CONDOBLIN ETHANOL SITE

PRELIMINARY GEOTECHNICAL INVESTIGATION

FOR SWAN HILL ETHANOL PTY LTD

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TYPICAL LANDSCAPE OF THE CONDOBLIN SITE

GTS Report Number 06/4479 January 2007

DISCLAIMER

This investigation has been carried out in goodwill and under the instructions of the Swan Hill Ethanol. The investigation has been undertaken with the care and skill of competent personnel as defined within Geotechnical Testing Services quality system. It is not a comprehensive investigation but a guide to the conditions throughout the designated area.

The results from this investigation relate to the specified sites labelled throughout this document, and hence the information obtained may need to be extrapolated to the rest of the designated area. While care has been taken throughout this investigation, soil conditions can vary between each individual test site and at depths greater than that excavated during this investigation. The actual conditions of the whole area can only be determined with further excavation. Hence, if variations from this report are found during excavations/construction then Geotechnical testing Services should be notified so it can be assessed and appropriate advice provided.

This document has been prepared for the Swan Hill Ethanol, and hence no responsibility or liability is being accepted to any third party, where any part of the report is used in either isolation or without consideration of the whole document. This document is not appropriate where there has been a significant change in the project or either for the specific needs of the reader.

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1 INTRODUCTION

Swan Hill Ethanol commissioned Geotechnical Testing Services (GTS) to undertake a geotechnical investigation for a proposed Ethanol Plant in the Condoblin Region. Both the field investigation and report were undertaken and completed by suitably qualified and/or experienced staff members. GTS has also the appropriate insurances required to undertake such work, and they are available upon request. The purpose of the investigation was to provide the relevant site and soil information for a future design and construct contract.

The investigation included six excavated test pits. The approximate dimension of each pit was three to four metres in depth, three to four metres in length and approx. half a metre in width. At each pit, a series of soil and geotechnical information was collected to provide the required information for the aforementioned contract.

The report presents all the soil and geotechnical information collected from the investigation with particular attention given to subsurface conditions in the location of proposed storage dams. The report will also provide

- a site classification in accordance with Australian Standard 2870 for any proposed small structures for this site
- preliminary recommendation on the maximum allowable bearing pressures for large or heavy loaded buildings
- preliminary assessment of the sub-grade conditions for proposed access roads
- preliminary advice on the suitability of the soil and proposed earthworks for dams
- preliminary advice on hardstand areas, retaining walls and batters on embankments

2 SITE AND GEOLOGY

2.1 SITE LOCATION AND GENERAL CONDITION

The proposed Ethanol plant is located approximately 5km north west of the Condoblin Township (Page Appendix (A)1). Price Merrit Pty Ltd completed a full feature survey of the site, and GTS has used a portion of this survey to highlight the location of each pit undertaken at the property (Page A2).

The property has experience unprecedented drought conditions in recent years, and subsequently the site was incredibly dry. At the time of this investigation the site had a very slight fall to the north east of the property. The surface of the site was dry, well covered in grasses and there were also no visual signs of any rock outcrops. However, there was visual evidence of surface cracking over the site. The land is relevantly clear with a few large trees present. Several photos of the area were taken during the investigation, some of which highlight the aforementioned features (Page A3-A4), namely

- The excavation of a test pit
- General landscape and vegetation of the area
- Surface cracking over the area
- A neighbouring dam to the test pit area

GTS has taken more photos of the site and these would be made available, if required.

2.2 GEOLOGY

The Condoblin ethanol site falls within the Murray Basin geological structure. The Murray Basin landscape predominantly Aeolian consisting of sandy ridges interrupted by clay pans and lunettes. Information provided by Department of Primary Industries- Minerals.

3 FIELD WORK

The geotechnical investigation was carried out in accordance with Australian Standard (AS) 1726 – Geotechnical Site Investigations. The location of test pits was provided by Mr Stewart Rendell of Swan Hill Ethanol, and each pit was excavated by Warren Ross Excavations in December, 2006, using a 20 tonne excavator. The field investigation was completed by Mr John Boykett, which included soil profiling and the taking field samples. Dr Scott Pigdon provided off-site supervision when required.

The geotechnical investigation consisted of field testing and the sampling of each soil at each varying soil profile. Field tests included both pocket penetrometer readings and dynamic cone penetration tests (depending upon soil structures). Disturbed samples were also recovered from test pits for laboratory testing.

On completion of each test pit, the excavated soil was used to backfill the open pit and then compacted to an appropriate level.

4. RESULTS

4.1 FIELD RESULTS – SOIL PROFILES

The soil profile observed in the wall of each test pit was found to be relatively consistent between the surface and approx. 1200mm.

• 0-200mm Sandy silty top soil, brown

• 200-600mm Silty clay, brown, high plasticity

• 600-1200mm Silty clay, pale red/brown, moderate plasticity

There were various soil profiles logged between 1200-4000mm, which were combinations of silty sandy clay to gravely clay, various colours and typically moderately to highly plastic (pages A5-A7). During the excavation of all 6 test pits no ground water was encountered.

