hours stom, average 2.5 mmh, Zone 1	OF_CAT5	0.094	0.094	0.256	0.035	0.02	10.91	0.48	AR&R 5 year,	5 minutes stor	m, average 15	54.5 mm/h, Zo	ne 1
OF_CAT7 0.018 0.018 0.258 0.018 0.011 6.14 0.033 RARK 5 year, 25 minutes storm, average 7.1 mr/h. Zone 1 OF_CAT9 0.095 0.0256 0.036 0.012 10.01 0.048 K 5 year, 25 minutes storm, average 7.1 mr/h. Zone 1 OF_CAT1 0.019 0.049 0.0256 0.034 0.02 10.01 0.48 RK 5 year, 25 minutes storm, average 7.1 mr/h. Zone 1 OF_CAT1 0.019 0.019 0.256 0.019 0.01 6.44 0.013 RKR 5 year, 25 minutes storm, average 7.1 mr/h. Zone 1 OF33 0.036 0.036 0.021 0.11 0.54 RKR 5 year, 25 minutes storm, average 2.5 mr/h. Zone 1 OF26 0.019 0.256 0.019 0.02 11.81 0.54 RKR 5 year, 3 hours storm, average 2.5 mr/h. Zone 1 OF20 0.134 0.134 0.256 0.039 0.02 11.81 0.54 RKR 5 year, 3 hours storm, average 2.5 mr/h. Zone 1 DETENTION BASIN DETAILS Max/U Max Q	OF_CAT6	0.082	0.082	0.256	0.033	0.02	10.56	0.46	AR&R 5 year,	25 minutes sto	orm, average 7	79.1 mm/h, Zo	ne 1
OPC_0218 ODD OD	OF_CAT7	0.018	0.018	0.256	0.018	0.01	6.14	0.33	AR&R 5 year,	25 minutes sto	orm, average 7	79.1 mm/h, Zo	ne 1
OF_CAT10 0.094 0.094 0.094 0.094 0.094 0.094 0.010 0.014 0.012 10.74 10.5 RRB.R Syear_Smutules storm, average 78.1 mmh, Zone 1 OF33 0.036 0.036 0.026 0.019 0.01 6.44 0.31 RRB.R Syear_Smutules storm, average 78.1 mmh, Zone 1 OF26 0.019 0.256 0.019 0.016 6.44 0.31 RRB.R Syear_Smutules storm, average 78.1 mmh, Zone 1 OF26 0.014 0.134 0.256 0.039 0.02 11.81 0.54 RRB.R Syear_Smutules storm, average 78.1 mmh, Zone 1 OF26 0.134 0.134 0.256 0.039 0.02 11.81 0.54 RRB.R Syear_Smutules storm, average 78.1 mmh, Zone 1 DF20POBED_FL 0.147 0.147 0.256 0.034 0.02 11.99 0.57 ARBR Syear_S hours storm, average 78.1 mmh, Zone 1 DETENTION BASIN DETAILS Nax Q Max Q </td <td>OF_CAT8</td> <td>0.017</td> <td>0.017</td> <td>0.256</td> <td>0.018</td> <td>0.01</td> <td>10.91</td> <td>0.31</td> <td>AR&R 5 year, AR&R 5 year</td> <td>5 minutes stor</td> <td>m. average 15</td> <td>54.5 mm/h. Zo</td> <td>ne 1</td>	OF_CAT8	0.017	0.017	0.256	0.018	0.01	10.91	0.31	AR&R 5 year, AR&R 5 year	5 minutes stor	m. average 15	54.5 mm/h. Zo	ne 1
OP_CAT11 0.019 0.026 0.019 0.01 0.31 ARR 5 year, 25 minutes storm, average 79.1 mm/h, Zone 1 OP3 0.038 ARR 5 year, 25 minutes storm, average 79.1 mm/h, Zone 1 0.011 0.031 ARR 5 year, 25 minutes storm, average 79.1 mm/h, Zone 1 OP25 0.014 0.014 0.026 0.032 0.011 0.051 ARR 5 year, 25 minutes storm, average 79.1 mm/h, Zone 1 OP25 0.014 0.014 0.026 0.032 0.011 0.051 ARR 5 year, 3 hours storm, average 25.8 mm/h, Zone 1 OP25 0.014 0.017 0.026 0.039 0.022 11.81 0.054 ARR 5 year, 3 hours storm, average 25.8 mm/h, Zone 1 DETENTION BASIN DETALS Image	OF_CAT10	0.094	0.094	0.256	0.034	0.02	10.74	0.5	AR&R 5 year,	5 minutes stor	m, average 15	54.5 mm/h, Zo	ne 1
