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REPORT

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CRONULLA SUTHERLAND LEAGUES CLUB LIMITED

ON

GEOTECHNICAL INVESTIGATION

FOR

PROPOSED CRONULLA LEAGUES CLUB REZONING

AT

CAPTAIN COOK DRIVE, WOOLOOWARE, NSW

27 September 2002

Ref: 17119SPrpt

ENVIRONMENTAL INVESTIGATION SERVICES, FOUNDATION AND SLOPE STABILITY INVESTIGATIONS, ENGINEERING GEOLOGY, PAVEMENT DESIGN, EXPERT WITNESS REPORTS, DRILLING SERVICES, EARTHWORKS COMPACTION CONTROL, MATERIALS TESTING, ASPHALTIC CONCRETE TESTING, QA AND QC TESTING, AUDITING AND CERTIFICATION. N.A.T.A. REGISTERED LABORATORIES





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FIGURE 1: INVESTIGATION LOCATION PLAN

APPENDIX A: LOGS OF GEOTECHNICAL INFORMATION AVAILABLE FROM INVESTIGATIONS

EXPLANATORY NOTES

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<u>1</u> INTRODUCTION

This report presents the results of the review of previous geotechnical investigations at Shark Park, Woolooware, NSW. The investigation was commissioned by Mr Andrew Durbidge of BDO Property Pty Ltd on behalf of Cronulla Sutherland Leagues Club Ltd in a letter dated 4 September 2002.

We understand that it is proposed to rezone the property to the north, east and south of the existing Club. The rezoning is to allow the construction of:

- a double basement car park over the majority of the site area, requiring excavation to a level of about 0.3m AHD (a depth of about 3m to 3.5m);
- a two storey extension to the south of the existing club;
- a three storey hotel facility to the east of the proposed club extension;
- five buildings of three to five levels comprising residential units and aged care facilities to the north and north-east of the existing club;
- the placement of the existing high voltage power lines to the north of the site underground.

There could also be future extensions to the western grandstand of Shark Park, and a future vehicle drop-off zone at the southern side of Shark Park, however we understand that these are not part of the current rezoning application.

The purpose of the review was to compile the available geotechnical information on subsurface conditions, and to use this to provide comments and recommendations on earthworks, excavation, shoring, retaining wall design, construction techniques, footing design, and discussion of the effects of potential dewatering.

A review of the available environmental site screening information was completed in conjunction with this investigation by Environmental Investigation Services (EIS), a division of Jeffery & Katauskas Pty Ltd. The results of the site screening are Ref: 17119SPrpt

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presented in the report E17119FK dated October 2002; the report should be reviewed in conjunction with this report.

2 EXISTING INFORMATION

Jeffery and Katauskas Pty Ltd have completed eight previous investigations within the proposed redevelopment area. A summary of these investigations is provided below.

- Reference 581 dated 27 July 1978 for a proposed grandstand the investigation comprised 2 augered boreholes drilled into the underlying sandstone.
- Reference 7391S dated 6 April 1990 for an unspecified proposed development the investigation comprised 2 boreholes cored into the sandstone bedrock, one borehole augered to 10 metres (m) depth, and 7 Electric Friction Cone Penetration (EFCP) Tests to 5m to 11m depth.
- Reference 8309K dated 25 July 1991 for a proposed amenities block the investigation comprised drilling three augered boreholes to depths ranging from 3.8m to 4.8m below existing ground levels.
- Reference 11630SV dated 1 February 1996 for the proposed southern stand the investigation comprised 7 augered boreholes to depths between 1.3m and 6.0m below existing ground levels.
- Reference 12308SV dated 24 January 1997 for proposed club extensions the investigation comprised 2 boreholes augered into the underlying sandstone and three boreholes augered to between 4.8m and 6.0m below the existing ground levels.
- Reference 12765SV dated 2 September 1997 for proposed extensions to the club - the investigation comprised the coring of 2 boreholes into the sandstone bedrock, the augering of 2 boreholes into the bedrock and augering 2 boreholes to 6.7m and 7.0m depth.

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 Reference 1.5009JTP dated 17 April 2000 for proposed redevelopment of the Shark Park area - the investigation comprised eight EFCP tests to refusal of the equipment (depths between 5.8m and 20.6m).

Several of the reports referred to obstructions and voids within the fill, and that metal, bricks and concrete were often encountered.

Copies of the borehole logs and EFCP test results are provided in Appendix A. The approximate locations of these tests are shown on the attached Figure 1; the locations have been scaled from the plans contained in the previous reports and so the plotted locations could be in error by about 10m or so. It should also be noted that these depths were from existing ground level at the time of the fieldwork for those investigations and depths may have subsequently changed following excavations or the placement of additional fill.

In addition to the above information, 12 boreholes have been auger drilled during the recent environmental investigation to obtain samples for acid sulphate soils assessment to depths of 6.0m below existing ground levels. The borehole logs from this recent investigation are also provided in Appendix A and the information has been used in compiling this report.

3 INVESTIGATION PROCEDURE

Generally the boreholes have been completed by auger drilling with a truck mounted drilling rig with the soil strength being assessed from the recorded Standard Penetration Tests. The sandstone bedrock, when encountered, was either augered with a tungsten carbide drilling bit (in which case the rock strength was assessed from observation of the auger drilling resistance and from examination of the rock cuttings recovered from the base of the augers) or diamond cored (where the



strength was assessed from examination of the recovered core and from Point Load Strength Index tests completed on the core).

The EFCP tests were completed with a purpose built truck mounted friction cone rig. The inferred strata and soil strengths shown on the EFCP traces have been assessed from correlations of the data with published charts and so the interpreted data is approximate only. The refusal depths are often assumed to be the top of bedrock and there seems to be reasonable correlation between the rock depths encountered in the boreholes and the inferred depths from the EFCP tests.

4 RESULTS OF THE INVESTIGATIONS

4.1 Site Description

The site is located to the north of Captain Cook Drive, Woolooware. The site is generally flat with a slight slope (less than 1°) down to the north. The regional topography falls gently toward the bay to the north apart from the golf course to the south of Captain Cook Drive that is generally at a lower level than the site.

A large multistorey brick building used as the leagues club is located within the central section of the site; this appeared to be in good external condition from a brief inspection of the exterior.

The main football ground was to the west of the club and there was a large multistorey grandstand at the west side of the field. At the north and south ends of the field are landscaped mounds (approximately 4m and 2m respectively above the general site level) used as spectator viewing areas. To the west of the large stand are several single storey concrete and brick buildings used as a gymnasium, amenities block and media facilities.



A drainage channel crosses the site from south to north at the west of these buildings. Mangroves line this channel and the water level was approximately 1m to 1.5m below the general site level at the time of inspection.

Two football fields are located on the far side of the main football ground with asphaltic concrete car parking on the southern side of the fields.

To the east and north of the Leagues Club is a second asphaltic concrete paved car park used by the Leagues Club. This area slopes at approximately 1° to the north with the southernmost portion gently sloping at approximately 1° to the south (toward the Captain Cook Drive boundary).

There is vacant land and mangrove swamps to the east of the site. Captain Cook Drive and then Woolooware Golf Course were located to the south. Solander Playing Fields and then industrial land lies to the west. An easement for transmission lines and then Woolooware Bay lie to the north.

4.2 Subsurface Conditions

In general terms, the testing on the site has disclosed poorly compacted fill over soft and very soft bay deposits of organic silty clays over stiff to very stiff clayey soils and medium dense to very dense sandy soils. Sandstone or inferred sandstone bedrock was encountered at depths ranging from 7.7m to 13.3m below existing ground level in the proposed works area while the sandstone to the west of the existing clubhouse extends considerably deeper (as deep as 20.6m).

Within the proposed works area, the fill had a thickness between 2.2m and 4.5m. The fill was often logged as silty sand and sandy clay with varying proportions of metal, timber, sandstone and demolition rubble. The fill was assessed as being poorly compacted.



The organic clays with some areas of clayey silty sand were encountered from the base of the fill at depths between 2.2m and 4.5m. These were generally of very soft to soft strength and had thicknesses of about 2.0m to 3.0m, though the thickness was limited to about 1.0m at some of the test locations.

Silty clays of at least stiff strength (and usually of very stiff strength) and sands generally of medium dense relative density were encountered below depths of 5 to 6m.

The sandstone bedrock (or inferred bedrock) was encountered at depths ranging from 5.6m to 20.6m below existing ground level. In the vicinity of the existing club, a sandstone capping layer was often encountered, this sandstone was generally about 0.5m to 1.0m thick and was overlying further clay bands which had thicknesses of 0.9m to 4.2m. Shallow refusal (5.8m and 5.6m) was encountered at location 803, and at a retest (numbered 803a) which was completed within 1.0m of the original test; this refusal may have been on sandstone bedrock, though this cannot be confirmed. The bedrock depths and inferred bedrock depths at the test locations are shown on the attached Figure 1.

Groundwater was encountered at depths between 0.4m and 3.8m during previous investigations. No long term groundwater monitoring has been undertaken during any of the investigations.

4.3 Site Anomalies And Construction Difficulties

There are several difficulties associated with the development at this site. These include:

• The presence of the deep, poorly compacted fill providing potentially poor trafficability, poor foundation conditions and poor pavement subgrade.



- The presence of obstructions and voids in the fill resulting in difficult piling conditions and the use of excess grout in auger grout injected piles.
- Methane has been encountered during investigations by EIS. This will require the adoption of a methane drainage blanket and extraction system below proposed structures and pavements. Other gases often found with methane are corrosive and hence copper pipes would not be recommended for underground services.
- The very soft and soft organic clay layer which will undergo additional consolidation settlements if additional load is placed above this layer. This could also give rise to negative skin friction effects on piles if the organic clay consolidates.
- The organic clays were found during the recent investigation by EIS to have an acid sulphate generation potential. As a result, if these soils are disturbed by excavation or are removed during pile construction, treatment of the soil for potential acid generation will be required. Reference should be made to the EIS report for details on acid sulphate management.
- The relatively high groundwater which will make earthworks such as replacement of fill, proof rolling and additional fill compaction difficult. This may require dewatering or the adoption of bridging layers necessary.
- The generally deep sandstone bedrock which will require long piled footings to be adopted.
- The capping layer of sandstone on which many piling systems could refuse. Very limited bearing pressures would have to be adopted if the piling cannot penetrate to the more competent sandstone bedrock at depth.

Although the above are potential problems for the construction of the proposed development at the site, the construction nevertheless appears feasible. These difficulties on the site require that good planning, design and construction techniques are used.



5 COMMENTS AND RECOMMENDATIONS

The geotechnical information available for the site is from numerous previous investigations. Further investigation for the proposed development will be useful in some areas to confirm target founding depths and allowable bearing pressures.

5.1 General Earthworks Comments

Excavation

Excavation will be required for the basement construction and the installation of underground services, including placing the existing high voltage power lines to the north of the site underground. We expect that the excavation will be limited to about 3m to 3.5m below excavation level.

The excavated material will be a combination of existing fill and natural organic soils. Reference should be made to the EIS report for details of the waste classification for these materials, and for any necessary treatment prior to disposal.

Excavations through the soils above the water table should be temporarily battered at no steeper than 1 Vertical (V) in 1.5 Horizontal (H). Where these excavations will extend below the water table, it will be necessary to dewater so that the excavation will be in "dry" soil which will require shoring of the sides of the excavation. We understand that the acid-sulphate reactivity of the soil will necessitate quite stringent controls on dewatering and so the construction of a sheet pile wall around the excavation will probably be required. Sheet pile walls may be designed using active and passive earth pressure coefficients and unit weights as provided in the table below. Appropriate surcharge loads and hydrostatic pressures (taking into account the dewatered condition) would have to be included in the design of the shoring.



Soil Description	Total Unit Weight (kN/m³)	Active Earth Pressure Coefficient (K₃)	Passive Earth Pressure Coefficient (K _P)
Fill	19	0.35	3.0
Peat, Organic Clay, Organic Sand	10	0.50	2.0
Remaining Clayey and Sandy Soil	20	0.3	3.3

There would be two options with regard to the sheet pile walls. The first of these would be to cantilever the walls, though the lateral deflections may not be tolerable where near existing structures (such as the club building and the service station to the east). To limit the deflections, the second option would be to use embedment for toe restraint of the sheet piles in conjunction with an upper row of anchors or tie backs. The anchors could be soil anchors of either the grouted type (conventional anchors) or buried plate type (such as 'Platypus' anchors). Grouted anchors should be designed for a friction angle of 25° provided they are bonded into the fill and all anchors should be proof loaded to at least 1.3 times their working load.

Engineered Fill

A basement will extend over the majority of the site area, and so very little fill will be placed during the construction. The fill is likely to be below entry pavements (where suitable placement procedures are often detailed during the construction works as they have relatively little effect on the proposed construction) and in landscaping areas where only nominal compaction is required unless there will be additional pavements or structures in those areas.



Any new structural fill placed, such as below proposed pavements, should be placed as engineered fill. Such fill should preferably be a well graded, select granular fill containing no organics or other deleterious substances. The fill should be placed in layers not exceeding 200mm loose thickness and compacted to at least 98% of Standard Maximum Dry Density (SMDD). Clayey fill is not ideal for use, though it may be used following approval of the material by the geotechnical engineers, and it should be compacted strictly to between 98% and 102% of SMDD and within 2% of the Standard Optimum Moisture Content (SOMC).