4.2 FIELD RESULTS - DYNAMIC CONE PENETROMETER RESULTS AND POCKET PENETROMTER RESULTS

The field investigation consisted of pocket penetrometer (PP) readings at every 1000mm, and each sample tested had an estimated shear capacity in excess of 225 kPa. A summary of PP results are presented in Table 4.1. Dynamic cone penetration (DCP) tests were preformed at the surface level of each pit and at every 100mm to approx. 500mm below ground level. An allowable bearing pressure was then calculated using Stockwell, M.J. (1977). Typically, the allowable bearing capacity of the soil at each level tested was in excess of 240 kPa. A summary of the DCP tests can be observed in Table 4.2.

Table 4.1 Summary of the Field Testing

(Pocket Penetrometer - Estimated Shear Strength (kPa))

Depth (mm)	Test Pit 1	Test Pit 2	Test Pit 3	Test Pit 4	Test Pit 5	Test Pit 6
1000	+225	+225	+225	+225	+225	+225
2000	+225	+225	+225	+225	+225	+225
3000	+225	+225	+225	+225	-	+225
3500	+225	+225	-	-	-	-

Table 4.2 Summary of the Field Testing (DCP - Estimated Bearing Capacity (kPa))

Depth (mm)	Test Pit 1	Test Pit 2	Test Pit 3	Test Pit 4	Test Pit 5	Test Pit 6
0-100	240	240	170	210	240+	240
100-200	240+	240+	210	210	230	240+
200-300	240+	240+	230	230	210	240+
300-400	240+	240+	240	240+	240	240+
400-500	240+	240+	240+	240+	240+	240+

4.3 LABORATORY RESULTS

The laboratory investigations were completed on eight selected samples over the six excavated test pits and at various soil depths. Soil tests preformed included Moisture Contents, Atterberg Limits, Sieve Analysis and Emerson Class Numbers. A summary of the results from each selected soil can be observed in Table 4.3. At each test pit soil samples were obtained immediately below topsoil at a depth of approximately 300mm. A California Bearing Ratio (CBR) was completed on each soil completed from this depth, and a summary of CBR results can be observed in Table 4.4.

Table 4.3 Summary of the Laboratory Testing

	Soil Moisture		Atterberg Limits				Soil	
Number	Depth (mm)	-	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Linear Shrinkage (%)	Passing 75μm (%)	Emerson Number
1	200	3.6	19	11	8	1.5	44	2
1	1000	8.7	59	29	30	14.0	22	2
4	300	11.2	41	20	21	9.0	60	2
4	1100	21.9	62	25	37	16.5	82	2
5	500	18.5	45	26	19	10.0	52	2
5	700	14.4	35	22	13	6.0	26	2
5	2500	19.3	70	23	47	17.0	85	2
5	3500	20.9	57	21	36	13.0	76	2

Note:

GTS is a NATA accredited laboratory and the NATA reports on each soil test can be observed in pages A8-A15

Table 4.4 Summary of the Laboratory Testing
(4-Day Soaked CBR – 98% Compaction and 100% Optimum)

Test Pit Number	Soil Depth (mm)	Max. Dry Density (t/m ³)	Optimum Moisture Content (%)	Swell (%)	CBR (%)
1	200	2.01	8.7	0.0	13.0
2	500	1.53	24.6	0.5	12.5
3	200	1.82	12.8	0.5	5.5
4	300	1.59	20.3	0.0	5.0
5	700	1.61	20.8	0.0	16.5
6	200	1.94	10.6	0.0	8.0

5 PRELIMINARY RECOMMENDATIONS

At the time of preparing this report, the type and extent of earthworks for buildings, roadways, dams, retaining walls and storage areas were not known. Hence, the recommendations given below are of a general nature only and should be treated as such.

5.1 **BUILDINGS**

5.1.1 Small Domestic Type Buildings

Where this type of construction is proposed the Australian Standard AS 2870-1996 "Residential Slabs and Footings – Construction" may apply to forms of construction other than houses, including some light industrial, commercial and institutional buildings. If they are similar to houses in size, loading and superstructure flexibility (refer to Section 3.1.1 of this standard for applicability). Standard footing designs are given in Section 3 of this standard for slab-on-ground, stiffened rafts, waffle rafts, strip footings, pad footings and piled foundations.

Further testing of the site at the specific location of these buildings will be required but initial consideration could be made using a 'Class H-D' classification.

This is based on the climatic conditions for the site being semi-arid leading to deep seated moisture movement and the predominantly clay based material being highly reactive (linear shrinkage values ranged to 17.0%). 'Class H-D' places limits on types of slab and footing systems and the method of construction as well as drainage details and the type of plumbing fittings for pipework.

5.1.2 Large Or Heavily Loaded Structures

These will generally require a stiffened raft construction or deep spread footings (pad footings or strip footings). Where pad footings are proposed, it is advisable to consider the use of concrete tie beams between the footings to limit the amount of differential settlement. The footings should be founded a minimum of 600 mm below existing surface level and into the natural sandy, silty clay material.

Initial estimates of safe bearing capacity taken from field DCP readings and PP readings are:

Pad Footings 200 kPa Strip Footings 150 kPa

Using these values should provide adequate safety margin against shear failure of the soil and excessive settlement under load. Design parameters for these footings should be re-assessed when actual locations and relative magnitudes of these loads are known.

Further factors to consider are moisture conditions at the time of construction and the requirements for resistance to lateral loads and uplift.