OF33 0.036 0.036 0.036 0.036 0.037 0.038 ARR S year. 25 minutes storm, average 75.1 mm/h. Zone 1 OP25 0.1134 0.134 0.256 0.039 0.02 11.81 0.54 ARR S year. 25 minutes storm, average 75.1 mm/h. Zone 1 OSD_TVO_STAGE 0.134 0.134 0.256 0.039 0.02 11.81 0.54 ARR S year. 3 hours storm, average 25.8 mm/h. Zone 1 SPROPOSED_FLC 0.147 0.147 0.256 0.04 0.02 11.81 0.54 ARR S year. 3 hours storm, average 25.8 mm/h. Zone 1 B_PROPOSED_FLC 0.147 0.256 0.04 0.02 11.99 0.57 ARR S year. 3 hours storm, average 25.8 mm/h. Zone 1 DETENTION BASIN DETAILS P P P P P P P OSD 58.03 480.9 0.134 0 0.134 P P P P CONTINUTY CHECK for AR&R 5 year. 2 hours storm, average 33 mm/h. Zone 1 P P P P P P P P P <t< td=""><td>OF_CAT11</td><td>0.019</td><td>0.019</td><td>0.256</td><td>0.019</td><td>0.01</td><td>6.44</td><td>0.31</td><td>AR&R 5 year,</td><td>25 minutes sto</td><td>orm, average 7</td><td>79.1 mm/h, Zo</td><td>ne 1</td></t<>	OF_CAT11	0.019	0.019	0.256	0.019	0.01	6.44	0.31	AR&R 5 year,	25 minutes sto	orm, average 7	79.1 mm/h, Zo	ne 1
Out2 Out3 Out3 Out3 Out3 Out13 Out3 Out2 11.81 Out4RR 5 year, 3 hours storm, average 25.8 mm/h, Zone 1 DF2 0.147 0.147 0.256 0.04 0.02 11.81 O.54 AR& 5 year, 3 hours storm, average 25.8 mm/h, Zone 1 DETENTION BASIN DETALS	OF33	0.036	0.036	0.256	0.024	0.01	7.93	0.38	AR&R 5 year,	25 minutes sto	orm, average 7	79.1 mm/h, Zo	ne 1
Dres Dres <thdres< th=""> Dres Dres <thd< td=""><td>OFZO OSD TWO STAGE</td><td>0.019</td><td>0.019</td><td>0.256</td><td>0.019</td><td>0.01</td><td>6.44 11 81</td><td>0.31</td><td>AR&R 5 year, AR&R 5 year</td><td>25 minutes store</td><td>average 7</td><td>9.1 mm/n, 20 mm/h. 700e</td><td>1 1</td></thd<></thdres<>	OFZO OSD TWO STAGE	0.019	0.019	0.256	0.019	0.01	6.44 11 81	0.31	AR&R 5 year, AR&R 5 year	25 minutes store	average 7	9.1 mm/n, 20 mm/h. 700e	1 1
B_PROPOSED_FLQ 0.147 0.147 0.256 0.04 0.02 11.99 0.57 A&&R 5 year. 3 hours storm, average 2.8 mm/h, Zone 1 DETENTION DASIN DETAILS N N N N N N N DETENTION PASIN DETAILS N N N N N N N N Name Max/VL Max/Q Max/Q <t< td=""><td>OF29</td><td>0.134</td><td>0.134</td><td>0.256</td><td>0.039</td><td>0.02</td><td>11.81</td><td>0.54</td><td>AR&R 5 year,</td><td>3 hours storm</td><td>, average 25.8</td><td>mm/h, Zone</td><td>1</td></t<>	OF29	0.134	0.134	0.256	0.039	0.02	11.81	0.54	AR&R 5 year,	3 hours storm	, average 25.8	mm/h, Zone	1
Image Image <th< td=""><td>B_PROPOSED_FLC</td><td>0.147</td><td>0.147</td><td>0.256</td><td>0.04</td><td>0.02</td><td>11.99</td><td>0.57</td><td>AR&R 5 year,</td><td>3 hours storm</td><td>, average 25.8</td><td>mm/h, Zone</td><td>1</td></th<>	B_PROPOSED_FLC	0.147	0.147	0.256	0.04	0.02	11.99	0.57	AR&R 5 year,	3 hours storm	, average 25.8	mm/h, Zone	1