Where fill is being placed in landscaped areas, or below areas which will be supported on piles, it should be compacted to at least 95% of SMDD.

5.2 Footing Design

The existing fill and organic clays on the site are not suitable for use as a bearing stratum for the proposed structures. We recommend that the proposed buildings be supported on piles founded on the sandstone bedrock. From the limited information available at present, we consider that piles founded within the bedrock of at least medium strength may be designed for an allowable end bearing pressure of 3500kPa. In many areas of the site, further investigations would be likely to prove bearing pressures to 6000kPa as being feasible. It should be noted however that in some areas, particularly around the existing club building, a capping layer of sandstone was found to overlie further clay bands; the piles would need to penetrate through these to the sandstone bedrock below to adopt the higher pressures. Allowable bearing pressures of about 600kPa appear to be feasible on the sandstone capping layer. Further information will be required at each of the building locations to provide further information on the variability so that the above allowable bearing pressures can be confirmed.

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Provided the above pressures are adopted, we expect settlements would be less than 1% of the pile diameter (ie settlements probably less than 10mm).

Where piles would only need to support relatively light loads, it may be possible to support them within the stiff to very stiff clayey soils. Such piles may be designed for an allowable end bearing pressure of 300 kPa. Any socket into the stiff to very stiff clay greater than 0.5m in length may be designed for an allowable shaft adhesion of 17kPa.

There are several piling techniques that may be adopted at this site and these are discussed in more detail below.

It would be possible to use driven steel or concrete piles on the site. In this case, there would be no spoil which would require treatment for potential acid sulphate problems. Driven piles also have the benefit that their load capacity can be calculated using published pile driving formulae. We expect that vibrations from the pile driving would not be of concern in the majority of the proposed development area, however this should be confirmed by reputable pile driving companies prior to the adoption of this piling system. One potential drawback of this system is that the piles may refuse on the capping layer of sandstone and so the pile capacity may be relatively low. Pre-drilling could be considered to overcome this but would add substantially to the cost.

An alternative to the driven piles would be the 'G pile' system. This technique involves jacking the piles into the ground from a very large ballasted rig. The load capacity of these piles can also be calculated from the piling records. These piles have the advantage over driven piles that there is very little vibration from the pile installation and so can be used close to existing structures. These piles also have the potential problem that premature refusal may occur on a capping layer of sandstone resulting in limited pile capacity, again, pre-drilling is an option.

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Auger grout injected piles would also be a possibility on this site. These would be particularly useful around the club where the depths to the rock are generally less than say 15m. More difficulty could be encountered however to the west of Shark Park where the rock was in excess of 20m. These piles have the benefit that they can be drilled to depth and therefore should have the capacity to drill through capping layers of sandstone, though drilling in sandstone is usually very slow and large volumes of excavated spoil are likely to be produced. We understand that this piling system has previously been used on the site and large volumes of grout were required, presumably to fill voids within the poorly compacted fill.

It may also be possible to drill piles using bentonite mud to support the hole during drilling and concreting. A variation to this would be to adopt barettes excavated through a bentonite slurry using a 'clamshell' mechanism (similar to that used for diaphragm wall construction). These drilling techniques are usually very expensive and are only likely to be economical if the column loads are very high.

Conventional bored piles are not considered suitable at this site due to the high groundwater level and the potential for collapse of the poor quality near surface soils.

Our recommended piling techniques would be to adopt either auger grout injected piles or piles drilled through bentonite slurry everywhere on the site, or a combination of driven piles when at a distance from existing structures (and where investigation shows there is no capping layer of sandstone) and auger grout injected piles elsewhere.

We note that obstructions within the fill have been previously noted and all of the above techniques could have difficulties with these. We therefore recommend that a low productivity and increased bit wear be allowed for in the tendering of piling.



Also, a provisional sum could be allowed for the possibility of having to excavate obstructions from the fill where premature refusal of the piling occurs.

5.3 Temporary And Permanent Groundwater Considerations

Some of the soils around the site have the potential to produce acidic leachate if they become unsaturated and oxygen is allowed to react with the soil. As a result, the level of groundwater will need to be carefully monitored and controlled during the construction period.

Dewatering of the basement excavation will be required with the currently proposed level of the basement. To reduce the effects of dewatering on the groundwater conditions outside the excavation, it will be necessary to have a 'cut-off' wall, such as a sheet pile wall, around the basement. This cut-off should be socketed below the base of the excavation such that the depth of embedment below the proposed excavation level is twice the distance between the basement level and the outside water level.

As the soils are generally likely to be of low permeability within the dewatering zone, conventional well or spearpoint dewatering systems are probably not generally suitable, though may be necessary in some areas. We suggest that the dewatering be trialed using a sump and pump technique. The sump could be formed by having large diameter drums or 'formatube' with many small holes in them installed into holes excavated below the base of the excavation. The void between the 'sump' and the excavated hole could then be filled with clean fine gravel and/or coarse sand as a filter. An automated pump system could then be installed in the sump. Reference should be made to the EIS report with regard to testing, treatment and disposal of the collected water.



It will then be necessary to have monitoring wells around the perimeter of the excavation to assess the effect of dewatering outside the cut-off wall; we would expect this effect to be very minor. If there is any drawdown of the groundwater outside the cut off, an injection system could be used to overcome the drawdown effect. The injected fluid could be:

- Water pumped from the sumps, treated as necessary;
- Water from the Bay;
- Water pumped from a deep well, at such depth that the water level near the surface will not be affected;
- Town water.

Appropriate injection of water would prevent drawdown of the water level in the short term. Any other environmental effects of using these waters, in relation to the injection of salt or chlorine is beyond our area of expertise but will need to be addressed by others.

Following the completion of the basement construction, the sheet piles should be removed to reduce their effect on the long-term groundwater flows. Following the sheet pile removal, the basement will extend only slightly below the water table. The majority of the soil between the water table and the bedrock will be left in place. There are also large areas along the foreshore where there will be no development intersecting the groundwater table. As a result, we would not expect there to be any significant effect on the long-term groundwater regime.

Further reduction of risk associated with changes to the groundwater regime could be achieved using a drainage and reinjection system. Such a system could comprise a subsoil drain directly above the existing groundwater level on the road side of the proposed basement, and by connecting this via a pipe and gravity drainage to a rubble soak away system above the current groundwater level on the Bay side of the proposed basement. We do not expect that such a system would be required.



5.4 Methane Drainage

We understand from EIS that there is a methane generation problem at the site and that a methane drainage system will be required. Such a system could comprise a drainage blanket of the entire development area, though we expect that this would be very expensive. Another alternative could be to complete the basement excavation and footing installation (piling), and excavate drainage slots, wrapped in filter geotextile and filled with clean, free draining, durable gravel and slotted PVC pipe. Following backfilling of these trench drains, a layer of 'bentofix' or 'claymax' should be placed over the entire site area and wrapped up the outside of retaining walls constructed inside the shored basement. This will provide a 'seal' to prevent the methane from entering the structures. For further details of the methane collection and disposal, reference should be made to the abovementioned EIS report.

5.5 Basement Design

The proposed two level car parking basement will extend slightly below the groundwater table. It will therefore be necessary to waterproof the basement to at least the highest foreseeable groundwater level. If more detailed information cannot be found, we recommend that allowance for hydrostatic pressures be made. A detailed study of local factors will be required to arrive at a realistic maximum level. The seal for the methane drainage will assist with the waterproofing of the basement, though we note that these products are of low permeability, not impermeable. We therefore recommend that the basement floor be designed to supply the waterproofing.

We note that the construction of the basement below the water table will either require dewatering, or hold down anchors, possibly of steel screw pile type, until there is sufficient load from the structures to withstand the potential uplift forces.

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As the subgrade below the basement floor will be organic and wet, it will not be possible to prepare the subgrade to construct slab on grade. We therefore recommend that the basement floor be designed as suspended from the piles. This may not require any thicker floor as the basement floor will have to be designed for hydrostatic uplift pressures anyway.

6 FURTHER INVESTIGATIONS

As mentioned above, the current investigations have provided information on inferred rock depth or rock depth and quality at relatively large centres. Further investigation will therefore be required to provide specific comments and recommendations for developments of specific areas.

7 GENERAL COMMENTS

Occasionally, the subsurface soil conditions between the completed boreholes and EFCP test locations may be found to be different (or may be interpreted to be different) from those inferred/expected. Variation can also occur with groundwater conditions, especially after climatic changes. If such differences appear to exist, we recommend that you immediately contact this office.

This report provides advice on geotechnical aspects of proposed civil and structural design. As part of the documentation stage of this project, Contract Documents and Specifications may be prepared based on our report. However, there may be design features we are not aware of or have not commented on for a variety of reasons. The designers should satisfy themselves that all the necessary advice has been obtained. If required, we could be commissioned to review the geotechnical aspects of contract documents to confirm the intent of our recommendations has been correctly implemented.

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The offsite disposal of soil may require classification in accordance with the EPA guidelines as inert, solid, industrial or hazardous waste. We can complete the necessary classification and testing if you wish to commission us. As testing requires about seven days to complete, allowance should be made for such testing in the construction program unless testing is completed prior to construction. If contamination is found to be present then substantial further testing and delays should be expected.

Should you have any queries regarding this report, please do not hesitate to contact the undersigned.

ो∽ P Wright Associate

P Stubbs Director For and on behalf of JEFFERY AND KATAUSKAS PTY LTD







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APPENDIX A

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FIELD LOG

Location No. BH1 1/2

Job No Date:	0: 15009. 24\$25.7	17P • 78	l	Metho	d: Aliger & WashBore		R.L. Datu			ce: NT
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FIELD LOG

CRONLILLA SHARKS Client: Project: SHARK PARK REDEVELOPMENT Location: CAPTAIN COOK DRIVE, WOOLOOWARE. R.L. Surface: NT Method: ALGER & WASHBORE 15009-JTP Job No: Datum: N. J Date: 24\$25.7.78 Consistency/ Rel. Density ò Log Ļ Moisture Condition Hand Peneti meter Structure (m,) Samples Unified Classif. ĸ and Soil Description Water Graphic Geology Field Level Depth Tests 1234 15 as above CH 16 17 SANDU CLAU CL 18 moded brownand SICH, Some dark /9 gres with dep th 20 SANDSTONE 21 END BOREHOLE 21.0m.

BH1

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FIELD LOG

				Annual Plate State			
Client: <i>CRONUL</i> Project: <i>SHARK</i> Location: <i>CAPTAN</i>	DADK	REDEV	ELOPMENT				
Job No: <i>15009.11</i> Date: 24425.7.	TP		d: ALGER & WASHBORE		Datu	Surfa m: N.7	ce: NT
Samples Water and Level Field Tests	Depth (m.) Graphic Log	Unified Classif.	Soil Description	Moisture Condition	Consistency/ Rel. Density	Hand Penetro Meter	Structure & Geology
(4,6,10)	15 16	C.H	CLAS as above	MINA.	544		
(3. 3. 4)	17		SANDY CLAY MEChum Dlashaly Methed grey and Servasen	MAR.	Shift		
	20	4	SANDSTONE				
			END BOREHOLE 2040	2			

Location No

2/2

.

CONSULTING GEOTECHNICAL ENGINEERS

1/4

BOREHOLE LOG



4.0

Borehole No.

101

Jeffery and Katauskas Pty Ltd consulting geotechnical engineers

BOREHOLE LOG

Borehole No.

101 _____2/4_

Loca	ect: _ ation:	LAPTAI.	PAR N Li	K REL	DEVI DRI I	ELOPMENT VE WOOLOOWARE. d: SPIRAL AUGER		3733(71400)(8410)(8410) 		
Job Date		15009.11 26 - 2 - 90		יו	- -	EDSON 3000				
Groundwater record	Samples	Field Tests	JDepth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand To Penetrometer PReadings	Remarks
FULL					<u>C</u> H	SAND: as above <u>grading to</u> SANDY CLAY: high	MC >PL	V. 5t H		1/2 m. CAVE-IN - CASED TO 7.5 m.
RETUR	v Д5	N= 17 3, 7, 10	8-			plasticity light grey, occasional arange brown veins, with occasional bands of clayey sand.			270 430 390	- COMMENCED MUD DRILLING -
			9-				7	· .		-
					:L- <i>CH</i>	SANDY CLAY: medium to high plasticity, light grey, occosional pockets of red brown very				-
	DS	N=12 3, 5, 7				sandy clay.			250 200 350 410 280	- -
			12 -							
¥4 RETURN			13 -			but with accosional ironstone bands.	MC>PL	_51 V. 51.		- FLUSH LOSS IN IRONSTONE BANDS
FULL RETURN	צם י	N=14 4, 6, 8							70 20 40 260 240	-

Jeffery and Katauskas Pty Ltd CONSULTING GEOTECHNICAL ENGINEERS

BOREHOLE LOG

Borehole No.