For industrial slabs and pavements subjected to heavy and frequent traffic (e.g. forklift vehicles) the designer should give consideration to the possibility of pumping action of water in the clay material below the slab, as the natural material on site appears susceptible to this problem.

CBR estimates of 5.0 to 16.5 and the percentage of soil passing 75 microns being over 45% in five of eight samples tested for the clay sub-grade material on site indicate a granular sub-base material or some other type of sub-grade drainage is warranted.

5.2 ROADWORKS

The natural clay material on site extends to at least 4.0 m below surface and is considered highly reactive to moisture variations (swelling when wet and shrinking when dry). In addition, the CBR values recorded indicate a low modulus of sub-grade reaction of approximately 40 kPa/mm. On this basis, it is suggested that imported granular material be used for roadwork constructions and/or lime stabilization of the existing clay material be used.

It is also important that adequate drainage be provided during construction and for in-service conditions.

5.3 DAMS

Dams will most likely be placed on-site to catch surface run-off from roadways and buildings and possibly for effluent. The soil material on-site appears to be generally both sandy and gravely in nature and subsequently it is unlikely that will be sufficiently impermeable to hold water. It is also unlikely that these materials will be suitable for use in the construction of the embankments due to the potential risk of piping.

Given the predominately sandy and gravely nature of the subsoil and the limited volume of clay in the area investigated it would be likely that a High Density Polyethylene (HDPE) membrane or similar would be required to line the dams for the retention of water. The liner would need to be covered with 0.5m of fine grained soil to protect the HDPE from both drainage and ultra-violet light. During installation care would also be needed to avoid punctures within the liner.

Correct construction techniques and compaction testing should prevent most problems related to dam construction. Further testing of specific dam sites will be required so that more accurate soil parameters can be ascertained for wall and liner design.

5.4 HARDSTAND AREAS

Refer also to the section on Roadwork above. Hardstand areas for storing transient loads that are not sensitive to differential settlement may be treated as for roadworks.

Where loads are longer term and/or sensitive to excessive or differential settlement they should be supported on a footing system as discussed in section on Large or Heavily Loaded Structures above. It is worth reiterating that the natural materials on-site are considered very susceptible to moisture movement variation and as such will require adequate attention to design of surface drainage.

5.5 RETAINING WALLS

Should retaining walls be proposed then the following guidelines should be observed:

- i. A suggested value for the Co-efficient of Active Earth Pressure, Ka, is in the order of 0.33;
- ii. Natural material should not be used for backfill as it is too liable to shrinkage and swelling. A coarse granular backfill is recommended with adequate attention to surface and subsurface drainage made.

5.6 BATTERS ON EMBANKMENTS

For short-term batters a grade of 1:1 is considered safe for slope stability where cut-off drains are used on the high side of the embankment. For longer term batters this grade should be reduced to say 1 vertical: 2 horizontal. Being a clay material and considered only slightly dispersive then erosion of batters should not be problematic.

Surface drains above and below these batters should be provided.

5.7 CONCLUSION

These preliminary recommendations are based on conditions encountered on-site at the time of investigation and results of tests carried out both in the field and in the laboratory.

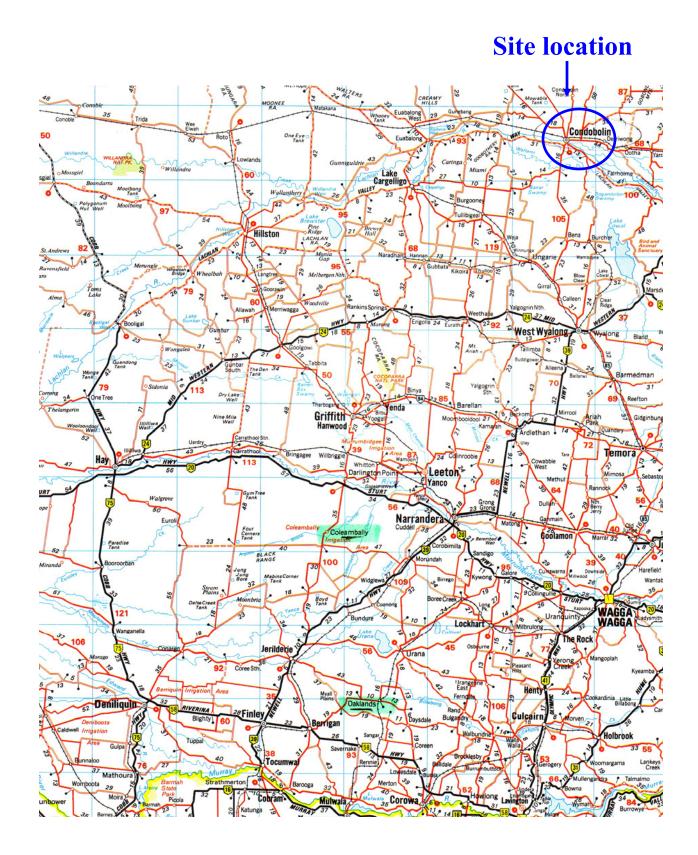
Although test results are generally consistent they are indicative for the locations tested only.

These recommendations are subject to verification by further investigations when the layout of the development and serviceability requirements are better understood.