DETENTION BASIN DETAILS Max Q Max		L											
Name Max VL Max Q Max Q <th< td=""><td>DETENTION BASIN</td><td>DETAILS</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	DETENTION BASIN	DETAILS											
OSD 58.03 480.9 0.134 0 0.134 0 0.134 0 0.134 0 0.134 0 0.134 0 0.134 0 0.134 0 0.134 0	Name	Max WL	MaxVol	Max Q	Max Q	Max Q							
OSD 58.03 480.9 0.134 0 0.134 0 0.134 0				Total	Low Level	High Level							
CONTINUITY CHECK for AR&R 5 year, 2 hours storm, average 33 mm/h, Zone 1	USD	58.03	480.9	0.134	0	0.134							
Node Inflow Outflow Storage Chan Difference Image: Constraint of the storage chan Image: Constrain Image: Constorain Image: Con		K for AR&R 5	vear. 2 hours	storm, average	33 mm/h 7004	I e 1							
(cu.m) (cu.m) % </td <td>Node</td> <td>Inflow</td> <td>Outflow</td> <td>Storage Chan</td> <td>Difference</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	Node	Inflow	Outflow	Storage Chan	Difference								
1 49.21 49.21 0		(cu.m)	(cu.m)	(cu.m)	%								
141.03 111.03 0 <td< td=""><td>1</td><td>49.21</td><td>49.21</td><td>0</td><td>0</td><td></td><td></td><td></td><td></td><td>[</td><td></td><td></td><td></td></td<>	1	49.21	49.21	0	0					[
4 60.31 0 <td>2</td> <td>141.63 71 24</td> <td>141.63 71 24</td> <td>0</td> <td>0</td> <td></td> <td> </td> <td> </td> <td></td> <td></td> <td></td> <td></td> <td></td>	2	141.63 71 24	141.63 71 24	0	0								
5 142.48 142.48 0 <td< td=""><td>4</td><td>60.31</td><td>60.31</td><td>0</td><td>0</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	4	60.31	60.31	0	0								
6 101.84 101.84 0 <td< td=""><td>5</td><td>142.48</td><td>142.48</td><td>0</td><td>0</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	5	142.48	142.48	0	0								
1 29.25 0 <td>6</td> <td>101.84</td> <td>101.84</td> <td>0</td> <td>0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	6	101.84	101.84	0	0								
9 144.3 144.3 0 0 </td <td>~ 7</td> <td>29.25</td> <td>29.25</td> <td>0</td> <td>0</td> <td></td> <td> </td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	~ 7	29.25	29.25	0	0								
10 142.35 142.35 0 <t< td=""><td>9</td><td>144.3</td><td>144.3</td><td>0</td><td>0</td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	9	144.3	144.3	0	0								
11 29.09 29.09 0	10	142.35	142.35	0	0								
ANS 1/9.2/ 1/9.2/ 0 <	11	29.09	29.09	0	0								
Difference O I ALS O I ALS <td>ANS BNS</td> <td>179.27</td> <td>179.27</td> <td>0</td> <td>0</td> <td></td> <td> </td> <td> </td> <td></td> <td></td> <td></td> <td></td> <td></td>	ANS BNS	179.27	179.27	0	0								