101 3/4

		ect: _		PAR	k RE	DEVI	Elopment Ve Wooldoware.	97979979797979797979797979797979797979	97-200 Data (94), 19, 200 P	<u>an na shakara ka</u>	
, ,		No	15009.JT 26 - 2 - 90	-p			d: SPIRAL AUGER EDSON 3000				
Groundwater	record	Samples	Field Tests	Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Preadings	Remarks
	~	يدن	Ľ				SANDY CLAY: OS OBOVE	MC 7 PL	51.		
		DS	N = 9 3, 5, 4	15 - -						140 200 130 140	-
				16 -							-
	-			- 17	<u>. 7. 1</u>		REFER TO CORED B.H. LOG				ATTEMPTED SPT 15 BLOWS / Omm.
				-							- -
	,		1	-	- - -						-
				- - - -							-
											-
СОРУВІСНТ					-			and the second	agagyaaa yaan ahaa ahaa ahaa ahaa ahaa ahaa		

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j:

CORED BOREHOLE LOG

Borehole No.

101 4/4

P	lient roje ocat	ct:	SHI	NULLA SHARKS ARK PARK REDEVELOP. TAIN COOK DRIVE, WO	ME OLC	N.	T V	VARE.		
)ate	Drille	d: <i>268</i>	Core Size: 27-2-90 Inclination SON 3000 Bearing:			~~	1. L. C.		
vel								POINT		DEFECT DETAILS
Water Loss/Level	Barrel Lift	Depth (m)	Graphic Log	CORE DESCRIPTION Rock Type, grain characteristics, colour, structure, minor components.	Weathering	Strength	ouclight	LOAD INDEX STRENGTH I _S (50)	(mm)	DESCRIPTION Type, inclination, thickness, planarity, roughness, coating. Specific General
				START CORING AT 16.49m						- - - - -
FULL RETURN		- - 17_ -		SANDSTONE: Fine groined, light grey & red brown, brown bands.	mw	1 M				- BEDDING PARTING D, DRANGE BROWN STAINING
70742		- 18 -			-	M				- CLAY SEAM, IOMM. - JOINTS 30° PLANAR, SMOOTH - - - CLAY SEAM 50 mm.
		- 19- -		but with Occosional shale layers.	HW MW					N.B. ALL DEFECTS NOT LABELLED ARE BEDDING PLANES, PLANAR, SMOOTH, E OCCASIONAL DRILLING BREAKS
		20		END OF BOREHOLE AT 19.581	₽₽. 					· · · · · · · · · · · · · · · · · · ·



CONSULTING GEOTECHNICAL ENGINEERS

Borehole No.

BOREHOLE LOG



Job I	No. 🟒	15009.JTT 26 - 2 - 90	p			IE WOOLDOWARE. ; SPIRAL AUGER EDSON 3000				
Groundwater record	Samples	Field Tests	Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer PReadings	Remarks
	D5 D5 D5	N=10 6, 4, 6 N=12 2, 1, 11	/- 2- 3-			BITUMINOUS PAVEMENT FILL Clayey Sand, fine groined, arange & de brown with Some Sandstone gravel. FILL: Silly Clay medium to high plasticity, dark brown, with Some shale & brick grovel. FILL: Sond fine to medium groined, orange brown with accosional sandstone gravel. Rubber fragments at 1.4m. FILL: Clayey Sand, fine grained, dark grey with damestic refuse including rubber fragments, plastic, brick, cloth. gravelly.				APPEARS MODERATELY WELL COMPACTED
	DS		4 - 5 -		OL.	ORGANIC SILTY CLAY: low plasticity dark green grey, with many decayed roots & some shells. becoming sondy	MC>PL	VS		STROMA DRGANIC ODDUR
	D5	N=3 1, 2, 1	6.			SAND: Time grained Clark brown, with shells.	W	VL		-

4

CONSULTING GEOTECHNICAL ENGINEERS

BOREHOLE LOG



REFER TO CORED B.H. LOG



2/3

Borehole No.

102

CORED BOREHOLE LOG

Borehole No.

102 _____3/3

	Ρ	lien rojeo ocat	ct:	SH.	INULLA SHARKS ARK PARK REDEVELOF TAIN COOK DRIVE, WC	PME	-N. 00,	T WARE.	an <u>a ann</u> a a sun a sun a sun anna an anna an anna an anna an an anna an an	
	J. D	ob N ate	lo: Drille	<i>1500</i> d: <i>260</i>	Core Size 27-2-90 Inclinatio SON 3000 Bearing:	e: /	N. 1			
	vel							POINT		DEFECT DETAILS
	Water Loss/Level	Barrel Lift	, Depth (m)	Graphic Log	CORE DESCRIPTION Rock Type, grain characteristics,	Weathering	Strength	LOAD INDEX STRENGTH I _S (50)	DEFECT SPACING (mm)	DESCRIPTION Type, inclination, thickness, planarity, roughness, coating. Specific General
-	>				START CORING AT 14.0m.			EW W S ES		
-	2025		- 14 - -		SANDSTONE: fine grained light grey, with some very thin clark grey laminae to 14.7m.	1 5.1	MS			-
-	10741 40		- 15 - -		Dis Deve, but light grey with bonds.					
			- 16 				5			- - -
					END OF BOREHOLE AT 16.9	5m.				
			- 18 — -							
1.01			- <u>9</u> 	-						
			-		ana ya kata mana mana kata mana mana mana mana mana mana mana m				· · · · · ·	


CONSULTING GEOTECHNICAL ENGINEERS

BOREHOLE LOG

Borehole No.

103

		5009.JTF 6 - 2 - 90		1	Method	EDSON 3000	·			
Groundwater record	Samples	Field Tests	Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand The Penetrometer Peredings	Remarks
	25	N= 12 3, 7, 5	2			FILL: Domestic refuse, including clothes, concrete & brick grovel, plastic Some sondy clay & clayey sond.				POORLY COMPACTED, Voided
			3 - 4 - 5 -			END OF BOREHOLE AT 2.3	<i>m</i> .			BESTRUCTION IN FILL CAUSED AUGE TO MOVE OUT OF LINE



CONSULTING GEOTECHNICAL ENGINEERS

BOREHOLE LOG



45

Borehole No.

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Im. WEST OF B.H.3

CONSULTING GEOTECHNICAL ENGINEERS

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BOREHOLE LOG

	Clie Proje	ect: _	CRONUL SHARK .	PAR.	K RE	DEVE	ELOPMENT	<u>ann for the second s</u>	<u>*************************************</u>		
	Loca	ation: 2	CAPTAII	V LL	00K .	DRI	IE WOOLOOWARE.				_ <u>.</u>
	Job Date					Metho	d: SPIRAL AUGER EDSON 3000				
	Groundwater record	Bamples	Field Tests	(Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Peadings	Remarks
				7			as above becoming mid brown mottled, with sandstone	MC>PL	V. 57.	-	
		DS	N = 22 4, 8, 4				with <u>s</u> andstone lovers.			260 320 280 300	
The second s				8-						-	
				9-		- -					
		DS								-	
· ···· · · · ·				- 10 -			END OF BOREHOLE AT 10	Om.		-	
					-						
			 	11 -				·			
					4					-	
				12						-	
				12 -	-						
					-					-	
				3-	-					-	
					-					-	
					-						b (reparting a second

2/2

Borehole No.

10.3A















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CONSULTING GEOTECHNICAL ENGINEERS

COPYRIGH⁻

BOREHOLE LOG

CRONULLA SHARKS Client: Project: SHARK PARK REDEVELOPMENT Location: CAPTAIN LOOK DRIVE WOOLDOWARE. R.L. Surface: 2.4m. Method: SPIRAL ALIGER Job No. ISDO9JTP A.H.D. Datum: G.C.H. RIG. 16 - 7 - 91 Date: ē Hand Penetromete Readings Consistency/ Rel. Density Unified Classification ndwater Graphic Log Moisture Condition Field Tests Depth (m.) Remarks Samples DESCRIPTION record kPa. *ز* . FILL: Clayey Sand with IA MEET some brovel, glass, cobbles, broken tile, metal pieces, grey. REFLISAL AT IM ON COBBLY FILL. POORLY COMPACTED. N=4 DS 4,2,2 2 SLINK LINDER WEIGHT DF RODS N >12 כם 1, 6, 11/50m 3 BOLINCING ORGANIC CLAY: high MC>PL ک DH PLINGENT plasticity, grey. GDOUR. Δ N < 1 2 | 700mi END OF BOREHOLE AT 4.7m 5 6

Borehole No.

301 E 301A



CONSULTING GEOTECHNICAL ENGINEERS

BOREHOLE LOG

Borehole No.

302

	ntion: No.		N D	00K .	DRI	ELOPMENT VE WOOLOQWARE. d: SPIRAL ALIGER G.C.H. RIG.		R.L. Dati	Surface: um: A	1:7m. 1.H.D.
record	Samples	Field Tests	Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	처 Hand Henetrometer Peadings	Remarks
~	 	N =6	1-			ASPHALTIC CONCRETE:over base. FILL: Clayey Sond with grovel, rubble and abundant timber fragments, dark grey.				PAVEMENT. POORLY COMPACTED.
:		2,3,3 N<1 1/700mm	2-		DH.	becoming more sitty sand. ORGANIC CLAY: high plasticity, with shell fragments.	MC>PL			-
		SLINK LINDER HAMMER WEIGHT.	4-	¥ ¥						-
			5-			END OF BOREHOLE AT 48	² m		-	
			6-						- -	



CONSULTING GEOTECHNICAL ENGINEERS

Borehole No.