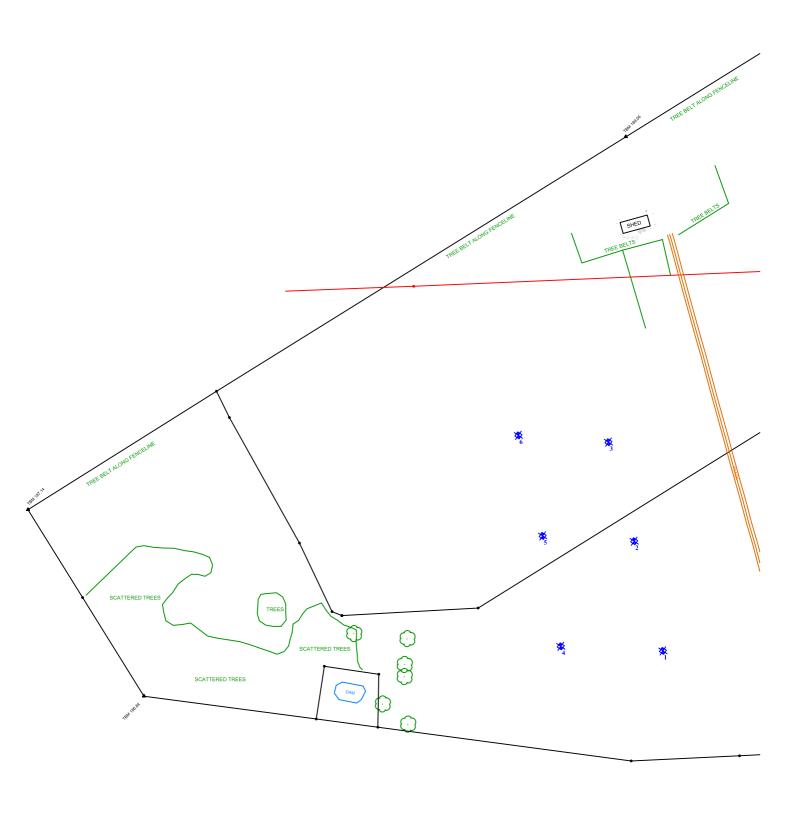
6 IMPORTANT NOTE

This report has highlighted several times that the subsoil present at Condoblin is susceptible to moisture movement variation. This investigation was undertaken during a period of extreme dry conditions, and subsequently sections of the subsoil are currently very dry. Hence, care is recommended.

APPENDIX



Location- Australian Road Atlas







Excavator and typical test pit



General landscape and vegetation of the area



Visual signs of surface cracking over the property



Dam with the vicinity of pits

TEST PITS No: 1 & 2

CLIENT: SWAN HILL ETHANOL Pty. Ltd LOCATION: CONDOBLIN JOB No.: 06-4479

METHOD: Test Pits- 22T Exacavator OPERATOR: John Boykett



LOG SHEET No: 1 OF 3

VS (very soft)

12-15

25-50

50-100

>200kPa

VSt (very stiff) 100-200

S (soft)

F (firm)

St (stiff)

H (hard)

4-10

30-50

MOISTURE CONDITION

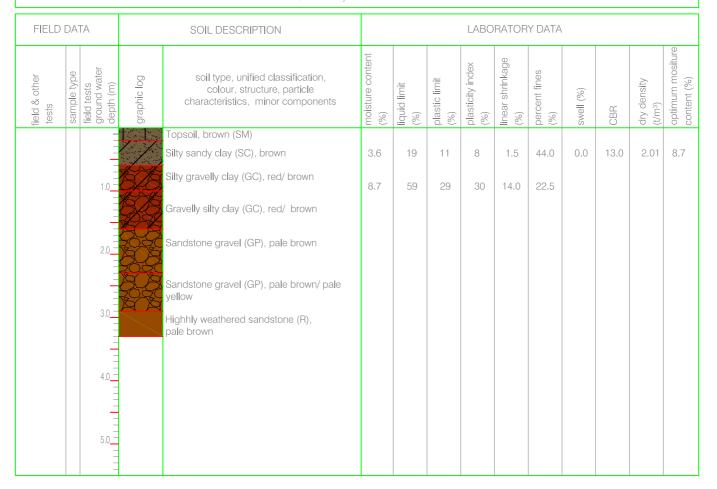
D = Dry M=Moist W=Wet

50-100

MD (medium dense) 10-30

D (dense)

VD (very dense)





■ Dynamic Cone Peneration

■ Pocket Penetrometer test

= Undisturbed Tube Sample

= Environmental Sample

Disturbed sample

| Bulk sample

DCP = Dynamic Cone Peneration (kPa)

GROUNDWATER ABBREVIATIONS

 \mathbf{Q} = Water level (during excavation)

PP = Pocket penetrometer (kPa)

Water level (static)