N28 53.65 53.65 0 0	N27	312.35 49.21	312.35 49.21	0	0								
N29 29.09 29.09 0 0 1 <th1< td=""><td>N28</td><td>53.65</td><td>53.65</td><td>0</td><td>0</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th1<>	N28	53.65	53.65	0	0								
0SD 804.16 445.88 358.33 0	N29	29.09	29.09	0	0								
N46 528.29 528.29 0	USD N36	804.16	445.88	358.33	0								
N47 528.13 528.13 0 0 0 0 0 Run Log for OSD_FINAL.drn run at 15:59:51 on 30/8/2010 Image: Constraint of the second secon	N46	445.72 528.29	445.72 528.29	0	0								
Image: Note of the second se	N47	528.13	528.13	0	0								
Run Log for USD_FINAL.drn run at 15:59:51 on 30/8/2010				/- ·									
	Run Log for OSD_F	INAL.drn run	at 15:59:51 on	30/8/2010	1		<u> </u>	<u> </u>					

	Name and F	ilo Path:	E·\AA003465\	D-Calculations\	Stormwater\09	SD Final drn					
DRAINS Version:		2010.01 - 5 A	ugust 2010		Stormwater O						
Modeller's Name:		Chris McClella	and								
Description:		Macquarie Pa	irk Commerce	Centre OSD DR	AINS Model						
DRAINS results pre	epared 30 Aug	ust. 2010 from	Version 2010.	09							T O
									K	ESUL	15
PIT / NODE DETAI	LS			Version 8			-		20	VEAR	ΔRI
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min Freeboard	Overflow	Constraint		20		
		IIGL	(cu.m/s)	(cu.m)	(m)	(cu.iii/s)					
SUB-CATCHMENT	DETAILS	David	0	David	0	0	Due la Olema				
Name	Max Flow Q	Paved Max Q	Grassed Max Q	Paved Tc	Grassed Tc	Supp. Tc	Due to Storm				
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)					
Cat1	0.043	0.04	0.003	5	6	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat2	0.119	0.119	0 013	3	0	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1 Zone 1	
Cat4	0.002	0.03	0.013	3	6	0	AR&R 20 yea	ir, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat5	0.12	0.12	0	3	0	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat6	0.108	0.031	0.077	6	7	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat/	0.024	0.024	0 009	6	0	0	AR&R 20 yea	ir, 25 minutes storm, averag	e 101.2 mm/h, e 101 2 mm/h	Zone 1 Zone 1	
Cat9	0.020	0.122	0.005	3	0	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat10	0.12	0.12	0	3	0	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
Cat11	0.025	0.024	0	4	5	0	AR&R 20 yea	r, 25 minutes storm, averag	e 101.2 mm/h,	Zone 1	
A_NAT_STATE B_NAT_STATE	0.155	0	0.155	0	15	0	AR&R 20 yea	ir, 2 nours storm, average 4 ir, 2 hours storm, average 4	3.2 mm/n, Zone 3.2 mm/h. Zone	• 1 • 1	
	0.004		0.004	0		0		,		- 	
A 15											
Outflow Volumes fo	r Total Catchn	nent (1.29 impe Total Pupoff	ervious + 1.83	Pervious = 3.12	total ha)						