BOREHOLE LOG

Proj€	ect: .		PAR.	K RE	DEVI	ELOPMENT VE WOOLOOWARE.			<u> </u>	
Job I Date	No.	15009J1 16 - 7 - 9	гр			d: <i>SPIRAL ALIGER</i> G.C.H. RIG.			Surface: um: /	1·7m. A.H.D.
ndwater record	Samples	Field Tests	Depth (m.)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Horetrometer Peredings	Remarks
		$ \begin{bmatrix} 2 \\ 9 \\ 4 \\ 2 \\ 3 \\ 1 \\ 1 \\ 1 $	2-		DL	FILL: Sandy Day Clayey Sand, medium plasticity, red brown and dork grey some gravel and cobbles, trace of timber pieces. ORGANIC SILTY CLAY: Jour to medium plasticity, dark grey obundant reed inclusions.		ب ک		PODRLY COMPACTED.
		```	4			END OF BOREHOLE AT 3.8m.				-



CONSULTING GEOTECHNICAL ENGINEERS

### **BOREHOLE LOG**

CRONULLA SHARKS Client: SHARK PARK REDEVELOPMENT **Project:** CAPTAIN COOK DRIVE, WOOLOOWARE Location: N/A R.L. Surface: Method: HAND AUGER Job No. 15009JTP Datum: Date: 25-1-96 Logged/Checked by: D.J./ Hand Penetrometer Readings (kPa.) SAMPLES Unified Classification Consistency/ Rel. Density Groundwater Record Graphic Log Tests E Moisture Condition Remarks DESCRIPTION Depth Field TOPSOIL: Silty sand, fine grained, brown, with some fine roots. GRASS COVER 0 DRY ON COMPLE-REFER TO М SCALA TION APPEARS FILL: Clayey silty sand, fine grained, grey, with some clay nodules and fine to medium POORLY TO MODERATELY COMPACTED gravel. FILL: Sand, fine to medium grained, yellow brown, with some clay bands. HAND AUGER REFUSAL END OF BOREHOLE AT 1.3m 2 3 5 6

Borehole No. 401



### **BOREHOLE LOG**

Borehole No.

Client: Project: Location:		K P	ARK I	REDE	VELOPMENT VE, WOOLOOWARE	een on all of the second dominant dominant dominant dominant dominant dominant dominant dominant dominant domin			
Job No. 15 Date: 25-		Ρ	927 227112275000000533 ⁷ 22		nod: HAND AUGER ged/Checked by: D.J./4	ki L		.L. Sur atum:	face: N/A
Groundwater Record U50 D5 SAMPLES	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
DRY ON R	EFER TO SCALA SHEET				TOPSOIL: Silty sand, fine to medium grained, brown, with some fine roots. FILL: Clayey silty sand, fine grained, grey, with some root bands and fine to medium gravel.	M			GRASS COVER APPEARS MODERATELY COMPACTED
		2			as above, but with some coarse slag gravel.			- - - - -	-
·····		3-			FILL: Gravelly sandy clay, low to medium plasticity, brown, fine to coarse sandstone gravel. END OF BOREHOLE AT 2.6m	MC>PL		- 	HAND AUGER REFUSAL
		- 4 -						- - - - -	-
		5 -						-	
		6 - - -							
		7						_	

#### **BOREHOLE LOG**

Borehole No. 403 1/1



#### **BOREHOLE LOG**

Borehole No.



#### **BOREHOLE LOG**

Borehole No.



Borehole No. 406 1/1



Borehole No. 407 1/1

Client:	CRONULLA SH	IARKS	ar ann an 1979 an an Anna an An
Project:		REDEVELOPMENT	
Location:	CAPTAIN COO	C DRIVE, WOOLOOWARE	2211-24 (1999) 12-1
<b>Job No.</b> 15	009JTP	Method: HAND AUGER	<b>R.L. Surface:</b> N/A
Date: 4-4-	-97	M	Datum: –
		Logged/Checked by: D.J./ M	
Groundwater Record U50 DB DB ES ES	Field Tests Depth (m) Graphic Log	DESCRIPTION	Condition Consistency/ Rel. Density/ Renetrometer kPand Readings (kPa.)
DRY ON RE	L. D. O FER TO O SCALA SHEET	FILL: Silty sand, fine to     medium grained, brown, with     some clayey sand bands and     fine to medium gravel.     FILL: Clayey silty sand, fine     grained, grey, with some     fine to coarse gravel.     FILL: Sandy clay, medium     plasticity, various colours,     with some fine to medium     gravel.     FILL: Silty sand, fine to     medium grained, brown, with     some clay nodules and fine to     coarse gravel.	M GRASS COVER APPEARS POORLY TO MODERATELY COMPACTED M
		END OF BOREHOLE AT 1.8m	REFUSAL





# Jeffery and Katauskas Pty Ltd CONSULTING GEOTECHNICAL ENGINEERS

#### SCALA PENETRATION TEST RESULTS

Client:	CRONULLA							
Project:		K REDEVELO						
Location:	CAPTAIN CO	DOK DRIVE, W	/OOLOOWAR	E	1.100000000		surfaces and a	
Job No.	15009JTP			Hammer We	eight & Drop: 9	kg/510mm		
Date:	25-1-96			Rod Diamet	er: 16mm			
Tested By:	D.J			Point Diame	ter: 20mm			
		Num	nber of Blows p	er 100mm Per	etration			
Test Location	401	402	407					
Depth (mm)		402	407					
0 - 100	1	1	1					
100 - 200	2	3	2					
200 - 300	3	3	1					
300 - 400	3	14	4					
400 - 500	3	19	4					
500 - 600	5	18	6					
600 - 700	4	9	7					
700 - 800	3	6	7					
800 - 900	3	4	11					
90 <u>0</u> - 1000	6	4.	7					
1000 - 1100	6	4	6					
1100 - 1200	4	5	15					
1200 - 1300	3	7	19					
1300 - 1400	3	6	9					
1400 - 1500	8	25	11					
1500 - 1600	23	12	12					
1600 - 1700	13	9	9					
1700 - 1800	9	. 11	9					
1800 - 1900	14	10	9					
1900 - 2000	9	10	9					
2000 - 2100	8	11	10					
2100 - 2200	9	9	10					
2200 - 2300	8	7	10					
2300 - 2400	8	15	9					
2400 - 2500	8	12	10					
2500 - 2600	8	15	11					
2600 - 2700	8	21	10					
2700 - 2800	7	21	8					
2800 - 2900	8	20	9					
2900 - 3000	END	END	END					

# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

#### **BOREHOLE LOG**





Borehole No. 501



Client: Project: Location:	SHAF	RK P		REDE	VELOPMENT VE, WOOLOOWARE	atterned by a second second second	1999 mar da la fasta da ana	1.000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000 - 000	
Job No. 1 Date: 11-					hod: SPIRAL AUGER GCH RIG ged/Checked by: L.S./#	R.L. Surface: N/A Datum:			
uroundwater Record U50 DB SAMPLES	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
	L	7	3	CL	as above, but with some red brown mottling and fine grained sand, some silt.	MC>PL	(VSt)		25mm
	e <u>Po ( </u>	- 9 –		-	SANDSTONE: fine to medium grained, pale grey, brown, dark brown and purple, some clay bands.	DW	М		MODERATE /TC' BIT RESISTANCE
				CL	SANDY CLAY: medium plasticity, brown and pale grey.	-	-	-	-
		11 - - -			SANDSTONE: fine to medium grained, brown and grey.	DW	VL		VERY LOW RESISTANCE
		12			as above, but pale grey.	-	L		LOW RESISTANCE
		13 -					M	-	MODERATE RESISTANCE

Client:	CRONULLA S	HARKS		VII	9979 B. G. C. MILLER (1993)		nan mangan ng kang mangang nan nan nan nan nan nan nan na na na na
Project:	SHARK PARK	REDE	VELOPMENT				
Location:	CAPTAIN CO	OK DR	IVE, WOOLOOWARE	anna a staintean an a	- Contraction of the Contraction of the		an a
1	15009JTP	Met	Method: SPIRAL AUGER GCH RIG				face: N/A
Date: 11	-12-96	Log	Logged/Checked by: L.S./			atum:	
<u> </u>						a.)	
eroundwater Record ES DB DB DB	Field Tests Depth (m) Graphic Loa	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
			SANDSTONE: as above.		м		MODERATE RESISTANCE
					L		LOW RESISTANCE
	15		END OF BOREHOLE AT 15.0m				
	-						-
	-						-
	16 -						~
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	17 -						-
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Borehole No. 501 3/3

### **BOREHOLE LOG**



1/2

Borehole No. 502



# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

#### **BOREHOLE LOG**



Borehole No. 502 2/2

#### **BOREHOLE LOG**



Borehole No.

#### **BOREHOLE LOG**



Borehole No.

1/1

504

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#### **BOREHOLE LOG**



### **BOREHOLE LOG**



1/2

Borehole No.

601



Job	ation: No. 15 e: 11-	5009JT	مىمى _{تىنى} بىرەرسىرەر بىرى _{يار} ئامرىد		COOK DRIVE, WOOLOOWARE Method: SPIRAL AUGER BCD 350			R.L. Surface: N/A Datum:			
					Log	ged/Checked by: S.E./	¥ 	<b></b> 1			
andwater Record	USO DB DS SAMPLES	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks	
<u>.</u> œ	1	N > 20 2,20/ 50mm DUNCING	- 7		SC	CLAYEY SAND: fine to medium grained, pale brown and red brown, with bands of coffee rock.	M	MD-D	-	-	
			-		-	SANDSTONE: fine to medium grained, mottled pale grey and red brown, with a trace of sandy clay bands.	DW	L	_	LOW 'TC' BIT RESISTANCE	
	)   1   1   1	1 > 20 20/ 50mm DUNCING	9 — - -		СН	SILTY CLAY: high plasticity, pale grey, with a trace of clayey sand bands.	MC <pl< td=""><td>н</td><td></td><td></td></pl<>	н			
			10		-	SANDSTONE: fine to medium grained, pale grey, with a trace of red brown mottling and clay bands	DW	L		- LOW RESISTANC	
			- - 11 -					LM	-	LOW TO MODERATE RESISTANCE	
			- 12 -						-	_	
			47			SANDSTONE: fine to medium grained, pale grey.	SW	м		MODERATE RESISTANCE	
						END OF BOREHOLE AT 13.0m			-		

#### **BOREHOLE LOG**



Borehole No.

Borehole No.

602 _{2/3}

Client: Project: Location:	CRONULL SHARK P CAPTAIN	ARK RE	EDEVELO	WOOLOOWARE					
Job No. 1 Date: 11–			Method: SPIRAL AUGER BCD 350 Logged/Checked by: S.E./			R.L. Surface: N/A Datum:			
			.oggea/	Checked by. S.L. / p					
Lroundwater Record ES DB SAMPLES	Field Tests Depth (m)	Graphic Log	Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks	
	N = 2 1,1,1		SILT grey sand	Y CLAY: medium plasticity, , with a trace of fine d and sandy bands.	MC>PL	St	100 110	HOLE COLLAPSING TO 7.0m RESIDUAL SOIL	
	8-		grai	DSTONE: fine to medium ned, red brown mottled grey.	DW	м-н	-	MODERATE TO HIGH 'TC' BIT RESISTANCE	
	9 -		as o but	ibove, with clay bands.			, , , , ,	LOW TO MODERATE RESISTANCE	
			CL SAN pale	DY CLAY: low plasticity, brown and orange brown.	MC>PL	-			
							-	- - -	
	12		– SANI grai	DSTONE: fine to medium ned, pale grey.	DW	L MH	-	LOW RESISTANCE	
	13						-	HIGH RESISTANCE	

# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

### **BOREHOLE LOG**



Borehole No. 602 3/3

Borehole No. 603

#### 3 1/3

# **BOREHOLE LOG**


# **BOREHOLE LOG**

Borehole No.

603 2/3

Client: Project: Location:	SHAI	RK P		REDE	VELOPMENT VE, WOOLOOWARE					
Job No. 15 Date: 12-		P		Method: SPIRAL AUGER BCD 550 Logged/Checked by: S.E./			R.L. Surface: N/A Datum:			
uroundwater Record ES DB DS SAMPLES DS	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks	
		7 		SM	SILTY SAND: fine to medium grained, grey.	W	MD		-	
	l = 13 5,6,7	- - - - - -			as above, but with sandy clay bands and a trace of extremely weathered shale bands.				- RESIDUAL SOIL - - - - -	
	t > 20 )/50mm	- 10 - - -							-	
		11 - - 12 -							 - - - - SANDSTONE ₿AND _ 150mm.t.	
		- - 13 - - -		_	SANDSTONE: fine to medium grained, pale grey.	SW	M-H		Omm MODERATE 'TC' BIT RESISTANCE	

# CORED BOREHOLE LOG

Borehole No. 603 3/3

	Cli	ient		(	CRONULLA SHARKS			<u>,</u>					
	Pre	ojeo	ct:		SHARK PARK REDEVEL								
	Lo	cat	ion:	C	CAPTAIN COOK DRIVE,	WOG	OLO	DWARE	and decrementary of the second s				
ľ	Jo	ЬN	lo.	1500	D9JTP Core	Size	: NN	/LC	R.L	Surface: N/A			
	Da	ate:	12	-8-	97 Inclin	atior	n: ∨	ERTICAL	Dat	tum:			
	Dr	ill 1	Гуре	: BC	D 550 Bearing	ng:			Logged/Checked by: S.E				
					CORE DESCRIPTION			POINT LOAD		DEFECT DETAILS			
	r ross/Level	Barrel Lift	h (m)	hic Log	Rock Type, grain character— istics, colour, structure, minor components.	Weathering	Strength	INDEX STRENGTH I (50)	DEFECT SPACING (mm)	DESCRIPTION Type, inclination, thickness, planarity, roughness, coating.			
I	water	Barr	Depth	Graphic		Wed	Stre		588 588 188 188 18	Specific General			
			13							- NOTE: DEFECTS NOT INDIVIDUALLY DESCRIBED ARE BEDDING PARTINGS 0-10°, PLANAR, ROUGH -			
			- 14		START CORING AT 14.06m SANDSTONE: fine to medium grained, pale grey and red brown banded, bedded at 5-10.	DW	L	×		- XWS, Bmm.t.			
a way to a			15 -	- - 15 -		as above, but mottled pale grey and red brown.			×		- CS, 0°, 20mm.t. - XWS, 0°, 30mm.t. - J, 23°, P, R		
	FULL		-				м	×		<ul> <li>Be, 17°, P, R</li> <li>IRON INDURATED BAND WITH CLAY, 40mm.t.</li> </ul>			
I	RET- URN		-		SHALY CLAY: high plasticity, grey to dark grey, with thin sandstone bands, MC <pl,< td=""><td></td><td></td><td></td><td></td><td>- CS, 0°, 30mm.t.</td></pl,<>					- CS, 0°, 30mm.t.			
	2		16 -		Hard. INTERBEDDED SHALE AND SANDSTONE: dark grey shale and fine grained, pale grey sandstone.	XW	EL- VL			-			
			· -		SANDSTONE: fine grained, grey.	DW	VL-L	×		- CS, 0º, 20mm.t.			
			17 -		SANDSTONE: fine to medium grained, pale grey, bedded at 15°.	S₩	Н	×		-			
				<u></u>	END OF BOREHOLE AT 17.16m					-			
				-						-			
			18 -							-			
										-			
										-			
			19 -							- -			
				_						-			
GHT				-						-			
COPYRIGHT			20	-						an an ann an			

# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

# **BOREHOLE LOG**



Borehole No. 604

1/3

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# **BOREHOLE LOG**



Borehole No.

604

# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

# **CORED BOREHOLE LOG**

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Borehole No. 604

С	lien	it:		CRONULLA SHARKS						
P	roje	ct:		SHARK PARK REDEVI	ELOPM	IENT				
L	oca	tion		CAPTAIN COOK DRIV	E, WO	OLO	OWARE			
J	ob	No.	150	09JTP Co	re Size	e: NI	MLC	R.1	Surface: N/A	
D	ate	: 12	-8-	-97 <b>Inc</b>	linatio	n: V	ERTICAL		tum:	•
D	rill	Туре	<b>:</b> B	CD 550 Bea	ring:			Log	gged/Checked by: S.E.	1ff
e e				CORE DESCRIPTION			POINT		DEFECT DETAILS	
iter Loss/Level	.ater Loss/L Barrel Litt Depth (m) Graphic Loa		aphic Log	Rock Type, grain character istics, colour, structure, minor components.	icter- Ire, - - -		INDEX STRENGTH I _s (50)	DEFECT SPACING (mm)	DESCRIPTION Type, inclination, thickness, planarity, roughness, coating.	
	Ba	0 13	ยั		§	Strength		500 100 50 100 100	Specific Gen	eral
		15		START CORING AT 13.44m					-	