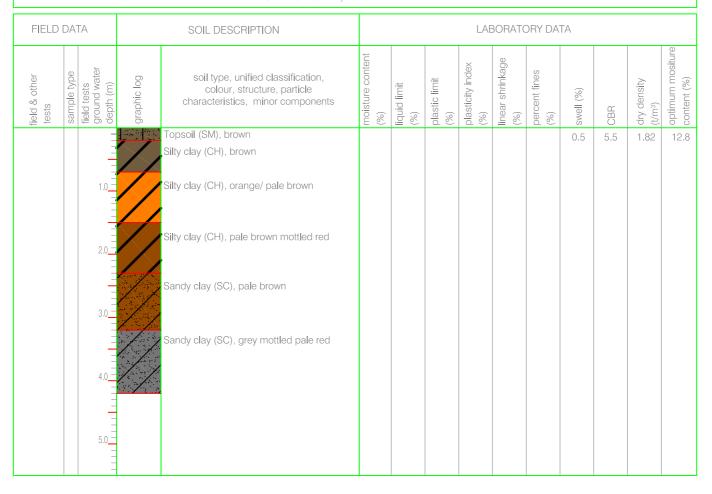
TEST PITS No: 3 & 4

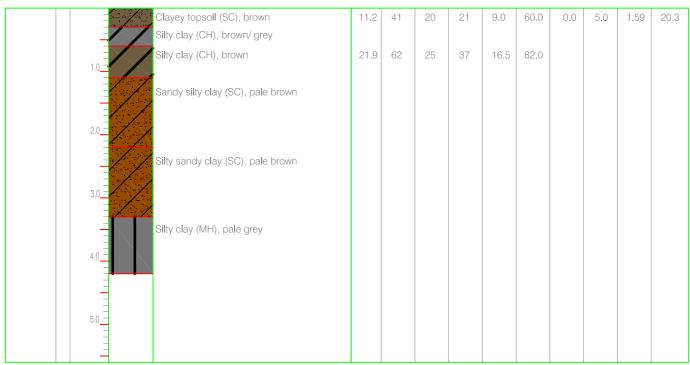
CLIENT: SWAN HILL ETHANOL Pty. Ltd LOCATION: CONDOBLIN JOB No.: 06-4479

METHOD: Test Pits- 22T Exacavator OPERATOR: John Boykett



LOG SHEET No: 2 OF 3





LEGEND

FIELD DATA ABREVIATIONS

DCP = Dynamic Cone Peneration (kPa)

PP = Pocket penetrometer (kPa)

Suv = Remoulded vane shear (kPa)

GROUNDWATER ABBREVIATIONS

■ = Water level (static)

□ = Water level (during excavation)

FIELD DATA SYMBOLS

▼ = Dynamic Cone Peneration

Undisturbed Tube SampleDisturbed sampleBulk sample

DENSITY (N-value)
VL (very loose) 0-4
L (loose) 4-10
MD (medium dense) 10-30
D (dense) 30-50
VD (very dense) 50-100
CO (compact) >50/150mm
MOISTURE CONDITION

D = Dry M=Moist W=Wet

CONSISTENCY (su)
VS (very soft) <12kPa
S (soft) 12-15
F (firm) 25-50
St (stiff) 50-100
VSt (very stiff) 100-200
H (hard) >200kPa

TEST PITS No: 5 & 6

CLIENT: SWAN HILL ETHANOL Pty. Ltd LOCATION: CONDOBLIN JOB No.: 06-4479

METHOD: Test Pits- 22T Exacavator OPERATOR: John Boykett



LOG SHEET No: 3 OF 3

S (soft)

F (firm)

St (stiff)

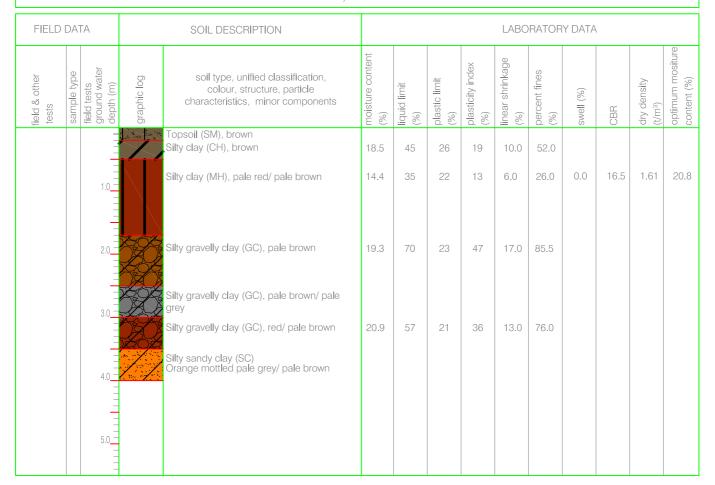
H (hard)

12-15

25-50

>200kPa

VSt (very stiff) 100-200





■ Pocket Penetrometer test

Undisturbed Tube Sample

/D (very dense)

50-100

MOISTURE CONDITION

D = Dry M=Moist W=Wet

>50/150mm

= Environmental Sample

= Disturbed sample

= Bulk sample

PP = Pocket penetrometer (kPa)

Water level (static)

Suv = Remoulded vane shear (kPa)

GROUNDWATER ABBREVIATIONS

SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289

TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report N° 06/4479 (Final)
	P.O Box 551	Page A8
	SWAN HILL	Date of Report: 11 Jan 2007
	Vic 3585	

LABORATORY INFORMATION

Project: Condoblin Ethanol Site

Sample Location: Condoblin

Date of Sampling: 12/12/06

SAMPLE IDENTIFICATION				
Laboratory Identification	Client Identification			
4479A	Pit 1 @ 200			
4479D	Pit 4 @ 300			
4479E	Pit 5 @ 700			
4479G	Pit 1 @ 1000			
4479H	Pit 4 @ 1100			
4479 I	Pit 5 @ 500			