Storm	cu.m	cu.m (Runoff	cu.m (Runoff	cu.m (Runoff %	()						
AR&R 20 year, 5 m	507.29	303.20 (59.8%	197.05 (93.8%	106.15 (35.7%)						
AR&R 20 year, 10 r	787.62	549.67 (69.8%	313.08 (96.0%	236.59 (51.3%)						
AR&R 20 year, 15 r	998.71 1170.22	734.33 (73.5% 883 41 (75.5%	400.46 (96.9%	333.87 (57.0%)			<u> </u>			
AR&R 20 year. 25 r	1317.03	1003.66 (76.2	532.22 (97.6%	471.44 (61.1%	,)						
AR&R 20 year, 30 r	1443.01	1104.29 (76.5	584.36 (97.8%	61.5%)						
AR&R 20 year, 45 r	1754.57	1357.46 (77.4	713.33 (98.29	644.13 (62.6%)			<u> </u>			
AR&R 20 year, 1 ho AR&R 20 year, 1 5	2002.1	1561.05 (78.0	976 09 (98.4%	745.26 (63.5% 897.12 (64.1%)						
AR&R 20 year, 2 ho	2698.62	2120.22 (78.6	1104.08 (98.8	1016.14 (64.29	%)						
AR&R 20 year, 3 ho	3185.87	2505.70 (78.7	1305.74 (99.0	1199.96 (64.39	%)						
Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm						
	(cu.m/s)	(m/s)	HGL (m)	HGL (m)							
CHANNEL DETAIL	S Max O	Max V	Chainage	Max	Due to Storm						
Indifie	(cu.m/s)	(m/s)	(m)	HGL (m)	Due to otomi						
OVERFLOW ROUT			Sofo O	May D		Max Width	MovV	Due to Storm			
OF CAT1	Max Q 0/S 0.043	Max Q D/S 0.043	Sale Q 0.256	0.026	0.01	Nax Width 8.53	0.39	AR&R 20 year. 25 minutes	storm, average	101.2 mm/h	Zone 1
OF_CAT2	0.119	0.119	0.256	0.037	0.02	11.45	0.52	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT3	0.062	0.062	0.256	0.029	0.01	9.73	0.44	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT4	0.057	0.057	0.256	0.028	0.01	9.43	0.43	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1 Zone 1
OF_CAT6	0.108	0.108	0.256	0.036	0.02	11.27	0.5	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT7	0.024	0.024	0.256	0.02	0.01	6.74	0.35	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT8	0.023	0.023	0.256	0.02	0.01	6.74	0.33	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT9 OF CAT10	0.122	0.122	0.256	0.037	0.02	11.45	0.53	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF_CAT11	0.025	0.025	0.256	0.021	0.01	7.03	0.33	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OF33	0.046	0.046	0.256	0.026	0.01	8.83	0.39	AR&R 20 year, 25 minutes	storm, average	101.2 mm/h,	Zone 1
OSD TWO STAGE	0.025	0.025	0.256	0.021	0.01 0.03	7.03 13.07	0.33	AR&R 20 year, 25 minutes	sorm, average	: 101.∠ mm/h, .2 mm/h. 7one	
OF29	0.204	0.204	0.256	0.045	0.03	13.07	0.62	AR&R 20 year, 2 hours sto	rm, average 43	.2 mm/h, Zone	1
B_PROPOSED_FL	0.256	0.256	0.256	0.05	0.03	13.97	0.66	AR&R 20 year, 1.5 hours s	torm, average 5	51 mm/h, Zone	1
								<u> </u>			
DETENTION BASI	N DETAILS			1			<u> </u>		1	<u> </u>	
Name	Max WL	MaxVol	Max Q	Max Q	Max Q						
080	E0.05	ECAO	Total	Low Level	High Level						
030	58.25	504.2	0.204	0	0.204						