FULL RET URN		14		SANDSTONE: pale grey with thin grey laminations.	SW	H	×		<ul> <li>Be, 15°, P, R, CLAY COATED</li> <li>Be, 15°, P, S</li> <li>XWS, 45mm.t.</li> <li>CS, 10mm.t.</li> <li>XWS, 5mm.t.</li> <li>8e, 10°, P, S</li> <li>XWS, 10mm.t.</li> <li>XWS, 10mm.t.</li> </ul>	
		17								

# **BOREHOLE LOG**

Borehole No. 605



# **BOREHOLE LOG**

**ULTTRIGE** 

CRONULLA SHARKS Client: SHARK PARK REDEVELOPMENT Project: CAPTAIN COOK DRIVE, WOOLOOWARE Location: N/A**R.L. Surface:** Method: SPIRAL AUGER Job No. 15009JTP BCD 350 Datum: Date: 13-8-97 Logged/Checked by: W.T./ Hand Penetrometer Readings (kPa.) SAMPLES Unified Classification Strength/ Rel. Density : troundwater Record Log Moisture Condition/ Weathering Tests Remarks Depth (m) DESCRIPTION Graphic Field n ROOT SYSTEM EXTENDS APPROX. 200mm BELOW FILL: Sand, fine to medium grained, dark yellow and brown, with a trace of sandstone gravel. М n SURFACE MC>PL FiLL: Gravelly sandy clay, medium plasticity, grey mottled red, with fine to coarse grained sand, sandstone gravel and glass APPEARS WELL 320 280 170 COMPACTED N = 15 4,7,8 FILL: Silty sand, fine to coarse grained, light brown and black, with organic matter (wood) and clay fines. APPEARS MODERATELY COMPACTED AFTER 5 MINS N = 8 1,4,4 2 ORGANIC SILTY CLAY: medium plasticity, dark brown and black, with fine roots and a trace of rootlets and shell MC>PL VS-S NO SAMPLE RECOVERED FROM SPT OL N = 1 1,0,1 fragments. 3 SOLID CONE < 11 700mm UNDER OWN WELGHT f (S-F)1 1 SILTY CLAY: medium plasticity, CL 1 light brown to dark grey, 2 with fine grained sand. 1 1 2 5 1 2 2 2 2 3 6 4 (VSt-H) 8 14 17 22 END OF BOREHOLE AT 6.7m

Borehole No. 606 '1/1

CONSULTING GEOTECHNICAL ENGINEERS

## **BOREHOLE LOG**

CRONULLA SHARKS Client: SHARK PARK REDEVELOPMENT Project: CAPTAIN COOK DRIVE, WOOLOOWARE Location: R.L. Surface: -Method: SPIRAL AUGER Job No. 15009JTP BCD 450 Datum: -Date: 6-10-94 Logged/Checked by: FK./ Hand Penetrometer Readings (kPa.) Unified Classification Consistency/ Rel. Density Groundwater Record Log Tests Moisture Condition Remarks E DESCRIPTION Samples Graphic Depth Field FILL: Silty clayey sand, medium grained, brown to dark brown with bricks, glass and ripped sandstone D 0 fragments and some root fibres. DS М as above, but with wood, plastic and igneous rock fragments. DS 2 DS CLAYEY SILT: low plasticity, dark brown with some fine MC>PL ORGANIC ODOUR roots. DS TEMPORAR Y 3 V PEIZOMETER INSTALLED TO 4.5m SLOTTED FOR 3m SANDY SILT: low plasticity, dark brown with some orange MC>PL brown ironstaining. DS END OF BOREHOLE AT 4.5m 5 6

Borehole No.

Borehole No. 702_{1/1} ,

Clier Proje Loca	ect:	SHA	RK P		REDE	VELOPMENT VE, WOOLOOWARE					
	<b>No.</b> 1 e: 6-1				Method: SPIRAL AUGER BCD 450 Logged/Checked by: FK.			R.L. Surface: – Datum: –			
uroundwater Record	Samples	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks	
<u>5</u> œ	DS	Le	0			FILL: Silty sandy clay. low to medium plasticity, brown with brick, timber, ripped sandstone, glass, steel and material fragments.	MC <pl< td=""><td></td><td>-</td><td></td></pl<>		-		
	DS					FILL: Silt, low plasticity, dark brown with some sand and some clay and wire, brick and ripped sandstone fragments.	MC>PL			-	
	DS		2 -		-	CLAYEY SILT: low plasticity, dark brown with some bands containing shell fragments, 100mm.t.	MC>PL			ORGANIC ODOUR TEMPORAR Y PIEZOMETER INSTALLED TO 4.5m. SLOTTED FOR 3m	
	DS		4-		SP	SAND: fine to medium grained, dark grey, with a trace of silt.	M .			· · · ·	
			5 -			END OF BOREHOLE AT 4.5m					
			6 -	-						· · · · · · · · · · · · · · · · · · ·	
			7	-				Martin Contractor			

Borehole No. 703 1/1

Clier Proje Loca	ect:	SHA	RK P		REDE	VELOPMENT VE, WOOLOOWARE	<u>an ann an Ann An</u>	en e			
Job	<b>No.</b> 1 e: 6-1	5009J			Method: SPIRAL AUGER BCD 450 Logged/Checked by: FK.			R.L. Surface: – Datum: –			
Groundwater Record	Samples	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks	
<u>.</u> 98	ES				20	FILL: Sandy clay, low to medium plasticity, dark brown with some igneous rock and ripped sandstone fragments.	D-M		-		
	ES		2			FILL: Silty sand, fine to medium grained, black with some igneous rock, glass and ripped sandstone fragments.	M			-	
	ES		3-		-	CLAYEY SILT: low plasticity, dark brown.	MC>PL			MODERATE ORGANIC ODOUR TEMPORARY PIEZOMETER	
	ES		4-							PIEZOMETER INSTALLED TO 4.5m. SLOTTED FOR 3m	
			5			END OF BOREHOLE AT 4.5m					
			6-						-		
			-							ana ang ang ang ang ang ang ang ang ang	

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CRONULLA SHARKS Client: SHARK PARK REDEVELOPMENT **Project:** CAPTAIN COOK DRIVE, WOOLOOWARE Location: R.L. Surface: -Method: SPIRAL AUGER Job No. 15009JTP GCH RIG Datum: -Date: 6-10-94 Logged/Checked by: FK./ 3 Hand Penetrometer Readings (kPa.) Consistency/ Rel. Density Unified Classification [og broundwater Record Moisture Condition Field Tests Remarks Depth (m) DESCRIPTION Samples Graphic FILL: Sand, fine to medium grained, brown with some silt and some igneous rock D £ fragments. ES FILL: Silt, low plasticity, black, with some sand, and some wood, ceramic, igneous MC>PL rock and ripped sandstone ES fragments. ES 3 13. MC>PL CLAYEY SILT: low plasticity, dark brown. ES END OF BOREHOLE AT 4.5m 5 6

Borehole No. 704 1/1

# Jeffery and Katauskas Pty Ltd CONSULTING GEOTECHNICAL ENGINEERS

# **BOREHOLE LOG**

Borehole No. 705 1/1

Clie				A SH ARK		S VELOPMENT		an the second	antive and Anna mutual and a second second	
Proj Loca	ation:					VE, WOOLOOWARE	VIETENIA VIOTENIA MARTINI			annan an ann an taoinn an taoin
	<b>No.</b> 1: e: 6-1		ΤP		Met	hod: SPIRAL AUGER GCH RIG	R.L. Surface: – Datum: –			
					Log	ged/Checked by: FK./(§	1			
oroundwater Record	Samples	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition	Consistency/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
<u></u>	ES		0			FILL: Sand, medium grained, light brown with some silf and igneous rock fragments.	м			- - -
<b>A</b>	ES		1 -			FILL: Silty sandy clay. low to medium plasticity, brown with some glass, brick, ripped sandstone and timber fragments.	MC>PL			-
	ES		2-			as above, but with approximately 40% ripped sandstone and timber fragments.	MC>PL			-
£			3		-	CLAYEY SILT: low plasticity, dark brown with some bands containing shell fragments.	MC>PL			TEMPORARY PIEZOMETER INSTALLED TO 4.5m SLOTTED TO 3m
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	ES		4 -		SP	SAND: fine to medium grained, dark grey with a trace of				- 
			5 -			SIIT. END OF BOREHOLE AT 4.5m				
			6 -							· •
			7						an Churter Childhair Walanza Person	

CRONULLA SHARKS **Client:** SHARK PARK REDEVELOPMENT Project: CAPTAIN COOK DRIVE, WOOLOOWARE Location: R.L. Surface: -Method: SPIRAL AUGER Job No. 15009JTP GCH RIG Datum: -Date: 6-10-94 Logged/Checked by: FK. / . Hand Penetrometer Readings (kPa.) Unified Classification Consistency/ Rel. Density uroundwater Record po_ Moisture Condition Remarks Field Tests Depth (m) DESCRIPTION Graphic Samples MC<PL FILL: Silty clay, medium to high plasticity, brown with some ironstone fragments. 0 ES MC>PL FILL: Silt, low plasticity, dark brown with some sand, and some wood fragments. ES MC>PL CLAYEY SILT: low plasticity, dark brown. ES 3 MC>PL CLAY: low to medium plasticity, dark brown grey with some silt and some sand. CL ES . END OF BOREHOLE AT 4.5m 5 6

Borehole No. 706 1/1

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS



Interpreted by:  $\mathcal{MK}$ . Checked by:  $\mathcal{PW}$ 



CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS



#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client:	Cronulla Sharks				n h i an ann dhann	
Project:	Shark Park Rede		NOW			·
Location:	Captain Cook Dr	'ive, wooloo	ware, INSW			
Job Ref.:	15009JTPcpt801	1	RL Surface: NA		Data File:	AP061129.H1
Test Date:	6/4/00		Datum: NA		Operator:	MK/PH
	Cone Resista	nce	Sleeve Friction	Friction Ratio	Interpre	eted Profile
	Qc (MPa)	Qc (MPa)	Fs (kPa)	Fr (%)		
		0 1 2 3 4 5	0 100 200 300 400 500		SILTY CLA	Y: very stiff.
				11	as ou but v hard.	bove, ery_stiff to
12				12	os ob but si	ove, Hift.
13				13		
14 (m) 14 (m) 14 (m) 14 (m) 14 (m) 14 (m) 15				14	as abi but ve	ove, ry stiff.
16				16	SILTY SAN, dense	0:medium
17				17	SILTY CLAY to har	': very stiff ⊲.
18				18		
19				19		
20				20	SILTY SAND: dense as obove bu Interpreted by;	loose to medium <u>it very toose</u> . M.K.

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS



Interpreted by: M.K.Checked by: PW



CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

## EFCP No. 802 1/2

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client:	Cronulla Sha					
Project: Location:		Redevelopment k Drive, Wooloo	WORD NIGIM			
Location	Captain Cool		wale, NOW			
Job Ref.:	15009JTPcp	t802	RL Surface: NA		Data File:	AP061016.H1
Test Date:	6/4/00		Datum: NA		Operator:	MK/PH
	Cone Res	istance	Sleeve Friction	Friction Ratio	Interpre	ted Profile
	Qc (MPa)	Qc (MPa)	Fs (kPa)	Fr (%)		
0 10 1 2 3 4 (m) the definition of the second se		Qc (MPa)	Fs (kPa)	Fr (%) 1 1 1 1 1 1 1 1	Clay of gravelly Appeor- compose ORGANIC SDFF to SILTY CLA SILTY SAN Very S SAND TO - loase f Dase f SILTY SAN Very O SILTY SAN Very O SILTY SAN Very O	rbedded silly nd silly sond, spoorly ted. SILTY CLAY: firm. NY: soft. SILTY CLAY: firm. SILTY STAND: SILTY STAND: SILT

Interpreted by: M.K. Checked by:  $\rho W$ 

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

## EFCP No. 802 2/2

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS



Interpreted by: M.K. Checked by: Pw

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

## EFCP No. 803 1/1

#### **ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS**

F	Client: Project:	Cronulla Sharks Shark Park Rec	levelopment			
	ocation:	Captain Cook D		ware, NSW		Data File: AP051349.H1
٦	est Date:	5/4/00		Datum: NA		Operator: MK/AK
		Cone Resista	ance	Sleeve Friction	Friction Ratio	Interpreted Profile
		Qc (MPa)	Qc (MPa)	Fs (kPa) 0 100 200 300 400 500	Fr (%) 0 5 10	
-12						FILL: Interbedded silty sand and silty elay. Appears well compacted. as above, but appears poorly to moderately compacted.
	2				2	as above, but appears moderately to well compacted.
	3					ORGAHIÇ SILTY CLAY: Soft to firm.
	a					SILTY_SAND: 10050 to
	Depth (m)					medium dense.
1	5				5 	as above, but dense to very dense.
	⁶ Re	fusal 5.84m				GRAVELLY SAND: Very dense.
	7				7 	
	8					
	9				9	
	10 -				10	Interpreted by: Mr

Interpreted by: M.K. Checked by:  $\rho_{\omega}$ 

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: **Cronulla Sharks** Project: Shark Park Redevelopment Location: Captain Cook Drive, Woolooware, NSW Job Ref.: 15009JTPcpt803a **RL Surface:** NA Data File: AP051431.H1 Test Date: 5/4/00 Datum: NA **Operator:** MK/AK **Cone Resistance Sleeve Friction** Friction Ratio Interpreted Profile Qc (MPa) Qc (MPa) Fs (kPa) Fr (%) 20 30 40 50 0 1 2 3 4 5 0 100 200 300 400 500 5 10 0 10 0 0 t 0 FILL: Interbedded silty sond and silty clay Appears maderately to well compacted. 1 1 as above but appears poorly to moderately compacted. 2 2 ORGANIC SILTY CLAY: Soft to firm. 3 3 4 4 SILTY SAND: loose to Depth (m) medium dense. as above, 5 5 but dense to very dense. Refusal 5.55m 6 6 7 7 8 8 9 9 10 10

> Interpreted by: M.K.Checked by:  $f \omega$

EFCP No. 803a 1/1

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#### **ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS**





Interpreted by: M.K. Checked by: PW

EFCP No.

804

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

19

20

Refusal 19.93m

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: Project: Location:	Cronulla Sharks Shark Park Rec Captain Cook D	levelopment	vare, NSW.			
Job Ref.: Test Date:	15009JTPcpt80 12/4/00		RL Surface: NA Datum: NA		Data File: Operator:	AP121115.H1 MK/PH
	Cone Resist	ance	Sleeve Friction	Friction Ratio		eted Profile
	Qc (MPa)	Qc (MPa)	Fs (kPa)	Fr (%)		
10 10 11 12 13 14 14 15 16 17					SILTY SAN SILTY CLAY Very S as obo but ver	D: medium dens stiff to tiff. ve y stiff to hord. No dense. stiff to
18				18		
44					SILTY SANL	r: medium

Interpreted by: M.K.Checked by:  $\rho W$ 

19

20

dense to dense.

SILTY CLAY : stiff to very stiff.

EFCP No.

804

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: Project: Location:	Cronulla Shar Shark Park Re Captain Cook	edevelopment	ware, NSW		
Job Ref.: Fest Date:	15009JTPcpt8 5/4/00	306	RL Surface: NA Datum: NA		Data File: AP051158.H1 Operator: MK/AK
	Cone Resistance		Sleeve Friction	Friction Ratio	Interpreted Profile
	Qc (MPa)	Qc (MPa)	Fs (kPa)	Fr (%)	
0 10 1 (m) the definition of t					FILL: Silly clay, Appears moderately compacted. FILL: Interbedded silty clay and silty sond. Appears poorly compacted. DRGANIC SILTY CLAY: Soft, with sond.
6				6	as above, but dense to very dense.
					CLAY: firm to stiff.
8				8	SILTY SAND: medium dense to dense. SILTY CLAY: very stiff SILTY SAND TO SANDY SILT medium dense/hord. SILTY CLAY:
9				9	SILTY CLAY: very stiff.

Interpreted by:  $\mathcal{M}.\mathcal{K}.$ Checked by:  $\mathcal{P}\mathcal{W}$ 



CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: Project: Location:	Cronulla Shark Shark Park Rec Captain Cook D	development	ware, NSW			