	SAMPLE DESCRIPTION			
Laboratory Identification	Description			
4479A	Sandy clay/ red/ brown			
4479D	Sandy clay, brown			
4479E	Sandy clay, red/ brown			
4479G	Sandy clay with sandstone, red/ brown			
4479H	Sandy clay, red/ brown			
4479 I	Sandy clay & limestone pieces, red/ brown			

Approved Signatory: S.P.Pigdon

Date:11 January, 2006
Testing Laboratory: Bendigo



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MDF 3.02 Issue A Rev 0 July 06

SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289

TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report N° 06/4479 (Final)
	P.O Box 551	Page A9
	SWAN HILL	Date of Report: 11 Jan 2007
	Vic 3585	

LABORATORY INFORMATION

Project: Condoblin Ethanol Site

Sample Location: Condoblin

Date of Sampling: 12/12/06

SAMPLE IDENTIFICATION				
Client Identification				
Pit 5 @ 2500				
Pit 5 @ 3500				
*				
*				
*				
*				

SAMPLE DESCRIPTION			
Laboratory Identification	Description		
4479J	Silty clay, pale brown/ grey mottled white		
4479K	Silty clay, red/ brown/ grey		
*	*		
*	*		
*	*		
*	*		

Approved Signatory: ______ S.P.Pigdon

Date:11 January 2007

Testing Laboratory: Bendigo

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MDF 3.02 Issue A Rev 0 July 06

SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289 TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report N° 06/4479 (Final)		
	P.O Box 551	Page A10		
	SWAN HILL Vic 3585	Date of Report:	11 Jan 2007	

Sample Identification:	4479A	4479D	4479E	4479G	4479H	44791
Client Identification	Pit 1 @ 200	Pit 4 @ 300	Pit 5 @ 700	Pit 1 @ 1000	Pit 4 @ 1100	Pit 5 @ 500
Onent Identinication		Plasticity	_			
Liquid Limit %	19	41	35	59	62	46
Plastic Limit %	11	20	22	29	25	26
Plasticity Index %	8	21	13	30	37	19
Linear Shrinkage %	1.5	9.0	6.0	14.0	16.5	10.0
Preparation Method:	Oven dry	Oven dry	Oven dry	Oven dry	Oven dry	Oven dry
Shrinkage Mould Length:	254mm	254mm	254mm	254mm	254mm	254mm
Shrinkage Crumbling:	Yes	Yes	Yes	Yes	Yes	Yes
Shrinkage Curling:	Yes	Yes	Yes	Yes	Yes	Yes
Test Methods Used:	2.1.1		3.1.2	3.2.1 3.3.	1 3.4.1	
		Mechanical	Analysis			
Sieve Size (mm)			Percentage Pa	assing (%)		
200	*	*	*	100	*	*
75.0	*	*	*	80	*	*
63.0	*	*	*	59	*	*
37.5	*	*	*	53	*	*
26.5	*	*	*	52	*	*
19.0	*	*	*	49	*	*
13.2	100	*	*	46	*	100
9.5	99	*	*	42	*	99
6.7	98	*	*	38	*	98
4.75	97	*	100	35	*	98
2.36	95	100	98	31	100	97
1.18	91	98	89	29	97	95
600μm	82	95	73	28	95	90
425μm	76	91	61	27	93	87
300μm	70	87	51	26	92	83
212μm	*	*	*	*	*	*
150μm	60	75	35	24	87	70
75μm	44	60	26	22	82	52
Test Method Used	3.6.1					
		Field Moistur	e Content			
Lab ld:	4479A	4479D	4479E	4479G	4479H	4479 I
Moisture Content (%)	3.6	11.2	14.4	8.7	21.9	18.5
Test Method Used:	3.7.1	•	•		•	•

Approved Signatory: S.P.Pigdon

Date:11 January 2007 Testing Laboratory: Bendigo



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SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289 TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report N° 06/4479 (Final)
	P.O Box 551	Page A11
	SWAN HILL Vic 3585	Date of Report: 11 Jan 2007

						_
Sample Identification:	4479J	4479K	*	*	*	*
Client Identification	Pit 5 @	Pit 5 @	*	*	*	*
	2500	3500				
		Plasticity				
Liquid Limit %	70	57	*	*	*	*
Plastic Limit %	23	21	*	*	*	*
Plasticity Index %	47	36	*	*	*	*
Linear Shrinkage %	17.0	13.0	*	*	*	*
Preparation Method:	Oven dry	Oven dry	*	*	*	*
Shrinkage Mould Length:	254mm	254mm	*	*	*	*
Shrinkage Crumbling:	Yes	Yes	*	*	*	*
Shrinkage Curling:	Yes	Yes	*	*	*	*
Test Methods Used:	2.1.1		3.1.2	3.2.1 3.3.1	3.4.1	I
	•	Mechanical A	Analysis			
Sieve Size (mm)			Percentage Pa	assing (%)		
200	*	*	*	*	*	*
75.0	*	*	*	*	*	*
63.0	*	*	*	*	*	*
37.5	*	*	*	*	*	*
26.5	*	*	*	*	*	*
19.0	*	*	*	*	*	*
13.2	*	100	*	*	*	*
9.5	*	99	*	*	*	*
6.7	*	98	*	*	*	*
4.75	*	96	*	*	*	*
2.36	100	91	*	*	*	*
1.18	98	89	*	*	*	*
600μm	98	88	*	*	*	*
425μm	97	87	*	*	*	*
300μm	96	86	*	*	*	*
212µm	*	*	*	*	*	*
150µm	92	82	*	*	*	*
75μm	86	76	*	*	*	*
Test Method Used	3.6.1	1	1	I I		
	1	Field Moisture	Content			
Lab ld:	4479J	4479K	*	*	*	*
Moisture Content (%)	19.3	20.9	*	*	*	*
	3.7.1	1	1	i e		