CONTINUITY CHE	CK for AR&R	20 year, 2 hour	rs storm, avera	ge 43.2 mm/h, 2	Zone 1						
Node	Inflow	Outflow	Storage Chan	Difference							
4	(cu.m)	(cu.m)	(cu.m)	% ^				<u> </u>			
2	186.09	186.09	0	0							
3	95.96	95.96	0	0							
4	82.67	82.67	0	0							
6	187.2	187.2	0	0							
7	38.43	38.43	0	0							
8	33.89	33.89	0	0							
9	189.59	189.59	0	0				├			
10	38.31	38.31	0	0							
ANS	281.4	281.4	0	0							
BNS	584.46	584.46	0	0				<u> </u>			
N28	05.25 72 32	05.25 72 32	0	0							
N29	38.31	38.31	0	0							
OSD	1078.49	718.89	359.66	0							
N36 N46	718.73	718.73	0	0							
N47	829.04	829.04	0	0							
			Ľ								
Run Log for OSD_F	INAL.drn run	at 16:13:42 or	n 30/8/2010		DECES						
The maximum flow	exceeded the	sate value in the	ne tollowing ov	ertiow routes: B	PROPOSED	FLOW	I	1	1		

		la Deth								
DRAINS Mode	I Name and F	11e Path: 2010.01 - 5 A	F:\AA003465\ ugust 2010	D-Calculations\	Stormwater\O	SD_Final.drn				
Modeller's Name:		Chris McClella	and							
Description:		Macquarie Pa	rk Commerce	Centre OSD DR	AINS Model					-
DRAINS results pre	nared 30 Aug	ist 2010 from	Version 2010 (10						
DIVANO results pre	pared 50 Aug		Version 2010.0						RESU	LIS
PIT / NODE DETAIL	LS			Version 8						
Name	Max HGL	Max Pond	Max Surface	Max Pond	Min	Overflow	Constraint			
		HGL	Flow Arriving	(cu.m)	(m)	(cu.m/s)				
N36	55.8		0.232	(00111)	()					
SUB-CATCHMENT	DETAILS	Payod	Grassod	Payod	Grassod	Supp	Duo to Storm			
Indille	Flow Q	Max Q	Max Q	Tc	Tc	Tc	Due to Storm			
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)				
Cat1	0.05	0.047	0.004	5	6	0	AR&R 100 ye	ar, 1.5 hours storm, average	66.4 mm/h, Zone 1	
Cat2 Cat3	0.15	0.15	0.015	3	0	0	AR&R 100 ye AR&R 100 ye	ar, 5 minutes storm, average	e 163.6 mm/n, Zone 1	
Cat4	0.067	0.047	0.021	3	6	0	AR&R 100 ye	ar, 1.5 hours storm, average	66.4 mm/h, Zone 1	
Cat5	0.151	0.151	0	3	0	0	AR&R 100 ye	ar, 5 minutes storm, average	247.4 mm/h, Zone 1	
Cat6	0.129	0.036	0.095	6	7	0	AR&R 100 ye	ar, 2 hours storm, average 56	6.5 mm/h, Zone 1	
Cat8	0.028	0.028	0.01	6	7	0	AR&R 100 ye	ar, 25 minutes storm, average	e 129.8 mm/h, Zone 1	
Cat9	0.153	0.153	0	3	0	0	AR&R 100 ye	ar, 5 minutes storm, average	247.4 mm/h, Zone 1	
Cat10	0.151	0.151	0	3	0	0	AR&R 100 ye	ar, 5 minutes storm, average	247.4 mm/h, Zone 1	
Cat11 A NAT STATE	0.031	0.03	0 199	4	5	0	AR&R 100 ye	ar, 5 minutes storm, average	247.4 mm/h, Zone 1 9 mm/h, Zone 1	
B_NAT_STATE	0.199	0	0.199	0	15	0	AR&R 100 ye	ar, 1 hour storm, average 82.	.9 mm/h, Zone 1	
	r Total Catal	ont (1.00 :			total bc)					
Storm	Total Rainfall	Total Runoff	Impervious R	Pervious = 3.12	ເບເລເ na) ff					