Job Ref.: Test Date:	15009JTPcpt80 5/4/00		RL Surface: NA Datum: NA		Data File: Operator:	AP051158.H1 MK/AK
	Cone Resist	tance	Sleeve Friction	Friction Ratio	Interpr	eted Profile
0.40	Qc (MPa)	Qc (MPa) 0 1 2 3 4 5	Fs (kPa) 0 100 200 300 400 500	Fr (%) 0 5 10		
10	20 30 40 50				SILTY CLA Very S	
				11	_SILTY CLA very s	Y & SANDY CLAY tiff to hard.
12 .						
13				13	GRAVELLY	SAND : very dens
	fusal 13.35m –			14		
14				15		
16 -						
17				17		
18						
19 -						
20				20	Interpreted by	

Interpreted by: MK. Checked by: PW



CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS



#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client:	Cronulla Sharks						
Project:	Shark Park Redevelopn	nent					
Location:	Captain Cook Drive, Wo	oolooware, NSW.					
	-						
Job Ref.:	15009JTPcpt807	RL Surface:	NA	Data File:	AP120934.H1		
Test Date:	12/4/00	Datum:	NA	Operator:	MK/PH		



Checked by: PW

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: **Cronulla Sharks** Project: Shark Park Redevelopment Captain Cook Drive, Woolooware, NSW. Location: Job Ref.: 15009JTPcpt807 RL Surface: NA Data File: AP120934.H1 Test Date: 12/4/00 Datum: NA **Operator:** MK/PH **Sleeve Friction** Interpreted Profile **Cone Resistance** Friction Ratio Qc (MPa) Qc (MPa) Fs (kPa) Fr (%) 20 30 40 012345 100 200 300 400 500 0 10 50 0 0 5 10 10 10 SILTY CLAY : stiff to Very _stiff. 11 11 12 12 13 13 Depth (m) 🕁 14 os above, but very stiff to hard. 15 15 2.2 16 16 17 17 18 18 Refusal 17.87m 19 19 20 20

Interpreted by:  $\mathcal{MK}$ Checked by:  $\mathcal{PW}$ 

EFCP No. 807 2/2

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS



Checked by:  $P_{W}$ 

EFCP No. 808

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

20

## EFCP No. 808 2/2

#### **ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS**

Client: Project:	Cronulla Shark	levelopment				
Location:	Captain Cook D 15009JTPcpt80 6/4/00		RL Surface: NA Datum: NA		Data File: Operator:	AP061530.H MK/PH
	Cone Resist	ance	Sleeve Friction	Friction Ratio	Interpre	eted Profile
	Qc (MPa)	Qc (MPa)	Fs (kPa)	Fr (%)		
	20 30 40 50	0 1 2 3 4 5			CLAY: Very	
11				11	SILTY CLAY	': very stiff.
12 -				12	as abov but stift	e, f to very stiff.
13 -				13		
Depth (m)				14	SILTY CLA With S	Y: very stiff and bonds.
15				15		
16				16		
17				17	SILTY CLAY: to har	very stiff
18						
19	fusal 18.93m			. 19	SILTY SAND	: very dense.

Interpreted by: M.K. Checked by:

20

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

## EFCP No. 809 1/2

#### **ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS**

Client:	Cronulla Sharks								
Project:	Shark Park Redev	velopment							
Location:	Captain Cook Drive, Woolooware, NSW								
Job Ref.:	15009JTPcpt809		RL Surface:	NA		Data File:	AP051052.H1		
Test Date:	5/4/00 Cone Resistance		Datum: NA Sleeve Friction			Operator:	MK/AK		
					Friction Ratio	Interpre	ed Profile		
		Qc (MPa)	Fs (kPa		Fr (%)				
0 10 0- <del> </del>	20 30 40 50 0	12345	0 100 200 300	) 400 500	0 5 10 i <del>rrrr; irrrr</del> f 0				
	immy Probe								
	or 880mm								
					_⊦_}₽⊨₽₩₽₽₽₽₽₽ ↓ <b>₩₩₽₽₽₽₽₽₽₽₽₽</b> ₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽	5111 · Inte	cheddad silty		
$\Box$					┤╤╤╤╤╤╼╼	clay a	nd silty sand.		
Z I			2			Appear compati	rbedded silly nd silly sand. rs poorly ded.		
						Ý			
2									



Interpreted by: M.K. Checked by: PW

CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

#### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS



Interpreted by: M.K.Checked by:  $\rho W$ 



CONSULTING GEOTECHNICAL AND ENVIRONMENTAL ENGINEERS

### ELECTRICAL FRICTION CONE PENETROMETER TEST RESULTS

Client: Project: .ocation:	Cronulla Sharks Shark Park Redevelopment Captain Cook Drive, Woolooware, NSW								
ob Ref.: est Date:	15009JTPcpt810 6/4/00		RL Surface: NA Datum: NA		Data File: Operator:	AP061409.H1 MK/PH			
est Date.	Cone Resistan	Ice	Sleeve Friction	Friction Ratio		ted Profile			
0 10	Qc (MPa) 20 30 40 50 0	Qc(MPa)	<b>Fs (kPa)</b> 0 100 200 300 400 500	<b>Fr (%)</b> 0 5 10					
					FILL: Interbedded si'lly sond and silly day. Appears poorly comported.				
Depth (m)				5	CLAY: fin				

.::

6

7

8

9

10

Refusal 7.89m

Interpreted by: *M.K.* Checked by: *PW* 

SILTY SAND : loose.

CLAY : VERY Stiff.

SILTY CLAY : Very stiff to hard.

INTERBEDDED SILTY SAND: loose, SILTY CLAY: very stiff.

GRAVELLY SAND : VERY dense

6

7

8

9

L 10



# **BOREHOLE LOG**

Borehole No.

**901**_{1/1}



# **BOREHOLE LOG**

Borehole No.

**902**_{1/1}



# **BOREHOLE LOG**

Borehole No.

**903**_{1/1}

Job No. 17119SP Date: 9-9-02				Method: SPIRAL AUGER JK550 Logged/Checked by: J.R./ ASH			<b>R.L. Surface:</b> ≅ 3.3m <b>Datum:</b> AHD			
Groundwater Record EC	U50 SAMPLES DS	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION	Moisture Condition/ Weathering	Strength/ Rel. Density	Hand Penetrometer Readings (kPa.)	Remarks
	N = 12 6,5,7 SPT 7/150mm REFUSAL N = 2 2,1,1	0			ASPHALTIC CONCRETE: 8mm.t., over FILL: Sandy gravel, fine to coarse grained igneous gravel, fine to coarse grained sand. FILL: Silty gravelly clay, medium plasticity, red brown mottled grey, fine to medium grained ironstone and sandstone gravel. FILL: Gravelly clayey sand, fine to medium grained, mottled grey and brown, fine to coarse grained ironstone, igneous and sandstone gravel, with a trace of wire, glass, plastic and timber fragments.	D MC>PL			0.0%CH4 20.9%02 APPEARS MODERATELY COMPACTED NO SAMPLE RECOVERY FROM SPT SAMPLER APPEARS POORLY COMPACTED	
		N = 3 1,2,1	4 - - - - - - - - - - - - - - - - - -		OL SC	ORGANIC SILTY CLAY: low plasticity, grey brown, with rootlets. CLAYEY SAND: fine to medium grained, grey brown, with a trace of rootlets and shell material.	MC > PL	(VS) VL		ORGANIC ODOUR 0.3%CH4 18.7%02

# **BOREHOLE LOG**

Borehole No

904.



# **BOREHOLE LOG**

Borehole No.

**905**_{1/1}



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# **BOREHOLE LOG**

Borehole No.

9061/1



# Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

# **BOREHOLE LOG**

**Borehole No** 

**907**_{1/1}



# **BOREHOLE LOG**

Borehole No.

9081/1



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# **BOREHOLE LOG**

**Borehole No** 





### Jeffery and Katauskas Pty Ltd consulting geotechnical and environmental engineers

# **BOREHOLE LOG**

Borehole No

**910**_{1/1}



# **BOREHOLE LOG**

Borehole No.

**911**_{1/1}

Clier Proje Loca	ect:	CRONULLA SUTHERLAND LEAGUES CLUB LIMITED CRONULLA SUTHERLAND LEAGUES CLUB REZONING PROPOSAL CRONULLA LEAGUES CLUB, CAPTAIN COOK DRIVE, WOOLOOWARE, NSW								NSW	
Job Date	Method:SPIRAL AUGER JK550R.L. Surface:N/AJK550Datum:Logged/Checked by:S.O.C./ ###							face: N/A			
Groundwater Record	ES UEO DB SAMPLES	Field Tests	Depth (m)	Graphic Log	Unified Classification	DESCRIPTION Description		Moisture Condition/ Weathering Strength/ Rel. Density Hand Penetrometer Readings (kPa.)		Remarks	
ON COMPLET ION		N = 6 5,4,2	0 - - - - - - - - - - - - - - - - - - -		014	FILL: Gravelly sand, fine to medium grained, light brown, fine to medium grained sandstone and igneous gravel. FILL: Sand, fine to medium grained, grey and brown, with a trace of clay fines. SILTY SAND: fine to medium	D	VL		- 0.0%CH4 20.8%O2 - APPEARS POORLY COMPACTED	
		N = 1 2,0,1			SM	grained, brown, with roots and organic fibres				POSSIBLY FILL TO 2.0m DEPTH 1.2%CH4 20.4%O2	
		SPT SUNK UNDER SELF WEIGHT	2		OL	ORGANIC SILTY CLAY: low plasticity, dark grey, with fibre, roots and timber fragments.	MC>PL			ORGANIC ODOUR 	
		N = 6 1,2,4	- 4 - - - 5 - - - - -		SC	CLAYEY SAND: fine to medium grained, light brown and light grey, with fine to coarse grained iron indurated sand bands.	W			- - - - - - - - - - -	
			6  - - - - - - - - - - -			END OF BOREHOLE AT 6.0m			-	0.7%CH4 <u>20.4%O2</u>	

# **BOREHOLE LOG**

CRONULLA SUTHERLAND LEAGUES CLUB LIMITED Client: CRONULLA SUTHERLAND LEAGUES CLUB REZONING PROPOSAL **Project:** CRONULLA LEAGUES CLUB, CAPTAIN COOK DRIVE, WOOLOOWARE, NSW Location: Method: SPIRAL AUGER R.L. Surface: ≅ 1.9m Job No. 17119SP JK550 Date: 11-9-02 Datum: AHD Logged/Checked by: S.O.C./ SAMPLES Hand Penetrometer Readings (kPa.) Groundwater Record Unified Classification Strength/ Rel. Density Moisture Condition/ Weathering Graphic Log Field Tests Depth (m) DESCRIPTION Remarks D ASPHALTIC CONCRETE: 6mm.t., MC<PL over FILL: Gravelly sand, fine to medium grained, brown. FILL: Clayey silt, low plasticity, 0.2%CH4 grev. ON N = 420.4% COMPLET 3,2,2 ION APPEARS POORLY COMPACTED FILL: Silty sand, fine to medium W grained, grey, with occasional steel wire, plastic and medium to coarse 1.6%CH4 N = 24grained sandstone gravel. 18.86%02 11,18,6 APPEARS WELL COMPACTED SULPHUR ODOUR ORGANIC SILTY CLAY: low MC>PL (S) 01 plasticity, grey, with shells, fibre. 19.0%CH4 N = 218.8%02 0,0,2 SPT SUNK 300mm UNDER SELF WEIGHT AT START OF TEST VS CL MC>PL SILTY CLAY: low plasticity, light brown, with occasional shells. 7.0%CH4 20 N = 319.9%02 20 0,1,2 10 SPT SUNK 150mm 5 UNDER SELF WEIGHT AT START OF TEST (S) SILTY CLAY: low plasticity, dark grey, with occasional timber fragments. 1.7%CH4 20.4%02 END OF BOREHOLE AT 6.0m

Borehole No.

**912**_{1/1}

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CONSULTING GEOTECHNICAL ENGINEERS



### **REPORT EXPLANATION NOTES**

### INTRODUCTION

These notes have been provided to amplify the geotechnical report in regard to classification methods, field procedures and certain matters relating to the Comments and Recommendations section. Not all notes are necessarily relevant to all reports.

The ground is a product of continuing natural and man-made processes and therefore exhibits a variety of characteristics and properties which vary from place to place and can change with time. Geotechnical engineering involves gathering and assimilating limited facts about these characteristics and properties in order to understand or predict the behaviour of the ground on a particular site under certain conditions. This report may contain such facts obtained by inspection, excavation, probing, sampling, testing or other means of investigation. If so, they are directly relevant only to the ground at the place where and time when the investigation was carried out.

## DESCRIPTION AND CLASSIFICATION METHODS

The methods of description and classification of soils and rocks used in this report are based on Australian Standard 1726, the S.A.A. Site Investigation Code. In general, descriptions cover the following properties – soil or rock type, colour, structure, strength or density, and inclusions. Identification and classification of soil and rock involves judgement and the Company infers accuracy only to the extent that is common in current geotechnical practice.

Soil types are described according to the predominating particle size and behaviour as set out in the attached Unified Soil Classification Table qualified by the grading of other particles present (e.g. sandy clay) as set out below:

Soil Classification	Particle Size
Clay	less than 0.002mm
Silt	0.002 to 0.06mm
Sand	0.06 to 2mm
Gravel	2 to 60mm

Cohesive soils are classified on the basis of strength (consistency) either by use of hand penetrometer, laboratory testing or engineering examination. The strength terms are defined as follows.

Classification	Unconfined Compressive Strength kPa
Very Soft	less than 25
Soft	25 - 50
Firm	. 50 – 100
Stiff	100 - 200
Very Stiff	200 - 400
Hard	Greater than 400
Friable	Strength not attainable
	<ul> <li>soil crumbles.</li> </ul>

Non-cohesive soils are classified on the basis of relative density, generally from the results of Standard Penetration Tests (S.P.T.) as below:

Relative Density	S.P.T. "N" Value (blows/300mm)					
Very loose	less than 4					
Loose	4 - 10					
Medium dense	10 - 30					
Dense	30 – 50					
Very Dense	greater than 50					

Rock types are classified by their geological names, together with descriptive terms regarding weathering, strength, defects, etc. Where relevant, further information regarding rock classification is given in the text of the report. In the Sydney Basin, "Shale" is used to describe thinly bedded to laminated siltstone.

### SAMPLING

Sampling is carried out during drilling or from other excavations to allow engineering examination (and laboratory testing where required) of the soil or rock.

Disturbed samples taken during drilling provide information on plasticity, grain size, colour, moisture content, minor constituents and, depending upon the degree of disturbance, some information on strength and structure.

Undisturbed samples are taken by pushing a thinwalled sample tube, usually 50mm diameter (known as a U50), into the soil and withdrawing it with a sample of the soil contained in a relatively undisturbed state. Such samples yield information on structure and strength, and are necessary for laboratory determination of shear strength and compressibility. Undisturbed sampling is generally effective only in cohesive soils.

Details of the type and method of sampling used are given on the attached logs.