Approved Signatory: S.P.Pigdon

Date:11 January 2007

Testing Laboratory: Bendigo



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MDF 3.02 Issue A Rev 0 July 06

SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289

TF	RI	FP	0	R ⁻	Г٠

Client:	Swan Hill Ethanol Pty Ltd	Report N° 06/4479 (Final)
	P.O Box 551	Page A12
	SWAN HILL	Date of Report: 11 Jan 2007
	Vic 3585	

LABORATORY INFORMATION

Project: Condoblin Ethanol Site

Sample Location: Condoblin

Date of Sampling: 12/12/06

SAMPLE IDENTIFICATION						
Laboratory Identification	Client Identification					
4479A	Pit 1 @ 200					
4479D	Pit 4 @ 300					
4479E	Pit 5 @ 700					
4479G	Pit 1 @ 1000					
4479H	Pit 4 @ 1100					
4479 I	Pit 5 @ 500					

SAMPLE DESCRIPTION					
Laboratory Identification	Description				
4479A	Sandy clay/ red/ brown				
4479D	Sandy clay, brown				
4479E	Sandy clay, red/ brown				
4479G	Sandy clay with sandstone, red/ brown				
4479H	Sandy clay, red/ brown				
4479 I	Sandy clay & limestone pieces, red/ brown				

Approved Signatory: S.P.Pigdon

Date:11 January 2007
Testing Laboratory: Bendigo



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SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289

TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report Nº 06/4479 (Final)	
	P.O Box 551	Page A13	
	SWAN HILL Vic 3585	Date of Report: 11 Jan 2007	

Sample Identification:	4479A	4479B	4479C	4479D
*Client Identification:	Pit 1 @ 200	Pit 2 @ 500	Pit 3 @ 200	Pit 4 @ 300

Test Results								
Date of Test:	22/12/06	22/12/06	22/12/06	22/12/06				
Laboratory Density Ratio:	98.0	97.0	98.5	98.0				
Laboratory Moisture Ratio:	97.5	102.5	97.5	102.5				
Moisture Content Top 30mm:	11.1	29.8	17.6	23.0				
Compaction Type:	Standard	Standard	Standard	Standard				
Number of Layers:	3	3	3	3				
% Material retained 19.0mm sieve:	0	0	0	0				
Material crushed & reused:	NA	NA	NA	NA				
Mass of Surcharge:g	5542.5	5500.8	5523.4	5491.4				

Soaked sample Information							
Period of Soaking (days)	4	4	4	4			
Dry Density After Soaking: t/m ³	1.96	1.47	1.78	1.55			
Moisture Content After Soaking: %	10.7	27.2	15.6	22.6			
Swell: %	0.0	0.5	0.5	0.0			

Maximum dry density / Optimum moisture content				
Maximum dry density: t/m ³	2.01	1.53	1.82	1.59
Optimum moisture content: %	8.7	24.6	12.8	20.4

Penetration Depth of C.B.R Determination:	13.0	11.0	5.0	4.0
5.0mm				
CALIFORNIA BEARING RATIO:				

Test Methods Used: 2.1.1 5.1.1 6.1.1

Date:11 January 2007

Testing Laboratory: Bendigo



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SOIL PROPERTIES- sampled by Laboratory Staff Testing in Accordance with AS1289

TEST REPORT:

Client:	Swan Hill Ethanol Pty Ltd	Report Nº 06	/4479 (Final)
	P.O Box 551	Page A14	
	SWAN HILL Vic 3585	Date of Report:	11 Jan 2007

Sample Identification:	4479E	4479*F	*	*
*Client Identification:	Pit 5 @ 700	Pit 6 @ 200		

Test Results					
Date of Test:	22/12/06	22/12/06	*	*	
Laboratory Density Ratio:	98.5	98.0	*	*	
Laboratory Moisture Ratio:	aboratory Moisture Ratio: 97.0 100.0		*	*	
Moisture Content Top 30mm:	23.0	23.0 13.1 *		*	
Compaction Type:	Type: Standard Standard		*	*	
Number of Layers:	of Layers: 3 3		*	*	
% Material retained 19.0mm sieve:	0	0	*	*	
Material crushed & reused:	NA	NA	*	*	
Mass of Surcharge:g	5526.0	5502.7	*	*	

Soaked sample Information				
Period of Soaking (days)	4	4	*	*
Dry Density After Soaking: t/m³	1.59	1.90	*	*
Moisture Content After Soaking: %	22.5	12.7	*	*
Swell: %	0.0	0.0	*	*

Maximum dry density / Optimum moisture content				
Maximum dry density: t/m ³	1.61	1.94	*	*
Optimum moisture content: %	120.8	10.6	*	*

Penetration Depth of C.B.R Determination:	16.0	8.0	*	*
5.0mm				
CALIFORNIA BEARING RATIO:				