	cu.m	cu.m (Runoff	cu.m (Runoff	cu.m (Runoff %	%)					
AR&R 100 year, 5 n	643.94	438.25 (68.1%	253.61 (95.1%	184.64 (48.9%)					-
AR&R 100 year, 10	1003.65	763.30 (76.1%	402.50 (96.9%	360.80 (61.3%)					
AR&R 100 year, 15	1277.47	1207.49 (80 5	608.07 (97.9%	+∍∠.∋0 (03.8% 599.42 (68.2%)					
AR&R 100 year, 25	1689.24	1367.68 (81.0	686.28 (98.2%	681.40 (68.8%)					
AR&R 100 year, 30	1855.3	1510.59 (81.4	755.02 (98.3%	755.57 (69.5%)					
AR&R 100 year, 45	2262.9	1861.78 (82.3 2143 02 (82 9	923.73 (98.6% 1058 84 (09 9	938.04 (70.7%) %)			├		
AR&R 100 year, 1.5	3110.91	2590.73 (83.3	1274.73 (99.0	1316.00 (72.2%	%)					
AR&R 100 year, 2 h	3529.44	2946.49 (83.5	1447.98 (99.1	1498.51 (72.49	%)					
AR&R 100 year, 3 h	4207.22	3514.74 (83.5	1728.54 (99.3	1786.20 (72.4%	%)					-
PIPE DETAILS										
Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm					
	(cu.m/s)	(m/s)	HGL (m)	HGL (m)						
CHANNEL DETAIL	<u></u>									
Name	Max Q	Max V	Chainage	Max	Due to Storm					
	(cu.m/s)	(m/s)	(m)	HGL (m)						
Name	E DETAILS Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm		
OF_CAT1	0.05	0.05	7.665	0.027	0.01	9.13	0.4	AR&R 100 year, 1.5 hours si	torm, average 66.4 mm/h,	Zone 1
OF_CAT2	0.15	0.15	7.665	0.041	0.02	12.17	0.55	AR&R 100 year, 5 minutes s	torm, average 247.4 mm/ł	n, Zone 1
OF_CAT3	0.073	0.073	7.665	0.031	0.01	10.2	0.46	AR&R 100 year, 15 minutes	storm, average 163.6 mm	/h, Zone 1
OF_CAT5	0.007	0.007	7.665	0.03	0.01	12.17	0.45	AR&R 100 year, 5 minutes s	torm, average 247.4 mm/l	n, Zone 1
OF_CAT6	0.129	0.129	7.665	0.038	0.02	11.63	0.54	AR&R 100 year, 2 hours sto	rm, average 56.5 mm/h, Z	one 1
OF_CAT7	0.028	0.028	7.665	0.022	0.01	7.33	0.34	AR&R 100 year, 20 minutes	storm, average 144.1 mm	/h, Zone 1
OF_CATO	0.026	0.026	7.665	0.021	0.01	12.17	0.36	AR&R 100 year, 25 minutes s	storm, average 129.6 mm	n, zone i . Zone 1
OF_CAT10	0.151	0.151	7.665	0.041	0.02	12.17	0.56	AR&R 100 year, 5 minutes s	torm, average 247.4 mm/l	n, Zone 1
OF_CAT11	0.031	0.031	7.665	0.023	0.01	7.63	0.35	AR&R 100 year, 5 minutes s	torm, average 247.4 mm/l	n, Zone 1
0F33 0F26	0.054	0.054	7.665	0.028	0.01	9.43	0.4	AR&R 100 year, 20 minutes	storm, average 144.1 mm torm, average 247.4 mm/	/n, ∠one 1 n. Zone 1
OSD_TWO_STAGE	0.232	0.232	7.665	0.048	0.03	13.61	0.64	AR&R 100 year, 2 hours sto	rm, average 56.5 mm/h, Z	one 1
OF29	0.232	0.232	7.665	0.048	0.03	13.61	0.64	AR&R 100 year, 2 hours sto	rm, average 56.5 mm/h, Z	one 1
B_PROPOSED_FL	0.293	0.293	7.665	0.053	0.04	14.51	0.69	AR&R 100 year, 1.5 hours st	torm, average 66.4 mm/h,	Zone 1
DETENTION BASIN	N DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q					
OSD	58 64	710 1	1 otal 0.232	LOW LEVEI	nign Level 0.232					-