### INVESTIGATION METHODS

The following is a brief summary of investigation methods currently adopted by the Company and some comments on their use and application. All except test pits, hand auger drilling and portable dynamic cone penetrometers require the use of a mechanical drilling rig which is commonly mounted on a truck chassis.

**Test Pits** – These are normally excavated with a backhoe or a tracked excavator, allowing close examination of the in situ soils if it is safe to descend into the pit. The depth of penetration is limited to about 3m for a backhoe and up to 6m for an excavator. Limitations of test pits are the problems associated with disturbance and difficulty of reinstatement and the consequent effects on close-by structures. Care must be taken if construction is to be

carried out near test pit locations to either properly recompact the backfill during construction or to design and construct the structure so as not to be adversely affected by poorly compacted backfill at the test pit location.

Hand Auger Drilling – A borehole of 50 to 100mm diameter is advanced by manually operated equipment. Premature refusal of the hand augers can occur on a variety of materials such as hard clay, gravel or ironstone, and does not necessarily indicate rock level.

Continuous Spiral Flight Augers - The borehole is advanced using 75 to 115mm diameter continuous spiral flight augers, which are withdrawn at intervals to allow sampling and in situ testing. This is a relatively economical means of drilling in clays and in sands above the water table. Samples are returned to the surface by the flights or may be collected after withdrawal of the auger flights, but they can be very disturbed and may be contaminated. Information from the drilling (as distinct from specific sampling by S.P.T.s or undisturbed samples) is of relatively lower reliability due to remoulding, contamination or softening of samples by groundwater, or uncertainties as to the orginal depth of the samples. Augering below the groundwater table is of even lesser reliability than augering above the water table. Use can be made of a Tugsten Carbide (T.C.) bit for auger drilling into rock to indicate rock quality and continuity by variation in drilling resistance and from examination of recovered rock fragments.

**Wash Boring** – The borehole is usually advanced by a rotary bit, with water being pumped down the drill rods and returned up the annulus, carrying the drill cuttings. Only major changes in stratification can be determined from the cuttings, together with some information from "feel" and rate of penetration.

**Mud Stabilised Drilling** – Either Wash Boring or Continuous Core Drilling can use drilling mud as a circulating fluid to stabilise the borehole. The term "mud" encompasses a range of products ranging from bentonite to polymers such as Revert or Biogel. The mud tends to mask the cuttings and reliable identification is only possible from intermittent intact sampling (e.g. from S.P.T. and U50 samples) or from rock coring, etc.

**Continuous Core Drilling –** A continuous core sample is obtained using a diamond tipped core barrel. Provided full core recovery is achieved (which is not always possible in very weak rocks and granular soils), this technique provides a very reliable (but relatively expensive) method of investigation. In rocks, an N.M.L.C. triple tube core barrel, which gives a core of about 50mm diameter, is usually used with water flush. The length of core recovered is compared to the length drilled and any length not recovered is shown as CORE LOSS. The location of losses are determined on site by the supervising engineer; where the location is uncertain, the loss is placed at the top end of the drill run.

Standard Penetration Tests - Standard Penetration Tests (S.P.T.) are used mainly in non-cohesive soils, but can also be used in cohesive soils as a means of indicating density or strength and also of obtaining a relatively undisturbed sample. The test procedure is described in Australian Standard 1289, "Methods of Testing Soils for Engineering Purposes" - Test F3.1.

The test is carried out in a borehole by driving a 50mm diameter split sample tube with a tapered shoe, under the impact of a 63kg hammer with a free fall of 760mm. It is normal for the tube to be driven in three successive 150mm increments and the 'N' value is taken as the number of blows for the last 300mm. In dense sands, very hard clays or weak rock, the full 450mm penetration may not be practicable and the test is discontinued.

The test results are reported in the following form:

In the case where full penetration is obtained with successive blow counts for each 150mm of, say, 4, 6 and 7 blows, as

In a case where the test is discontinued short of full penetration, say after 15 blows for the first 150mm and 30 blows for the next 40mm, as

The results of the test can be related empirically to the engineering properties of the soil.

Occasionally, the drop hammer is used to drive 50mm diameter thin walled sample tubes (U50) in clays. In such circumstances, the test results are shown on the borehole logs in brackets.

A modification to the S.P.T. test is where the same driving system is used with a solid 60° tipped steel cone of the same diameter as the S.P.T. hollow sampler. The solid cone can be continuously driven for some distance in soft clays or loose sands, or may be used where damage would otherwise occur to the S.P.T. The results of this Dynamic Cone Penetration Test are shown as "N_c" on the borehole logs, together with the number of blows per 150mm penetration.

### Static Cone Penetrometer Testing and

**Interpretation** – Cone penetrometer testing (sometimes referred to as a Dutch Cone) described in this. report has been carried out using an Electronic Friction Cone Penetrometer (E.F.C.P.). The test is described in Australian Standard 1289, Test F5.1.

In the tests, a 35mm diameter rod with a conical tip is pushed continuously into the soil, the reaction being provided by a specially designed truck or rig which is fitted with an hydraulic ram system. Measurements are made of the end bearing resistance on the cone and the frictional resistance on a separate 134mm long sleeve, immediately behind the cone. Transducers in the tip of the assembly are electrically connected by wires passing through the centre of the push rods to an amplifier and recorder unit mounted on the control truck.

As penetration occurs (at a rate of approximately 20mm per second) the information is output on continuous chart recorders. The plotted results given in this report have been copied from the original records.

The information provided on the charts comprises:

- Cone resistance the actual end bearing force divided by the cross sectional area of the cone – expressed in MPa.
- Sleeve friction the frictional force on the sleeve divided by the surface area – expressed in kPa.
- Friction ratio the ratio of sleeve friction to cone resistance, expressed as a percentage.

There are two scales available for measurement of cone resistance. The lower (A) scale (0 to 5 MPa) is used in softer soils where increased sensitivity is required. The main (B) scale has a range of 0 to 50 MPa.

The ratios of the sleeve resistance to cone resistance will vary with the type of soil encountered, with higher relative friction in clays than in sands. Friction ratios of 1% to 2% are commonly encountered in sands and occasionally very soft clays, rising to 4% to 10% in stiff clays and peats. Soil descriptions based on friction ratios are only inferred and must not be considered as exact.

Correlations between E.F.C.P. and S.P.T. values can be developed for both sands and clays but may be site specific.

Interpretation of E.F.C.P. values can be made to empirically derive modulus or compressibility values to allow calculation of foundation settlements.

Stratification can be inferred from the cone and friction traces and from experience and information from nearby boreholes etc. Where shown, this information is presented for general guidance, but must be regarded as interpretive. The test method provides a continuous profile of engineering properties but, where precise information on soil classification is required, direct drilling and sampling may be preferable.

**Portable Dynamic Cone Penetrometers –** Portable Dynamic Cone Penetrometer tests are carried out by driving a rod into the ground with a falling weight hammer and measuring the blows for successive 100mm increments of penetration.

Two relatively similar tests are used:

Cone penetrometer (commonly known as the Scala Penetrometer) – a 16mm rod with a 20mm diameter cone end is driven with a 9kg hammer dropping 510mm (A.S. 1289, Test F3.2). The test was developed initially for pavement subgrade investigations, and correlations of the test results with California Bearing Ratio have been published by various Road Authorities.

Perth sand penetrometer – a 16mm diameter flat ended rod is driven with a 9kg hammer, dropping 600mm (A.S. 1289, Test F3.3). This test was developed for testing the density of sands (originating in Perth) and is mainly used in granular soils and filling.

### LOGS

The borehole or test pit logs presented herein are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on the frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will enable the most reliable assessment, but is not always practicable or possible to justify on economic grounds. In any case, the boreholes or test pits represent only a very small sample of the total subsurface conditions.

The attached explanatory notes define the terms and symbols used in preparation of the logs.

Interpretation of the information shown on the logs, and its application to design and construction, should therefore take into account the spacing of boreholes or test pits, the method of drilling or excavation, the frequency of sampling and testing and the possibility of other than "straight line" variations between the boreholes or test pits. Subsurface conditions between boreholes or test pits may vary significantly from conditions encountered at the borehole or test pit locations.

### GROUNDWATER

Where groundwater levels are measured in boreholes, there are several potential problems:

- Although groundwater may be present, in low permeability soils it may enter the hole slowly or perhaps not at all during the time it is left open.
- A localised perched water table may lead to an erroneous indication of the true water table.
- Water table levels will vary from time to time with seasons or recent weather changes and may not be the same at the time of construction.
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must be washed out of the hole or "reverted" chemically if water observations are to be made.

More reliable measurements can be made by installing standpipes which are read after stabilising at intervals ranging from several days to perhaps weeks

1.1



for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from perched water tables or surface water.

### FILL

The presence of fill materials can often be determinted only by the inclusion of foreign objects (e.g. bricks, steel etc.) or by distinctly unusual colour, texture or fabric. Indentification of the extent of fill materials will also depend on investigation methods and frequency. Where natural soils similar to those at the site are used for fill, it may be difficult with limited testing and sampling to reliably determine the extent of the fill.

The presence of fill materials is usually regarded with caution as the possible variation in density, strength and material type is much greater than with natural soil deposits. Consequently, there is an increased risk of adverse engineering characteristics or behaviour. If the volume and quality of fill is of importance to a project, then frequent test pit excavations are preferable to boreholes.

### LABORATORY TESTING

Laboratory testing is normally carried out in accordance with Australian Standard 1289 "Methods of Testing Soil for Engineering Purposes." Details of the test procedure used are given on the individual report forms and the attached explanatory notes summarise important aspects of the Laboratory Test Procedures adopted.

### ENGINEERING REPORTS

Engineering reports are prepared by qualifed personnel and are based on the information obtained and on current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal (e.g. a three storey building) the information and interpretation may not be relevant if the design proposal is changed (e.g. to a twenty storey building). If this happens, the Company will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical aspects and recommendations or suggestions for design and construction. However, the Company cannot always anticipate or assume responsibility for:

- unexpected variations in ground conditions the potential for this will be partially dependent on borehole spacing and sampling frequency as well as investigation technique.