Test Methods Used: 2.1.1 5.1.1 6.1.1

Date:11 January 2007

Testing Laboratory: Bendigo

ratory: Bendigo



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Client: **Geotechnical Testing Services**

PO Box 555 Address:

GOLDEN SQUARE VIC 3555

Certificate of Analysis Batch No: 07-00422

Replacement Report

Attention: Scott Pigdon Report Number: 2313

Page 1 of 3 This report replaces Report Number: 1794 Date Issued: 20-Feb-2007

Client Program Ref: 06/4479 Condoblin PO No: Not Available Date Sampled: 12-Dec-2006

Ecowise Program Ref: 22347

The sample(s) referred to in this report were analysed by the following method(s):						
Analysis	Method	Laboratory	Analysis	Method	Laboratory	
CEC	WSL 068	Melbourne	EC	WSL 063	Melbourne	
Exch. Cations	WSL 023A	Melbourne	OOC	WSL 064	Melbourne	
рН	WSL 062	Melbourne				



Ecowise Environmental Gate 6 Sharon Street, La Trobe University, Bendigo, VIC

Tel: 03 5444 7890 Fax: 03 5444 7895

Client sample reference 4479H had insufficient sample for Organic Carbon analysis.

Date Received: 19-Jan-2007

The units for CEC are meq/100 gm.

Principal Contact for this Report:

WK Woodall.

Wavne Woodall



The results in this report were authorised by:

Name Title

John Levvey **Principal Trace Metals Chemist**

Samantha Smith **Client Manager** Vic Willms **Manager Chemistry**

Process Co-ordinator

Batch No: 07-00422

Report Number: 2313

Client Program Ref: 06/4479 Condoblin

Client: Geotechnical Testing Services

Ecowise Program Ref: 22347



Date Issued: 20-Feb-2007

Soil Analysis	Analysis:	рН	EC	000	CEC
Soil Analysis Sample Sampled Date	Your Ref Component.	pH Units	EC uS/cm	Ox Org C %	CEC -
1106554 12-12-06 4	479 A	7.6	8	1.0	18
1106555 12-12-06 4	479 D	7.4	200	1.0	27
1106556 12-12-06 4	479 E	7.8	750	1.2	25
1106557 12-12-06 4	479 G	8.2	470	0.8	0.19
1106558 12-12-06 4	479 H	8.3	1300		20
1106559 12-12-06 4	479 I	7.9	140	0.8	22
1106560 12-12-06 4	479 J	8.8	260	0.5	19
1106561 12-12-06 4	479 K	9.3	280	0.9	23
1106562 12-12-06 4	479 TP1	7.9	5	1.2	9.2
1106563 12-12-06 4	479 TP3	7.7	5	1.3	15
1106564 12-12-06 4	479 TP5	7.6	6	1.2	20

Soil Me	etals - O	ES	Analysis:	Exch. Cations
CON MICICIO - CEO		Component:	Ex-Na	
Sample	Sampled Da	ate Your Ref	Units:	mg/kg
1106554	12-12-06	4479 A		95
1106555	12-12-06	4479 D		2100
1106556	12-12-06	4479 E		1500
1106557	12-12-06	4479 G		780
1106558	12-12-06	4479 H		3000
1106559	12-12-06	4479 I		650
1106560	12-12-06	4479 J		2700
1106561	12-12-06	4479 K		2700
1106562	12-12-06	4479 TP1		47
1106563	12-12-06	4479 TP3		200
1106564	12-12-06	4479 TP5		380



Quality Control

Soil Metals - OES	Exch. Cations
con motalic CEC	Ex-Na
1107390 BLANK Value (mg/kg)	1.2
1107391 DUPLICATE Sample Value (mg/kg)	920
1107391 DUPLICATE Duplicate Value (mg/kg)	920
1107391 DUPLICATE % RPD (%)	0.9
1107392 DUPLICATE Sample Value (mg/kg)	630
1107392 DUPLICATE Duplicate Value (mg/kg)	640
1107392 DUPLICATE % RPD (%)	0.8
1107393 DUPLICATE Sample Value (mg/kg)	52
1107393 DUPLICATE Duplicate Value (mg/kg)	53
1107393 DUPLICATE % RPD (%)	1.4

Soil Analysis		pН	000	CEC	
		pH	Ox Org C	CEC	
					32
					34
1108383	DUPLICATE	% RPD (%)			6.8
					25
					45
1108385	SPIKE	% Recovery (%)			84.8
					22
					42
1108386	SPIKE	% Recovery (%)			82.3
					20
					20
1108387	DUPLICATE	% RPD (%)			0.9
1108890	DUPLICATE	Sample Value (%)		1.1	
1108890	DUPLICATE	Duplicate Value (%)		1.0	
1108890	DUPLICATE	% RPD (%)		9.5	
1108891	DUPLICATE	Sample Value (%)		1.2	
1108891	DUPLICATE	Duplicate Value (%)		1.1	
1108891	DUPLICATE	% RPD (%)		8.7	
1109184	DUPLICATE	Sample Value (Units)	7.9		
1109184	DUPLICATE	Duplicate Value (Units)	7.9		
1109184	DUPLICATE	% RPD (%)	0.0		

Batch No: 07-00422

Report Number: 2313