	00.04	, 10.1	0.202	0	0.202					
CONTINUITY CHEC	CK for AR&R 1	00 year, 1 hou	ir storm, avera	ge 82.9 mm/h, z	Cone 1					
Node	Inflow	Outflow	Storage Chan	Difference %				├───┤───┤		
1	62.98	62.98	(00.11)	0						
2	178.46	178.46	0	0						
3	93.65	93.65	0	0						
4	81.6 179.52	81.6 179.52	0	0						
6	154.73	154.73	0	0					<u></u>	
7	36.85	36.85	0	0						
8	33.74	33.74	0	0				├───┤───┤		
10	179.36	179.36	0	0						
11	36.8	36.8	0	0						
ANS	300.26	300.26	0	0						
BNS N27	623.22 62 QR	623.22 62 QR	0	0						+
N28	70.6	70.6	0	0						
N29	36.8	36.8	0	0						
OSD N36	1049.15	677.21	372.02	0	ļ					
N46	784.27	784.27	0	0						
N47	78/ 1	784.1	0	0			l			
	704.1	101.1	-							
		at 16:12:42	30/8/2010							

ARI - 5YR Peak Flows									
	A - 'Natural	A - Proposed	B - 'Natural	B - Proposed					
Duration (min)	State'	Development	State'	Development	WL (mAHD)				
5	0.030	0.030	0.054	0.057	57.110				
10	0.056	0.027	0.103	0.058	57.330				
15	0.074	0.032	0.136	0.070	57.500				
20	0.088	0.032	0.162	0.069	57.630				
25	0.096	0.033	0.179	0.078	57.730				
30	0.095	0.031	0.184	0.073	57.810				
45	0.094	0.027	0.187	0.063	58.000				
60	0.104	0.030	0.206	0.110	58.020				
90	0.103	0.032	0.216	0.120	58.020				
120	0.133	0.031	0.220	0.131	58.030				
240	0.087	0.017	0.171	0.147	58.030				
Peak	0.133	0.033	0.220	0.147	58.030				

ARI - 20YR Peak Flows										
	A - 'Natural	A - Proposed	B - 'Natural	B - Proposed						
Duration (min)	State'	Development	State'	Development	WL (mAHD)					
5	0.049	0.038	0.089	0.072	57.230					
10	0.086	0.035	0.158	0.073	57.520					
15	0.113	0.041	0.207	0.089	57.730					
20	0.134	0.041	0.245	0.087	57.910					
25	0.144	0.043	0.269	0.100	58.020					
30	0.139	0.039	0.269	0.177	58.040					
45	0.137	0.036	0.271	0.218	58.080					
60	0.150	0.038	0.296	0.228	58.140					
90	0.143	0.042	0.301	0.256	58.200					
120	0.155	0.040	0.304	0.249	58.250					
240	0.123	0.022	0.244	0.230	58.120					
Peak	0.155	0.043	0.304	0.256	58.250					

ARI - 100YR Peak Flows												
	A - 'Natural A - Proposed B - 'Natural B - Proposed											
Duration (min)	State'	Development	State'	Development	WL (mAHD)							
5	0.073	0.050	0.134	0.093	57.380							
10	0.125	0.043	0.229	0.093	57.760							
15	0.163	0.050	0.299	0.128	58.020							
20	0.188	0.050	0.354	0.243	58.120							
25	0.190	0.049	0.365	0.354	58.180							
30	0.184	0.046	0.356	0.245	58.220							
45	0.183	0.044	0.359	0.243	58.350							
60	0.199	0.047	0.394	0.272	58.490							
90	0.183	0.050	0.385	0.293	58.560							
120	0.196	0.049	0.391	0.286	58.640							
240	0.158	0.027	0.315	0.258	58.400							
Peak	0.199	0.050	0.394	0.354	58.640							