- changes in policy or interpretation of policy by statutory authorities.

the actions of persons or contractors responding to commercial pressures.

If these occur, the Company will be pleased to assist with investigation or advice to resolve any problems occurring.

### SITE ANOMALIES

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, the Company requests that it immediately be notified. Most problems are much more readily resolved when conditions are exposed than at some later stage, well after the event.

### REPRODUCTION OF INFORMATION FOR CONTRACTUAL PURPOSES

Attention is drawn to the document "Guidelines for the Provision of Geotechnical Information in Tender Documents", published by the Institution of Engineers, Australia. Where information obtained from this investigation is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. The Company would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

### **REVIEW OF DESIGN**

Where major civil or structural developments are proposed <u>or</u> where only a limited investigation has been completed <u>or</u> where the geotechnical conditions/ constraints are quite complex, it is prudent to have a joint design review which involves a senior geotechnical engineer. We would be happy to assist in this regard as an extension of our investigation commission.

### SITE INSPECTION

The Company will always be pleased to provide engineering inspection services for geotechnical aspects of work to which this report is related.

Requirements could range from:

- i) a site visit to confirm that conditions exposed are no worse than those interpreted, to
- ii) a visit to assist the contractor or other site personnel in identifying various soil/rock types such as appropriate footing or pier founding depths, or
- iii) full-time engineering presence on site.

# **GRAPHIC LOG SYMBOLS** FOR SOILS AND ROCKS

ROCK

. (3

:



SOIL



FILL



TOPSOIL



CLAY (CL, CH)



SILT (ML, MH)



SAND (SP, SW)



GRAVEL (GP, GW)



SANDY CLAY (CL, CH)





SILTY CLAY (CL, CH)



GRANITE, GABBRO



BASALT, ANDESITE



+ + + + + + + +

CONGLOMERATE

SILTSTONE, MUDSTONE,

SANDSTONE

CLAYSTONE

LIMESTONE

SHALE







PHYLLITE, SCHIST





TUFF



DOLERITE, DIORITE



ALP.





000

SHEARED OR CRUSHED SEAM

BRECCIATED OR SHATTERED SEAM/ZONE

**ě** é

**IRONSTONE GRAVEL** 



ORGANIC MATERIAL

**OTHER MATERIALS** 

CONCRETE V'rA





COLLUVIUM

SILTY SAND (SM)

CLAYEY SAND (SC)

GRAVELLY CLAY (CL, CH)





CLAYEY GRAVEL (GC)



SANDY SILT (ML)





PEAT AND ORGANIC SOILS



QUARTZITE

Jeffery and Katauskas Pty Ltd



# UNIFIED SOIL CLASSIFICATION TABLE

Laboratory Classification Criteria		ss bəfi ifed as Z Z A	and name of the second	A State and A Stat	2 10 2281 2 10 2282 10 2282 10 228 2 28 2 28 2 29 2 29 2 20 2 20 2 20 2 20 2 20 2 20	nercen	and the set of the set	De		60 EComparing solis at equal liquid limit	xəbni y	8 S		0 10 20 30	Liquid limit	Plasticity chart for laboratory classification of fine grained soils					
Information Required for Describing Soils	Give typical name; indicate approximate percentages of stand and gravel: maximum size; and hardness of the condition, and hardness of the condition, and other pertinent description information; and symbols in parentheses For undisturbed solis add informa- tion on stratification, degree on drainage characteristics and drainage characteristics field a appliar gravely valout 20% hard, angular gravely valout 20% hard, angular gravel par- ticles 12 mm maximum size; inluvial sand; (SM) parenti gravel valor enter gradits coarse to fine, about 10% dry strength; well com- pacted and onoist in place; alluvial sand; (SM) and character of place degree and character of place degree amount and maximum size of the model and that and the south parter of place in place.										ination on structure, stratinca- tion, consistency in undisturbed and remoulded states, moisture and drainage conditions	Example:	Clayey silt, brown; slightly plastic; small percentage of	nne sano: numerous verucal root holes; firm and dry in place; loess; (ML)							
Typical Names	Weil graded gravels, gravel- sand mixtures, little or no fines	Poorly graded gravels, gravel- sand mixtures, little or no fines	Silty gravels, poorly graded gravel-sand-silt mixtures	Clayey gravels, poorly graded gravel-sand-clay mixtures	Well graded sands, gravelly sands, little or no fines	Poorly graded sands, gravelly sands, little or no fines	Silty sands, poorly graded sand- silt mixtures	Clayey sands, poorly graded sand-clay mixtures			Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with slight plasticity	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	Organic silts and organic silt- clays of low plasticity	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts	Inorganic clays of high plas- ticity, fat clays	Organic clays of medium to high plasticity	Peat and other highly organic soils				
Group Symbols a	GIF	GP	сM	20	AKS	SP	WS	sc			ML	CT	70	HW	CH	HO	Pr				
tto su	grain size and substantial all intermediate particle	range of sizes sizes missing	fication pro-	n procedures,	substantial ite particle	Predominantly one size or a range of sizes with some intermediate sizes missing	Predominantly one size or a range of sizes with some intermediate sizes missing	Predominantly one size or a range of sizes with some intermediate sizes missing	one size or a range of sizes ntermediate sizes missing	one size or a range of sizes ntermediate sizes missing	fication pro-	a procedures,	μη Sieve Size	Toughness (consistency near plastic limit)	None	Medium	Slight	Slight to medium	High	Slight to medium	our, odour, y by fibrous
ures basing fractic	Wide range in grain size and substantial amounts of all intermediate particle sizes	Predominantly one size or a range of sizes with some intermediate sizes missing	Nonplastic fines (for identification cedures see ML below)	Plastic fines (for identification procedures, see $CL$ below)	Wide range in grain sizes and substantial amounts of all intermediate particle sizes						one size or a intermediate	Nonplastic fines (for identification pro- ccdures, see ML below)	Plastic fines (for identification procedures see $CL$ below)	aller than 380	Dilatancy (reaction to shaking)	Quick to slow	None to very slow	Slow	Slow to none	None	None to very slow
Field Identification Procedures cles larger than 75 $\mu$ m and bas estimated weights)	Wide range i amounts o sizes	Predominantl with some	Nonplastic fli cedures see	Plastic fines (for i see CL below)	Wide range in amounts o sizes				Nonpíastic fit cedures, s	Plastic fines (for i see <i>CL</i> below)	on Fraction Smaller than 380	Dry Strength. (crushing character- istics)	None to slight	Medium to high	Slight to medium	Slight to medium	High to very high	Medium to high	Readily identified spongy feel and texture		
Field Identif ticles larger th estima	le or no	t fines)			s with a with seciable and of a with a with	nqqs) oms	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					05			oils						
Field Identification Procedures (Excluding particles larger than $75 \mu m$ and basing fractions on estimated weights)	I the smallest particle visible to naked eve)						dentification Procedures	is ei esie ev	vəis mu č	27 5AT) 27 5AT 27 5AT) 27 5AT 27	:/ IIP	clays Limit		11	Highly Organic Soils						
	Fine-grained soils More than half of material is smaller More than half of material is smaller than 75 µm sieve size than 75 µm sieve size																				

NOTE: 1) Soils possessing characteristics of two groups are designated by combinations of group symbols (e.g. GW-GC, well graded gravel-sand mixture with clay fines).

2) Soils with liquid limits 🔆 the order of 35 to 50 may be visually. Lassified as being of medium plasticity.



### LOG SYMBOLS

LOG COLUMN	SYMBOL	DEFINITION
Groundwater Record		Standing water level. Time delay following completion of drilling may be shown.
	<del>C</del>	Extent of borehole collapse shortly after drilling.
	<b>&gt;</b>	Groundwater seepage into borehole or excavation noted during drilling or excavation.
Samples	ES	Soil sample taken over depth indicated, for environmental analysis.
	U50	Undisturbed 50mm diameter tube sample taken over depth indicated.
	DB	Bulk disturbed sample taken over depth indicated.
	DS	Small disturbed bag sample taken over depth indicated.
Field Tests	N = 17 4, 7, 10	Standard Penetration Test (SPT) performed between depths indicated by lines. Individual figures show blows per 150mm penetration. 'R' as noted below.
	$N_c = 5$ $7$ $3R$	Solid Cone Penetration Test (SCPT) performed between depths indicated by lines. Individual figures show blows per 150mm penetration for 60 degree solid cone driven by SPT hammer. 'R' refers to apparent hammer refusal within the corresponding 150mm depth increment.
	VNS = 25	Vane shear reading in kPa of Undrained Shear Strength.
	PID = 100	Photoionisation detector reading in ppm (Soil sample headspace test).
Moisture Condition	MC>PL	Moisture content estimated to be greater than plastic limit.
(Cohesive Soils)	MC≈PL	Moisture content estimated to be approximately equal to plastic limit.
	MC < PL	Moisture content estimated to be less than plastic limit.
(Cohesianlana Esila)	D	DRY - runs freely through fingers.
(Cohesionless Soils)	м	MOIST - does not run freely but no free water visible on soil surface.
	w	WET - free water visible on soil surface.
Strength (Consistency)	VS	VERY SOFT - Unconfined compressive strength less than 25kPa
Cohesive Soils	S	SOFT - Unconfined compressive strength 25-50kPa
	F	FIRM - Unconfined compressive strength 50-100kPa
	St	STIFF - Unconfined compressive strength 100-200kPa
	VSt	VERY STIFF - Unconfined compressive strength 200-400kPa
	·н	HARD - Unconfined compressive strength greater than 400kPa
	( )	Bracketed symbol indicates estimated consistency based on tactile examination or other tests.
Density Index/ Relative		Density Index (I _n ) Range (%) SPT 'N' Value Range (Blows/300mm)
Density (Cohesionless Soils)	VL	Very Loose <15 0-4
	L	Loose 15-35 4-10
	MD	Medium Dense 35-65 10-30
	D	Dense 65-85 30-50
	VD	Very Dense > 85 > 50
	( )	Bracketed symbol indicates estimated density based on ease of drilling or other tests.
Hand Penetrometer	300	Numbers indicate individual test results in kPa on representative undisturbed material unless noted
Readings	250	otherwise.
Remarks	'V' bit	Hardened steel 'V' shaped bit.
	'TC' bit	Tungsten carbide wing bit.
	60	Penetration of auger string in mm under static load of rig applied by drill head hydraulics without rotation of augers.

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### LOG SYMBOLS

### ROCK MATERIAL WEATHERING CLASSIFICATION

TERM	SYMBOL	DEFINITION
Residual Soil	RS	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported.
Extremely weathered rock	xw	Rock is weathered to such an extent that it has "soil" properties, ie it either disintegrates or can be remoulded, in water.
Distinctly weathered rock	WD	Rock strength usually changed by weathering. The rock may be highly discoloured, usually by ironstaining. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores.
Slightly weathered rock	sw	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh rock	FR	Rock shows no sign of decomposition or staining.

### ROCK STRENGTH

Rock strength is defined by the Point Load Strength Index (Is 50) and refers to the strength of the rock substance in the direction normal to the bedding. The test procedure is described by the International Journal of Rock Mechanics, Mining, Science and Geomechanics. Abstract Volume 22, No 2, 1985.

TERM	SYMBOL	ls (50) MPa	FIELD GUIDE
Extremely Low:	EL.		Easily remoulded by hand to a material with soil properties.
		0.03	
Very Low:	VL		May be crumbled in the hand. Sandstone is "sugary" and friable.
		0.1	
Low:	L		A piece of core 150mm long x 50mm dia, may be broken by hand and easily scored
		0.3	with a knife. Sharp edges of core may be friable and break during handling.
Medium Strength:	М		A piece of core 150mm long x 50mm dia, can be broken by hand with difficulty.
		1	Readily scored with knife.
High:	н		A piece of core 150mm long x 50mm dia. core cannot be broken by hand, can be
		3	slightly scratched or scored with knife; rock rings under hammer.
Very High:	VH		A piece of core 150mm long x 50mm dia, may be broken with hand-held pick after
very mgn.			more than one blow. Cannot be scratched with pen knife; rock rings under hammer.
		10	
Extremely High:	EH		A piece of core 150mm long x 50mm dia. is very difficult to break with hand-held
			hammer. Rings when struck with a hammer.

### ABBREVIATIONS USED IN DEFECT DESCRIPTION

ABBREVIATION	DESCRIPTION	NOTES
Be	Bedding Plane Parting	Defect orientations measured relative to the normal to the long core axis
CS	Clay Seam	(ie relative to horizontal for vertical holes)
L,	Joint	
Р	Planar	
Un	Undulating	
S	Smooth	
R	Rough	
IS	Ironstained	
xws	Extremely Weathered Seam	
Cr	Crushed Seam	
60t	Thickness of defect in millimetres	